Bi-CMOS IC LED Driver IC



http://onsemi.com

Overview

LV5026MC is a High voltage LED drive controller which drives LED current up to 3A with external MOSFET. LV5026MC is realized very simple LED circuits with a few external parts. It corresponds to various wide dimming controls including the TRIAC dimming control.

Note) This LV5026MC is designed or developed for general use or consumer appliance. Therefore, it is NOT permitted to use for automotive, communication, office equipment, industrial equipment.

Functions

- High voltage LED controller
- Various Dimming Control
 - -TRIAC & Analog Input & PWM Input
- Soft Start function
- Built-in TRIAC stabilized function
- Built-in circuit of detection of overvoltage of CS pin.
- Selectable Switching frequency [50kHz or 70kHz, open: 50kHz]
- Short protection circuit
- Selectable reference Voltage
 - -Internal 0.605V & External Input Voltage
- Low noise switching system/skip frequency function
 - 5 stages skip mode Frequency
 - Soft driving

Specifications

Maximum Ratings at $Ta = 25^{\circ}C$

Parameter	Symbol	Conditions	Ratings	Unit
Maximum input voltage	V _{IN} max (Note1)		-0.3 to 42	V
REF_OUT, REF_IN, RT, CS, PWM_D, ACS			-0.3 to 7	V
OUT1 pin	V _{OUT} _abs		-0.3 to 42	V
OUT2 pin	V _{OUT} 2_abs		-0.3 to 42	V
Allowable power dissipation	Pd max	With specified board*	1.0	W
Junction temperature	Тј		150	°C
Operating junction temperature	Topj (Note2)		-30 to +125	°C
Storage temperature	Tstg		-40 to +150	°C

^{*1} Specified board: 58.0mm x 54.0mm x 1.6mm (glass epoxy board)

Note1) Absolute maximum ratings represent the values which cannot be exceeded for any length of time.

Note2) Even when the device is used within the range of absolute maximum ratings, as a result of continuous usage under high temperature, high current, high voltage, or drastic temperature change, the reliability of the IC may be degraded. Please contact us for the further details.

Stresses exceeding Maximum Ratings may damage the device. Maximum Ratings are stress ratings only. Functional operation above the Recommended Operating Conditions is not implied. Extended exposure to stresses above the Recommended Operating Conditions may affect device reliability.

Recommended Operating Conditions at $Ta = 25^{\circ}C$

	Parameter	Symbol	Conditions	Ratings	Unit	
Input v	roltage	VIN		8.5 to 24	V	Ì

^{*} Note : supply the stabilized voltage.

Electrical Characteristics at Ta = 25 °C, $V_{\mbox{IN}} = 12 \mbox{V}$, unless otherwise specified.

Parameter	Symbol	Conditions	Ratings			Unit
Parameter	Symbol	Symbol Conditions		typ	max	Unit
Reference voltage block						
Built-in reference voltage	VREF		0.585	0.605	0.625	V
VREF V _{IN} line regulation	VREF_LN	V _{IN} = 8.5 to 24V		±0.5		%
Reference output voltage	REFOUT	I _{REFOUT} = 0.5mA		3.0		V
- Maximum load	REFOUT_MAX		0.5			mA
- equivalent output impedance	REFOUT_RO			10		Ω
Under voltage lockout						
Operation start Input voltage	UVLOON		8	9	10	V
Operation stop input voltage	UVLOOFF		6.3	7.3	8.3	V
Hysteresis voltage	UVLOH			1.7		V
Oscillation	1		<u>.</u>			
Frequency	FOSC1	RT =OPEN	40	50	60	kHz
	FOSC2	RT = REF_OUT	55	70	85	kHz
FOSC1 Switch voltage	V _{OSC} 1		2		5	V
FOSC2 Switch voltage	Vosc2				0.5	V
Maximum ON duty	MAXDuty			93		%
Comparator						
Input offset voltage	V _{IO} _VR			1	10	mV
(Between CS and VREF)						
Input offset voltage	V _{IO} _RI			1	10	mV
(Between CS and REFIN) Input current	I _{IO} SC			160		nA
input current				80		
CS nin may valtage	I _{IO} REF VOM			80	1	nA V
CS pin max voltage	TMSK			150	'	
malfunction prevention mask time	TIVISK			150		ns
PWM_D circuit	L		I	I		
OFF voltage	VOFF		2		5	V
ON voltage	VON		0		0.6	V
Thermal protection circuit	1			I		
Thermal shutdown temperature	TSD	*Design guarantee		165		°C
Thermal shutdown hysteresis	ΔTSD	*Design guarantee		30		°C
Drive Circuit	l	1	1			
OUT sink current	IOI		500	1000		mA
OUT source current	100			120		mA
Minimum On time	TMIN			200	300	ns

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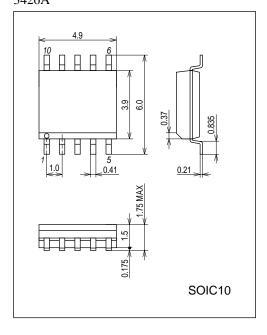
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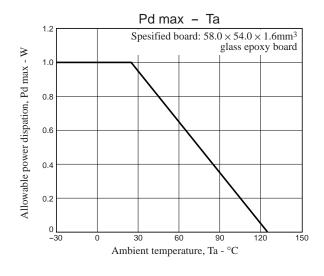
Doromotor	Cumbal	Conditions		Ratings		Llois	
Parameter	Symbol	Conditions	min	typ	max	Unit	
TRIAC Stabilization circuit							
Threshold of OUT2	V _{ACS}	OUT2 = High [less than right record]	2.8	3.0	3.2	V	
OUT2 sink current	I _O 2I	V _{IN} = 12V, OUT2 = 6V		0.6		mA	
OUT2 source current	I _O 2O	V _{IN} = 12V, OUT2 = 6V		0.6		mA	
V _{CC} current							
UVLO mode V _{IN} current	I _{CC} OFF	V _{IN} < UVLOON		80	120	μΑ	
Normal mode V _{IN} current	I _{CC} ON	V _{IN} > UVLOON, OUT = OPEN		0.8		mA	
V _{IN} over voltage protection circuit							
V _{IN} over voltage protection voltage	V _{IN} OVP		24	27	30	V	
V _{IN} current at OVP	I _{IN} OVP	V _{IN} = 30V	0.7	1.0	1.5	mA	
CS terminal abnormal sensing circuit							
Abnormal sensing voltage	CSOCP			1.9		V	

^{*:} Design guarantee (value guaranteed by design and not tested before shipment)

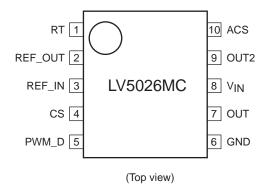
Package Dimensions

unit: mm (typ) 3426A

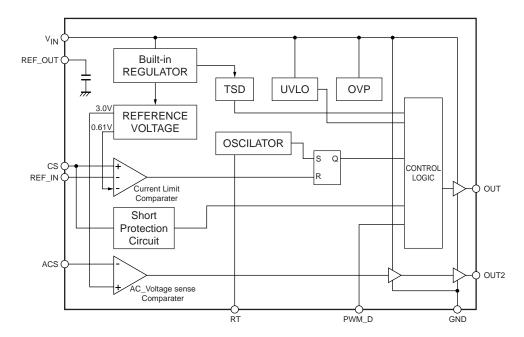




Pin Assignment

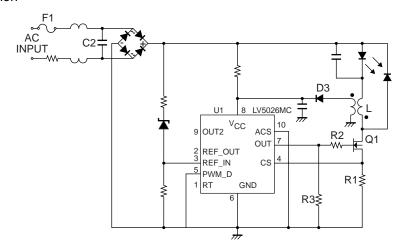


Block Diagram

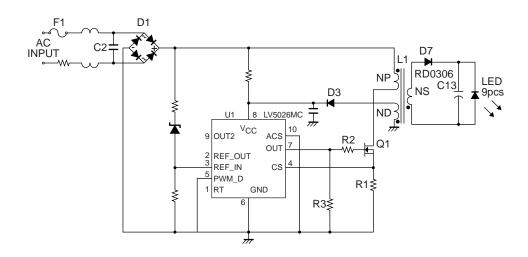


Sample Application Circuit

Non isolation



Isolation



Pin Functions

PIN F	unctions		
Pin No.	Pin name	Pin function	Equivalent circuit
1	RT	Switching frequency selection pin. L or Open: 50kHz switching, H: 70 kHz switching. In case of 70kHz,connect RT pin to REFOUT pin. on time	VREF-OUT Ο (3V typ) RT Ο 1kΩ GND Ο
2	REF_OUT	Built-in 3V Regulate out Pin. If this function isn't used, please connect to nothing.	OVIN OVREF-OUT (3V typ)
3	REF_IN	External LED current Limit Setting pin. If less than VREF (0.61V) voltage is input, Peak current value is used at the input voltage. If more than REF_IN voltage is input, it is done at VREF voltage. If this function isn't used, please connect nothing.	CSO WHO REF_IN GND
4	CS	LED current sensing in. If this terminal voltage exceeds VREF (Or REF_IN), external FET is OFF. And if the voltage of the terminal exceeds 1.9V, LV5026MC turns to latch-off mod	CSO WHO REF_IN GND
5	PWM_D	PWM Dimming pin.L or open: normal operation, H: Stop operation.	V _{IN} Ο Σ 200kΩ Ε 700kΩ
6	GND	GND pin.	0 VIII
7	OUT	Driving the external FET Gate Pin.	→ V _{IN}
8	VIN	Power supply pin. Operation : V _{IN} > UVLOON Stop: V _{IN} < UVLOOFF Switching Stop: V _{IN} > V _{IN} OVP	OOUT
9	OUT2	This pin drive the FET which is stabilized the TRIAC dimming application. If ACS is less than 3V, OUT2 turn High voltage. If this function isn't used, please connect nothing.	$\begin{array}{c c} & & & & \\ & & & & \\ \hline & & & & \\ & & & &$
10	ACS	ACS pin senses AC Voltage. If this function isn't used, please connect GND.	O VIN O ACS

LED current and inductande setting

• Relation ship beween REF_IN and CS pin voltage(Power Factor Crrection(PFC))

The output current value is the average of the current value that flows during one cycle. The current value that flows into coil is a triangular wave shown in the figure below. Make sure to set Ipk so that (average of current value at one cycle) is equal to (LED current value). Ipk is set by the relationship between REF_IN voltage and Rcs voltage.

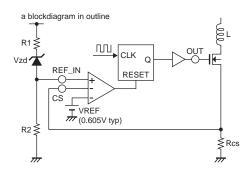
This relationship make Power Factor Correction (PFC). Therefore, it is available to make LED current a sine curve.

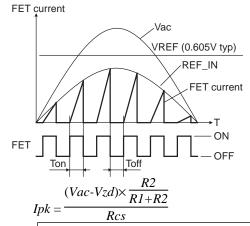
• Setting Zener voltage

Vzd depend on LED voltage (VF). Choose Zener diode around Vf (LED voltage). When VAC voltage is lower than Vf, LED operation is not normal. Using Zener diode prevents incorrect operating during VAC voltage lower than Vf. In detail, refer to [LED current and inductance setting]

In case of REF_IN pin open, this error amplifier negative input(-) is under control of internal VREF voltage

(0.605 Vtyp).





Ipk: peak inductor current

Vf: LED forward voltage drop

Vac: effective value, R.M.S value

VREF: Built-in reference voltage (0.605V)

VREF IN: REF IN voltage (6 pin)

Rs: External sense resistor

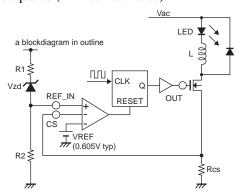
Vzd: Zener diode voltage (REF IN pin)

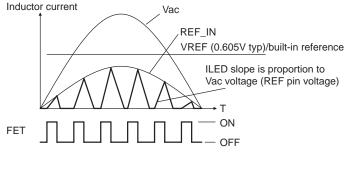
LED current and inductance setting

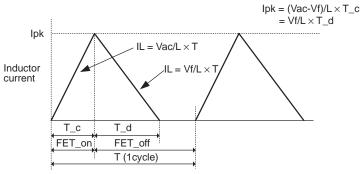
It is available to use both no-isolation and isolation applications.

(For non-isolation application)

The output current value is the average of the current value that flows during one cycle. The current value that flows into coil is a triangular wave shown in the figure below. Make sure to set IL_PK so that (average of current value at one cycle) is equal to (LED current value).







Given that the period when current flows into coil is

DutyI =
$$\frac{T_c + T_d}{T}$$

 $Ipk \times \frac{1}{2} \times (Duty \times T)/T = ILED$
 $Ipk \times \frac{2 \times ILED}{DutyI}$ (1) since $Ipk \times \frac{VREF_IN}{Rcs}$
 $Rcs \times \frac{VFEF_IN}{Ipk} = \frac{DutyI \times VFEF_IN}{2ILED}$ (2)

Ipk: peak inductor current Vf: LED forward voltage drop Vac: effective value(R.M.S value)

VREF: Built-in reference voltage (0.605V)

VREF_IN: REF_IN voltage (6 pin)

Rs: External sense resistor

Vzd: Zener diode voltage (REF_IN pin)

Since formula for LED current is different between on period and off period as shown above,

$$Ipk \times \frac{Vac - Vf}{L} \times T_{-}c = \frac{Vf}{L} \times T_{-}d \quad (3)$$

Since $T_{-}c + T_{-}d = DutyI \times T$, $T_{-}c = DutyI \times T - T_{-}d \quad (4)$

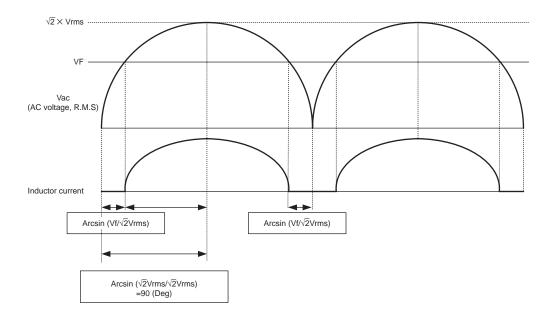
Since
$$T c + T d = DutyI \times T$$
, $T c = DutyI \times T - T d$ (4)

Based on the result of (3) and (4),
$$T_d = DutyI \times T \times \frac{Vac - Vf}{Vac}$$
 (5)

To obtain L from the equation (1), (3), (5),

$$L \times \frac{Vf \times DutyI}{2 \times ILED} \times DutyI \times T = \frac{Vac - Vf}{Vac} = \frac{Vf}{2 \times ILED} \times \frac{1}{fosc} \times \frac{Vac - Vf}{Vac} \times (DutyI)^{2}$$
 (6)

Since LED and inductor are connected in serial in non-isolation mode, LED current flows only when AC voltage exceed VF.



Given that the ratio of inductor current to AC input is DutyAC.

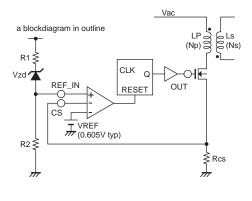
$$DutyAC = \frac{90 - \arcsin\left(\frac{Vf}{\sqrt{2}Vrms}\right)}{90}$$

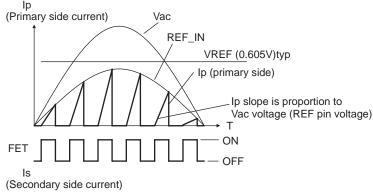
Since the period when the inductor current flows are limited by DutyAC, the formula (6) is represented as follows:

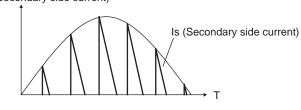
$$L = \frac{Vf}{2 \times ILED} \times \frac{1}{fosc} \times \frac{Vac - Vf}{VIN} \times (DutyI)^{2} \times \left(\frac{90 - \arcsin\left(\frac{Vf}{\sqrt{2}Vrms}\right)}{90}\right)^{2}$$
(7)

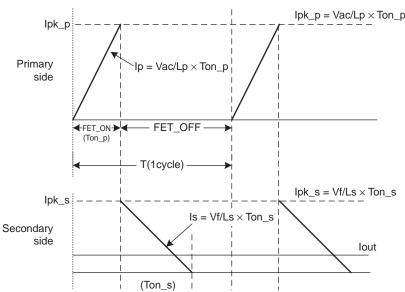
(for Isolation circuit)

Using the circuit diagram below, the wave form of the current that flows to Np and Ns is as follows. Current waveform flows to primary side and secondary.









[Inductance Lp of primary side and sense resistor Rs]

If a peak current flow to transformer is represented as Ipk_p, the power (Pin) charged to the transformer on primary side can be represented as:

$$Pin = \frac{1}{2} \times Lp \times (Ipk_p)^2 \times fosc \quad (11)$$

$$Ipk_p = \frac{Vac}{Lp} \times Ton_p \quad (12)$$

$$Lp = \frac{Vac^{2} \times Ton_p^{2} \times fosc}{2 \times Pin} = \frac{Vac^{2} \times Don_p^{2}}{2 \times Pin \times fosc}$$
 (13)

$$(Don_p = \frac{Ton_p}{T} = Ton_p \times fosc),$$

To substitute the following to the formula below,

$$\therefore \eta = \frac{Pout}{Pin} \quad (14)$$

$$\therefore Lp = \frac{Vac^2 \times Ton_p^2 \times fosc \times \eta}{2 \times Pout} = \frac{Vac^2 \times Don^2 \times \eta}{2 \times Pout \times fosc}$$
 (15)

Sense resistor is obtained as follows.

$$Rs = \frac{VREF_IN}{Ipk_p} = \frac{VREF_IN \times Lp}{Vac \times Ton_p} = \frac{VREF_IN \times Lp}{Vac \times Don_p \times T}$$
(16)

[Inductance Ls of secondary side]

Since output current Iout is the average value of current flows to transformer of secondary side

$$Iout = Ipk_s \times \frac{Ton_s}{T} \times \frac{1}{2} = \frac{Ipk_s \times Don_s}{2} (Don_s = \frac{Ton_s}{T} = Ton_s \times fosc)$$
 (17)

$$Ipk_s = \frac{Vout}{Ls} \times Ton_s = \frac{Vout}{Ls} = \frac{Don_s}{fosc}$$
 (18)

$$Ls = \frac{Vout \times T \times Don_s^2}{2 \times Iout} = \frac{Vout \times Don_s^2}{2 \times Iout \times fosc} = \frac{Vout^2 \times Don_s^2}{2 \times Pout \times fosc}$$
(19)

Calculation of the ratio of transformer coil on primary side and secondary side

Since ratio and inductance of transformer coil is

$$\frac{Ns}{Np} = \frac{\sqrt{Ls}}{\sqrt{Lp}} \qquad (20)$$

substituted equations (15), (19) for (20)

$$\therefore \frac{Np}{Ns} = \frac{Vac}{Vout} \times \sqrt{\eta} \times \frac{Don_p}{Don\ s}$$
 (21)

Calculation of transformer coil on primary side and secondary side

$$N = \frac{Vac \times 10^8}{2 \times \Delta B \times Ae \times fosc}$$
 (22)

 ΔB : variation range of core flux density [Gauss]

Ae: core section area [cm²]

To use Al (L value at 100T),

$$N = \sqrt{\frac{L}{Al}} \times 10^2 \quad (23)$$

L: inductance [µH]

Al: L value at 100T [uH/N²]

lg (Air gap) is obtained as follows:

$$\lg = \frac{\mu_{\rm r} \, \mu_0 \, N^2 \, A_e \, 10^2}{I_{\rm r}} \quad (24)$$

 μr : relative magnetic permeability, $\mu r = 1$

 μ 0: vacuum magnetic permeability μ 0 = $4\pi*10^{-7}$

N: turn count [T]

Ae: core section area [m²]

L: inductance [H]

Bleeder current cuircuit for TRIAC dimmer

1. Operating voltage setting

ACS pin voltage set operating voltage at OUT2. ACS pin threshold volage is 3V typ.

OUT2 operating voltage is set by R1 and R2. R1 and R2 is determined below.

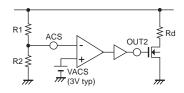
$$ACS = Vac \times \frac{R2}{R1 + R2}$$

2. Bleeder current setting

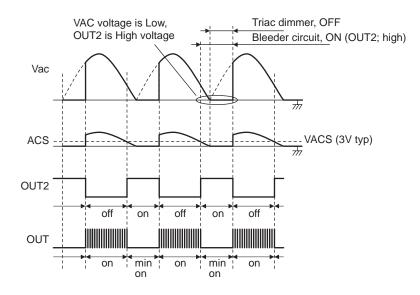
Rd set hold current at Triac dimmer.

Bleeder current is set at Rd depending on Triac dimmer.

a blockdiagram in outline



a blockdiagram in outline



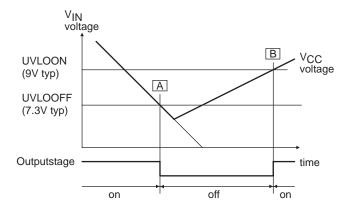
Description of operation

protection function

	tilte	outline	monitor point	note
1	UVLO	Under voltage lock out	V _{CC} voltage	
2	OCP	Over current protection	CS voltage	available FET current
3	OVP	Over voltage protection	V _{CC} voltage	
4	OTP	Over Temperature Protection	PN Junction temperature	
	(TSD)	(Thermal Shut Down)		

1. UVLO (Under voltage lock out)

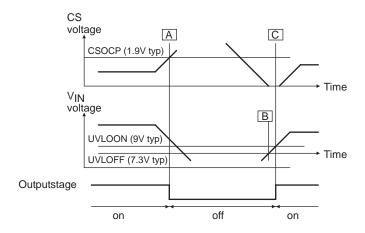
If V_{IN} voltage is 7.3V or lower, then UVLO operates and the IC stops. When UVLO operates, the power supply current of the IC is about $80\mu A$ or lower. If V_{IN} voltage is 9V or higher, then the IC starts switching operation.



2. UVLO (Under voltage lock out)

The CS pin sense the current through the MOS FET switch and the primary side of the transformer. This provides an additional level of protection in the event of a fault. If the voltage of the CS pin exceeds VCSOCP (1.9V typ) (\boxed{A}), the iternal comparator will detect the event and turn off the MOSFET. The peak switch current is calculated Io (peak) [A] = VSOCP [V]/Rsense [Ω]

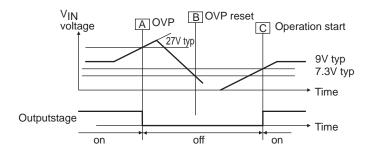
The V_{CC} pin is pulled down to fixed level, keeping the controller lached off. The lach reset occurs when the user disconnects LED from VAC and lets the V_{CC} falls below the V_{CC} reset voltage, UVLOOFF (7.3V typ)(\boxed{B}). Then V_{CC} rise UVLOON (9V typ) (\boxed{C}), restart the switching.



3. OVP (Over voltage protection)

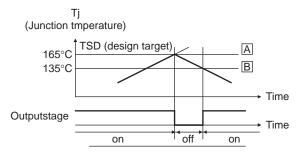
If the voltage of V_{IN} pin is higher than the internal reference voltage $V_{IN}OVP$ (27V typ), switching operation is stopped.

The stopping operation is kept until the voltage of V_{IN} is lower than 7.3V. If the voltage of V_{IN} pin is higher than 9V, the switching operation is restated.



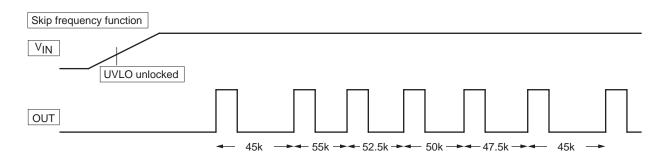
4. TSD (Thermal shut down protection)

The thermal shutdown function works when the junction temperature of IC is 165° C (typ) (\boxed{A}), and the IC switching stops. The IC starts switching operation again when the junction temperature is 135° C typ (\boxed{B}) or lower.



Skip frequency function

LV5026MC contains the skip frequency function for reduction of the peak value of conduction noise. This function changes the frequency as follows.

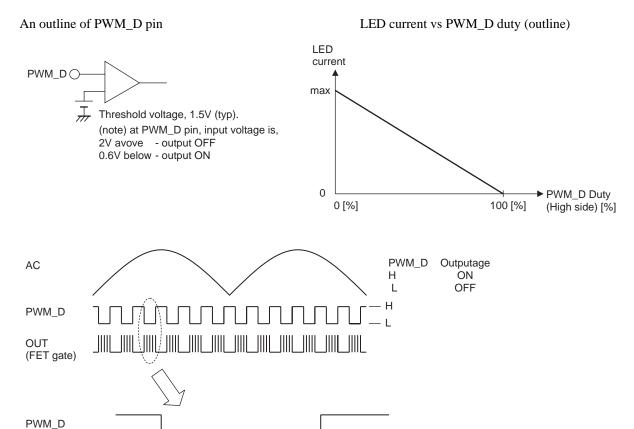


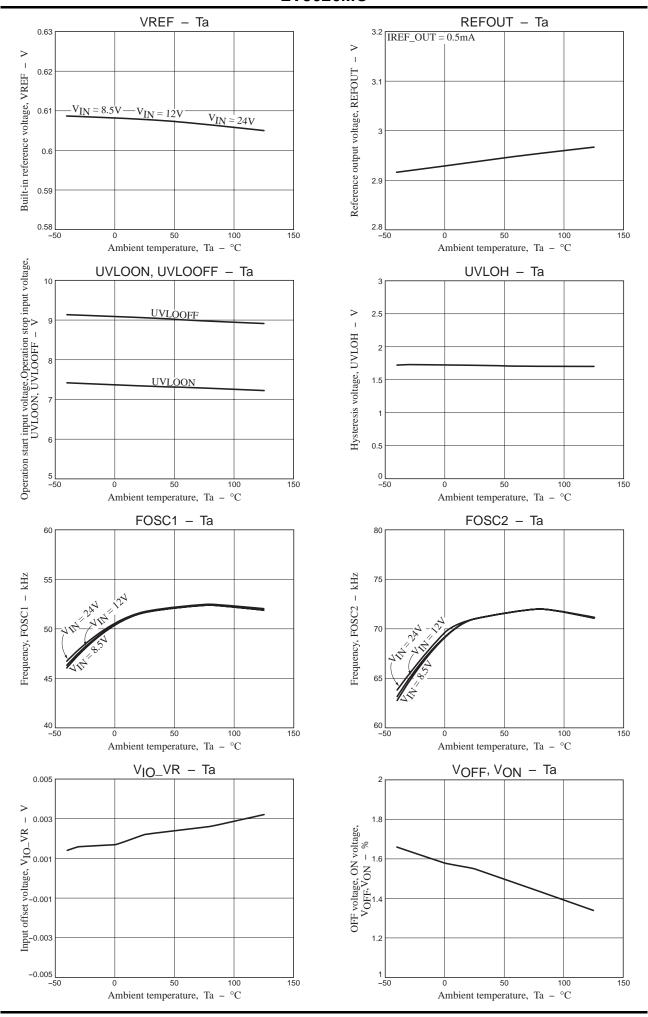
Switching frequency is changed as follows. ... $\times 0.9 \rightarrow \times 1.1 \rightarrow \times 1.05 \rightarrow \times 1 \rightarrow \times 0.95 \rightarrow \times 0.9 \rightarrow \times 1.1 \dots$ It's repeated by this loop.

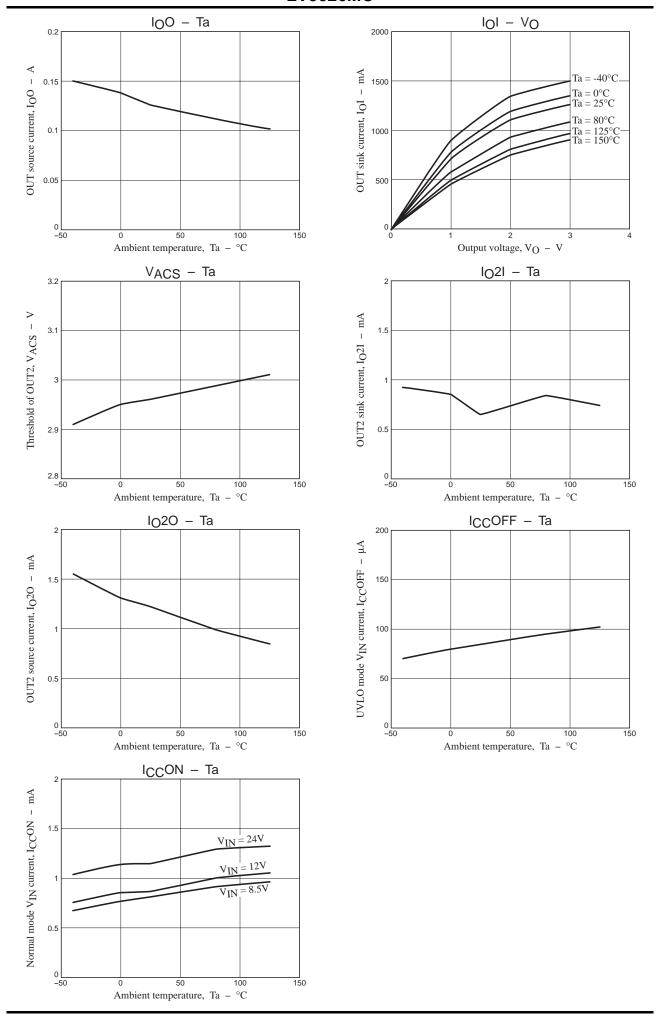
PWM dimmer function

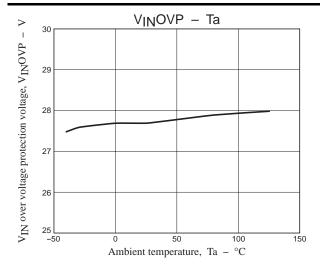
OUT (FET gate) FET current (CS voltage)

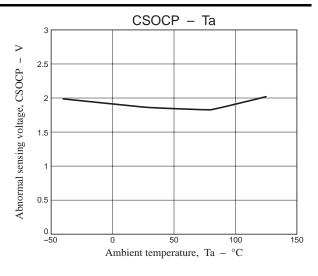
LED current can be adjusted according to Duty of PWM pulse input to PWM dimmer pin. PWM pulse is High (2V to 5V) then switching operation stops, and LED current stops flowing. PWM pulse is Low (under 0.6V), then switching operation stop is released, and it returns to normal operation.











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