## FEATURES

- Conversion Gain: 8.5 dB at 2500 MHz

■ IIP3: 27.7 dBm at 2500 MHz

- Noise Figure: 9.5 dB at 2500 MHz
- 15.9dB NF Under 5dBm Blocking
- High Input P1dB
- 52 dB Channel Isolation at 2500 MHz
- 3.3V Supply, 1.3W Power Consumption
- Low Power Mode for O.8W Consumption
- Independent Channel Shutdown Control
- $50 \Omega$ Single-Ended RF and LO Inputs
- LO Input Matched In All Modes
- OdBm LO Drive Level
- $-40^{\circ} \mathrm{C}$ to $105^{\circ} \mathrm{C}$ Operation
- Small QFN ( $5 \mathrm{~mm} \times 5 \mathrm{~mm}$ ) Package and Solution Size


## APPLICATIONS

- Wireless Infrastructure Diversity Receivers (LTE, WiMAX)
- Transmit DPD Receivers
- MIMO Infrastructure Receivers
- Broadband Microwave Receivers
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Dual 2.3GHz to 4.5 GHz High Dynamic Range Downconverting Mixer DESCRIPTIOn

The LTC®5593 is part of a family of dual-channel high dynamic range, high gain downconverting mixers covering the 600 MHz to 4.5 GHz RF frequency range. The LTC5593 is optimized for 2.3 GHz to 4.5 GHz RF applications. The LO frequency must fall within the 2.1 GHz to 4.2 GHz range for optimum performance. A typical application is a LTE or WiMAX multichannel or diversity receiver with a 2.3GHz to 2.7GHz RF input.

The LTC5593's high conversion gain and high dynamic range enable the use of lossy IF filters in high selectivity receiver designs, while minimizing the total solution cost, board space and system-level variation. A low current mode is provided for additional power savings and each of the mixer channels has independent shutdown control.

High Dynamic Range Dual Downconverting Mixer Family

| PART NUMBER | RF RANGE | LO RANGE |
| :---: | :---: | :---: |
| LTC5590 | 600 MHz to 1.7 GHz | 700 MHz to 1.5 GHz |
| LTC5591 | 1.3 GHz to 2.3 GHz | 1.4 GHz to 2.1 GHz |
| LTC5592 | 1.6 GHz to 2.7 GHz | 1.7 GHz to 2.5 GHz |
| LTC5593 | $\mathbf{2 . 3 \mathrm { GHz } \text { to } 4 . 5 \mathrm { GHz }}$ | $\mathbf{2 . 1 G H z}$ to 4.2 GHz |

## TYPICAL APPLICATION

LTE Diversity Receiver


Wideband Conversion Gain, IIP3 and NF vs IF Frequency (LTC5593 Only, Measured on Evaluation Board)

ABSOLUTE MAXIMUM RATINGS
(Note 1)
Supply Voltage (VCC) ..... 4.0V
IF Supply Voltage (VCCIF) ..... 5.5 V
Enable Voltage (ENA, ENB)

$\qquad$ ..... 0.3 V
Bias Adjust Voltage (IFBA, IFBB) ..... -0.3 V to $\mathrm{V}_{\mathrm{CC}}+0.3 \mathrm{~V}$
Power Select Voltage (ISEL) ............. -0.3 V to $\mathrm{V}_{\text {CC }}+0.3 \mathrm{~V}$
LO Input Power (2GHz to 5GHz) ..... 9dBm
LO Input DC Voltage ..... $\pm 0.1 \mathrm{~V}$
RFA, RFB Input Power (2GHz to 5GHz) ..... 15dBm
RFA, RFB Input DC Voltage ..... $\pm 0.1 \mathrm{~V}$
Operating Temperature Range ( $\mathrm{T}_{\mathrm{C}}$ ) $-40^{\circ} \mathrm{C}$ to $105^{\circ} \mathrm{C}$
Storage Temperature Range

$\qquad$
$-65^{\circ} \mathrm{C}$ to $150^{\circ} \mathrm{C}$
Junction Temperature ( $\mathrm{T}_{\mathrm{J}}$ ) ..... $150^{\circ} \mathrm{C}$
PIn CONFIGURATIOn


## ORDER INFORMATION

| LEAD FREE FINISH | TAPE AND REEL | PART MARKING | PACKAGE DESCRIPTION | TEMPERATURE RANGE |
| :--- | :--- | :--- | :--- | :--- |
| LTC5593IUH\#PBF | LTC5593IUH\#TRPBF | 5593 | $24-$ Lead $(5 \mathrm{~mm} \times 5 \mathrm{~mm})$ Plastic QFN | $-40^{\circ} \mathrm{C}$ to $105^{\circ} \mathrm{C}$ |

Consult LTC Marketing for parts specified with wider operating temperature ranges.
Consult LTC Marketing for information on non-standard lead based finish parts.
For more information on lead free part marking, go to: http://www.linear.com/leadfree/
For more information on tape and reel specifications, go to: http://www.linear.com/tapeandreel/

DC ELECTRICAL CHARACTGRISTICS
unless otherwise noted. Test circuit shown in Figure 1. (Note 2)

| PARAMETER | CONDITIONS | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Power Supply Requirements ( $\mathrm{V}_{\text {CCA }}, \mathrm{V}_{\text {CCB }}, \mathrm{V}_{\text {CCIFA }}, \mathrm{V}_{\text {CCIFB }}$ ) |  |  |  |  |  |
| $\mathrm{V}_{\text {CCA }}, \mathrm{V}_{\text {CCB }}$ Supply Voltage (Pins 12, 19) |  | 3.1 | 3.3 | 3.5 | V |
| $V_{\text {CCIFA }}$, V CCIFB Supply Voltage (Pins 9, 10, 21, 22) |  | 3.1 | 3.3 | 5.3 | V |
| Mixer Supply Current (Pins 12, 19) | Both Channels Enabled |  | 196 | 242 | mA |
| IF Amplifier Supply Current (Pins 9, 10, 21, 22) | Both Channels Enabled |  | 200 | 251 | mA |
| Total Supply Current (Pins 9, 10, 12, 19, 21, 22) | Both Channels Enabled |  | 396 | 493 | mA |
| Total Supply Current - Shutdown | ENA = ENB = Low |  |  | 500 | $\mu \mathrm{A}$ |

Enable Logic Input (ENA, ENB) High = On, Low = Off

| ENA, ENB Input High Voltage (On) |  | 2.5 |  |
| :--- | :--- | :--- | :---: |
| ENA, ENB Input Low Voltage (Off) |  | V |  |
| ENA, ENB Input Current | -0.3 V to $\mathrm{V}_{\text {CC }}+0.3 \mathrm{~V}$ | -20 | 0.3 |
| Turn-On Time |  | 0.9 | V |
| Turn-Off Time |  | $\mu \mathrm{A}$ |  |

Low Power Mode Logic Input (ISEL) High = Low Power, Low = Normal Power Mode

| $I_{\text {SEL }}$ Input High Voltage |  | 2.5 |  | V |
| :---: | :---: | :---: | :---: | :---: |
| IseL $^{\text {Input Low Voltage }}$ |  |  | 0.3 | V |
| ISEL Input Current | -0.3 V to $\mathrm{V}_{\text {CC }}+0.3 \mathrm{~V}$ | -20 | 30 | $\mu \mathrm{A}$ |

Low Power Mode Current Consumption (ISEL = High)

| Mixer Supply Current (Pins 12, 19) | Both Channels Enabled | 127 | 159 | mA |
| :--- | :--- | :--- | :--- | :--- |
| IF Amplifier Supply Current (Pins 9, 10, 21, 22) | Both Channels Enabled | 120 | 157 | mA |
| Total Supply Current (Pins $9,10,12,19,21,22)$ | Both Channels Enabled | 247 | 316 | mA |

## LTC5593

AC ELECTRICAL CHARACTERISTICS $\mathrm{V}_{\mathrm{CC}}=3.3 \mathrm{~V}, \mathrm{~V}_{\mathrm{CCIF}}=3.3 \mathrm{~V}, \mathrm{ENA}=\mathrm{ENB}=$ high, $\mathrm{I}_{\mathrm{SEL}}=10 \mathrm{low}, \mathrm{T}_{\mathrm{C}}=25^{\circ} \mathrm{C}$,
$P_{\mathrm{LO}}=0 \mathrm{dBm}, \mathrm{P}_{\mathrm{RF}}=-3 \mathrm{dBm}$ ( $\Delta \mathrm{f}=2 \mathrm{MHz}$ for two tone IIP3 tests), unless otherwise noted. Test circuit shown in Figure 1. (Notes 2, 3, 4)


Low Side LO Downmixer Application: $I_{\text {SEL }}=$ Low, IF $=190 \mathrm{MHz}, \mathrm{f}_{\mathrm{LO}}=\mathrm{f}_{\mathrm{RF}}-\mathrm{f}_{\mathrm{IF}}$

| PARAMETER | CONDITIONS | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Conversion Gain | $\begin{aligned} & \hline \mathrm{RF}=2300 \mathrm{MHz} \\ & \mathrm{RF}=2500 \mathrm{MHz} \\ & \mathrm{RF}=2700 \mathrm{MHz} \\ & \mathrm{RF}=3200 \mathrm{MHz} \\ & \mathrm{RF}=3500 \mathrm{MHz} \\ & \mathrm{RF}=3800 \mathrm{MHz} \end{aligned}$ | 6.8 | $\begin{aligned} & 9.0 \\ & 8.5 \\ & 8.0 \\ & 8.1 \\ & 7.6 \\ & 7.0 \end{aligned}$ |  | dB $d B$ $d B$ $d B$ $d B$ $d B$ |
| Conversion Gain Flatness | $\mathrm{RF}=2500 \pm 30 \mathrm{MHz}, \mathrm{LO}=2310 \mathrm{MHz}$, IF $=190 \pm 30 \mathrm{MHz}$ |  | $\pm 0.25$ |  | dB |
| Conversion Gain vs Temperature | $\mathrm{T}_{\mathrm{C}}=-40^{\circ} \mathrm{C}$ to $105^{\circ} \mathrm{C}, \mathrm{RF}=2500 \mathrm{MHz}$ |  | -0.008 |  | $\mathrm{dB} /{ }^{\circ} \mathrm{C}$ |
| Input 3rd Order Intercept | $\begin{aligned} & \mathrm{RF}=2300 \mathrm{MHz} \\ & \mathrm{RF}=2500 \mathrm{MHz} \\ & \mathrm{RF}=2700 \mathrm{MHz} \\ & \mathrm{RF}=3200 \mathrm{MHz} \\ & \mathrm{RF}=3500 \mathrm{MHz} \\ & \mathrm{RF}=3800 \mathrm{MHz} \end{aligned}$ | 24.0 | $\begin{aligned} & 26.1 \\ & 27.7 \\ & 27.6 \\ & 26.5 \\ & 26.0 \\ & 26.1 \end{aligned}$ |  | dBm <br> dBm <br> dBm <br> dBm <br> dBm <br> dBm |
| SSB Noise Figure | $\begin{aligned} & \hline \mathrm{RF}=2300 \mathrm{MHz} \\ & \mathrm{RF}=2500 \mathrm{MHz} \\ & \mathrm{RF}=2700 \mathrm{MHz} \\ & \mathrm{RF}=3200 \mathrm{MHz} \\ & \mathrm{RF}=3500 \mathrm{MHz} \\ & \mathrm{RF}=3800 \mathrm{MHz} \end{aligned}$ |  | $\begin{gathered} \hline 9.4 \\ 9.5 \\ 9.7 \\ 11.2 \\ 11.3 \\ 12.0 \end{gathered}$ |  | dB $d B$ $d B$ $d B$ $d B$ $d B$ |
| SSB Noise Figure Under Blocking | $\begin{aligned} & \mathrm{f}_{\mathrm{RF}}=2500 \mathrm{MHz}, \mathrm{f}_{\mathrm{LO}}=2310 \mathrm{MHz}, \mathrm{f}_{\mathrm{BLOCK}}=2600 \mathrm{MHz}, \\ & \mathrm{P}_{\text {BLOCK }}=5 \mathrm{dBm} \\ & \mathrm{P}_{\text {BLOCK }}=8 \mathrm{dBm} \end{aligned}$ |  | $\begin{aligned} & 15.9 \\ & 19.4 \end{aligned}$ |  | dB dB |
| 2RF-2LO Output Spurious Product $\left(f_{\mathrm{RF}}=\mathrm{f}_{\mathrm{LO}}+\mathrm{f}_{\mathrm{IF}} / 2\right)$ | $\begin{aligned} & \mathrm{f}_{\mathrm{RF}}=2405 \mathrm{MHz} \text { at }-10 \mathrm{dBm}, \mathrm{f}_{\mathrm{LO}}=2310 \mathrm{MHz}, \\ & \mathrm{f}_{\mathrm{IF}}=190 \mathrm{MHz} \end{aligned}$ |  | -64 |  | dBc |
| 3RF-3LO Output Spurious Product $\left(f_{R F}=f_{L O}+f_{f /} / 3\right)$ | $\begin{aligned} & \mathrm{f}_{\mathrm{RF}}=2373.3 \mathrm{MHz} \text { at }-10 \mathrm{dBm}, \mathrm{f}_{\mathrm{LO}}=2310 \mathrm{MHz}, \\ & \mathrm{f}_{\mathrm{IF}}=190 \mathrm{MHz} \end{aligned}$ |  | -70 |  | dBC |
| Input 1dB Compression | $\begin{aligned} & f_{\mathrm{RF}}=2500 \mathrm{MHz}, V_{\text {CCIF }}=3.3 \mathrm{~V} \\ & \mathrm{f}_{\mathrm{RF}}=2500 \mathrm{MHz}, \mathrm{~V}_{\mathrm{CCIF}}=5 \mathrm{~V} \end{aligned}$ |  | $\begin{aligned} & 10.4 \\ & 13.7 \end{aligned}$ |  | $\begin{aligned} & \mathrm{dBm} \\ & \mathrm{dBm} \end{aligned}$ |

## LTC5593

AC ELECTRICAL CHARACTGRISTICS $v_{\text {CC }}=3.3 V, v_{\text {ClIIF }}=3.3 v$, ENA $=E N B=$ high, $, T_{C}=25^{\circ} C, P_{L 0}=0 \mathrm{dBm}$,
$P_{\text {RF }}=-3 \mathrm{dBm}$ ( $\Delta \mathrm{f}=2 \mathrm{MHz}$ for 2-tone IIP3 tests), unless otherwise noted. Test circuit shown in Figure 1. (Notes 2, 3)
Low Power Mode, Low Side LO Downmixer Application: $I_{\text {SEL }}=$ High, IF $=190 \mathrm{MHz}, \mathrm{f}_{\mathrm{LO}}=\mathrm{f}_{\mathrm{RF}}-\mathrm{f}_{\mathrm{IF}}$

| PARAMETER | CONDITIONS | MIN | TYP |
| :--- | :--- | :---: | :---: |
| Conversion Gain | $\mathrm{RF}=2500 \mathrm{MHz}$ | 7.8 | UNITS |
|  | $\mathrm{RF}=3500 \mathrm{MHz}$ | 6.3 | dB |
| Input 3rd Order Intercept | $\mathrm{RF}=2500 \mathrm{MHz}$ | 21.6 | dB |
|  | $\mathrm{RF}=3500 \mathrm{MHz}$ | 21.0 | dBm |
| SSB Noise Figure | $\mathrm{RF}=2500 \mathrm{MHz}$ | 9.2 | dBm |
|  | $\mathrm{RF}=3500 \mathrm{MHz}$ | dB |  |
| Input 1dB Compression | $\mathrm{RF}=2500 \mathrm{MHz}, \mathrm{V}_{\text {CCIF }}=3.3 \mathrm{~V}$ | 11.5 | dB |
|  | $\mathrm{RF}=2500 \mathrm{MHz}, \mathrm{V}_{\text {CCIF }}=5 \mathrm{~V}$ | 10.0 | dBm |

High Side LO Downmixer Application: $I_{\text {SEL }}=$ Low, $\mathrm{IF}=190 \mathrm{MHz}, \mathrm{f}_{\mathrm{LO}}=\mathrm{f}_{\mathrm{RF}}+\mathrm{f}_{\mathrm{IF}}$

| PARAMETER | CONDITIONS | MIN TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: |
| Conversion Gain | $\begin{aligned} & \hline \mathrm{RF}=2300 \mathrm{MHz} \\ & \mathrm{RF}=2500 \mathrm{MHz} \\ & \mathrm{RF}=2700 \mathrm{MHz} \\ & \mathrm{RF}=3200 \mathrm{MHz} \\ & \mathrm{RF}=3500 \mathrm{MHz} \\ & \mathrm{RF}=3800 \mathrm{MHz} \end{aligned}$ | $\begin{aligned} & 8.7 \\ & 8.4 \\ & 8.0 \\ & 7.7 \\ & 7.2 \\ & 6.8 \end{aligned}$ |  | dB $d B$ $d B$ $d B$ $d B$ $d B$ |
| Conversion Gain Flatness | $\mathrm{RF}=2500 \pm 30 \mathrm{MHz}, \mathrm{LO}=2690 \mathrm{MHz}$, IF $=190 \pm 30 \mathrm{MHz}$ | $\pm 0.1$ |  | dB |
| Conversion Gain vs Temperature | $\mathrm{T}_{\mathrm{C}}=-40^{\circ} \mathrm{C}$ to $105^{\circ} \mathrm{C}, \mathrm{RF}=2500 \mathrm{MHz}$ | -0.006 |  | $\mathrm{dB} /{ }^{\circ} \mathrm{C}$ |
| Input 3rd Order Intercept | $\begin{aligned} & \mathrm{RF}=2300 \mathrm{MHz} \\ & \mathrm{RF}=2500 \mathrm{MHz} \\ & \mathrm{RF}=2700 \mathrm{MHz} \\ & \mathrm{RF}=3200 \mathrm{MHz} \\ & \mathrm{RF}=3500 \mathrm{MHz} \\ & \mathrm{RF}=3800 \mathrm{MHz} \end{aligned}$ | $\begin{aligned} & 25.1 \\ & 25.5 \\ & 25.9 \\ & 24.5 \\ & 24.2 \\ & 23.8 \end{aligned}$ |  | dBm <br> dBm <br> dBm <br> dBm <br> dBm <br> dBm |
| SSB Noise Figure | $\begin{aligned} & \mathrm{RF}=2300 \mathrm{MHz} \\ & \mathrm{RF}=2500 \mathrm{MHz} \\ & \mathrm{RF}=2700 \mathrm{MHz} \\ & \mathrm{RF}=3200 \mathrm{MHz} \\ & \mathrm{RF}=3500 \mathrm{MHz} \\ & \mathrm{RF}=3800 \mathrm{MHz} \end{aligned}$ | $\begin{aligned} & 10.0 \\ & 10.5 \\ & 10.6 \\ & 11.1 \\ & 12.1 \\ & 12.1 \end{aligned}$ |  | $d B$ $d B$ $d B$ $d B$ $d B$ $d B$ |
| SSB Noise Figure Under Blocking | $\begin{aligned} & \mathrm{f}_{\mathrm{RF}}=2500 \mathrm{MHz}, \mathrm{f}_{\mathrm{LO}}=2690 \mathrm{MHz}, \mathrm{f}_{\mathrm{BLOCK}}=2400 \mathrm{MHz}, \\ & \mathrm{P}_{\text {BLOCK }}=5 \mathrm{dBm} \\ & \mathrm{P}_{\mathrm{BLOCK}}=8 \mathrm{dBm} \end{aligned}$ | $\begin{aligned} & 17.8 \\ & 21.8 \end{aligned}$ |  | dB dB |
| 2LO-2RF Output Spurious Product $\left(f_{R F}=f_{L O}-f_{I F} / 2\right)$ | $\begin{aligned} & \mathrm{f}_{\mathrm{RF}}=2595 \mathrm{MHz} \text { at }-10 \mathrm{dBm}, \mathrm{f}_{\mathrm{LO}}=2690 \mathrm{MHz}, \\ & \mathrm{f}_{\mathrm{IF}}=190 \mathrm{MHz} \end{aligned}$ | -66 |  | dBc |
| 3L0-3RF Output Spurious Product $\left(f_{\mathrm{RF}}=f_{\mathrm{LO}}-f_{\mathrm{IF}} / 3\right)$ | $\begin{aligned} & f_{\mathrm{RF}}=2626.67 \mathrm{MHz} \text { at }-10 \mathrm{dBm}, \mathrm{f}_{\mathrm{LO}}=2690 \mathrm{MHz}, \\ & \mathrm{f}_{\mathrm{IF}}=190 \mathrm{MHz} \end{aligned}$ | -75 |  | dBc |
| Input 1dB Compression | $\begin{aligned} & \mathrm{RF}=2500 \mathrm{MHz}, \mathrm{~V}_{\text {CCIF }}=3.3 \mathrm{~V} \\ & \mathrm{RF}=2500 \mathrm{MHz}, \mathrm{~V}_{\text {CCIF }}=5 \mathrm{~V} \end{aligned}$ | $\begin{aligned} & 10.7 \\ & 14.1 \end{aligned}$ |  | dBm dBm |

AC ELECTRICAL CHARACTERISTICS $V_{c c}=3.3 v, V_{c C l I F}=3.3 v, E N A=E N B=H i g h, T_{C}=25^{\circ} C, P_{L 0}=0 d B m$, $P_{\mathrm{RF}}=-3 \mathrm{dBm}$ ( $\Delta \mathrm{f}=2 \mathrm{MHz}$ for two tone IIP3 tests), unless otherwise noted. Test circuit shown in Figure 1. (Notes 2, 3)

Low Power Mode, High Side LO Downmixer Application: $I_{\text {SEL }}=H i g h, ~ I F=190 M H z, f_{L O}=f_{\text {RF }}+f_{I F}$

| PARAMETER | CONDITIONS | MIN | TYP |
| :--- | :--- | ---: | ---: |
| Conversion Gain | $\mathrm{RF}=2500 \mathrm{MHz}$ | 7.4 | UNITS |
|  | $\mathrm{RF}=3500 \mathrm{MHz}$ | dB |  |
| Input 3rd Order Intercept | $\mathrm{RF}=2500 \mathrm{MHz}$ | 2.9 | dB |
|  | $\mathrm{RF}=3500 \mathrm{MHz}$ | 22.1 | dBm |
| SSB Noise Figure | $\mathrm{RF}=2500 \mathrm{MHz}$ | 20.2 | dBm |
|  | $\mathrm{RF}=3500 \mathrm{MHz}$ | 10.6 | dB |
| Input 1dB Compression | $\mathrm{RF}=2500 \mathrm{MHz}, \mathrm{VCCIF}=3.3 \mathrm{~V}$ | 12.4 | dB |
|  | $\mathrm{RF}=2500 \mathrm{MHz}, \mathrm{V}_{\mathrm{CCIF}}=5 \mathrm{~V}$ | 10.9 | dBm |

Note 1: Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. Exposure to any Absolute Maximum Rating condition for extended periods may affect device reliability and lifetime.
Note 2: The LTC5593 is guaranteed functional over the case operating temperature range of $-40^{\circ} \mathrm{C}$ to $105^{\circ} \mathrm{C}$. $\left(\theta_{\mathrm{JC}}=7^{\circ} \mathrm{C} / \mathrm{W}\right)$

Note 3: SSB Noise Figure measured with a small-signal noise source, bandpass filter and 6dB matching pad on RF input, bandpass filter and 6 dB matching pad on the LO input, and no other RF signals applied.
Note 4: Channel $A$ to channel $B$ isolation is measured as the relative IF output power of channel $B$ to channel $A$, with the RF input signal applied to channel $A$. The RF input of channel $B$ is $50 \Omega$ terminated and both mixers are enabled.

## TYPICAL AC PGRFORMANCE CHARACTERISTICS 2.3 GHz to 2.7 GHzz , low side LO.

$\mathrm{V}_{\mathrm{CC}}=3.3 \mathrm{~V}, \mathrm{~V}_{\mathrm{CCIF}}=3.3 \mathrm{~V}, \mathrm{ENA}=\mathrm{ENB}=$ high, $\mathrm{I}_{\mathrm{SEL}}=\mathrm{low}, \mathrm{T}_{\mathrm{C}}=25^{\circ} \mathrm{C}, \mathrm{P}_{\mathrm{LO}}=0 \mathrm{dBm}, \mathrm{P}_{\mathrm{RF}}=-3 \mathrm{dBm}(-3 \mathrm{dBm} /$ tone for 2-tone IIP3 tests, $\Delta f=2 M H z), I F=190 \mathrm{MHz}$, unless otherwise noted. Test circuit shown in Figure 1.


$\mathrm{V}_{\mathrm{CC}}=3.3 \mathrm{~V}, \mathrm{~V}_{\mathrm{CCIF}}=3.3 \mathrm{~V}, \mathrm{ENA}=\mathrm{ENB}=\mathrm{High}, \mathrm{I}_{\mathrm{SEL}}=\mathrm{Iow}, \mathrm{T}_{\mathrm{C}}=25^{\circ} \mathrm{C}, \mathrm{P}_{\mathrm{LO}}=0 \mathrm{dBm}, \mathrm{P}_{\mathrm{RF}}=-3 \mathrm{dBm}(-3 \mathrm{dBm} /$ tone for 2-tone IIP3 tests, $\Delta f=2 \mathrm{MHz}), \mathrm{IF}=190 \mathrm{MHz}$, unless otherwise noted. Test circuit shown in Figure 1.


5593 G10
SSB Noise Figure vs RF Blocker Level


Conversion Gain Distribution


Single-Tone IF Output Power, $2 \times 2$ and $3 \times 3$ Spurs vs RF Input Power


5593 G11
LO Leakage vs LO Frequency


5593 G14
IIP3 Distribution

$2 \times 2$ and $3 \times 3$ Spurs vs RF Frequency


5593 G12
RF Isolation vs RF Frequency


5593 G15
SSB Noise Figure Distribution


## TYPICAL AC PERFORMANCE CHARACTERISTICS

2.3 GHz to 2.7 GHz , low side LO, $\mathrm{I}_{\mathrm{SEL}}=$ high (low power mode). $\mathrm{V}_{\mathrm{CC}}=3.3 \mathrm{~V}, \mathrm{~V}_{\text {CIIF }}=3.3 \mathrm{~V}, \mathrm{ENA}=\mathrm{ENB}=\mathrm{High}, \mathrm{T}_{\mathrm{C}}=25^{\circ} \mathrm{C}, \mathrm{P}_{\mathrm{LO}}=0 \mathrm{dBm}$, $P_{R F}=-3 \mathrm{dBm}(-3 \mathrm{dBm} /$ tone for 2-tone IIP3 tests, $\Delta \mathrm{f}=2 \mathrm{MHz}), \mathrm{IF}=190 \mathrm{MHz}$, unless otherwise noted. Test circuit shown in Figure 1 .


2300 MHz Conversion Gain, IIP3 and NF vs LO Power


Conversion Gain, IIP3 and NF vs Supply Voltage (Single Supply)


SSB NF vs RF Frequency


2500MHz Conversion Gain, IIP3 and NF vs LO Power


Conversion Gain, IIP3 and RF Input P1dB vs Temperature


Channel Isolation vs RF Frequency


2700MHz Conversion Gain, IIP3 and NF vs LO Power


## RF Isolation and LO Leakage vs Frequency



## TYPICAL AC PGRFORMANCE CHARACTERISTICS

2.3 GHz to 2.7 GHz , high side $\mathrm{LO} . \mathrm{V}_{\mathrm{CC}}=3.3 \mathrm{~V}, \mathrm{~V}_{\text {CCIF }}=3.3 \mathrm{~V}, \mathrm{ENA}=\mathrm{ENB}=$ high, $\mathrm{I}_{\text {SEL }}=10 w, \mathrm{~T}_{\mathrm{C}}=25^{\circ} \mathrm{C}, \mathrm{P}_{\mathrm{LO}}=0 \mathrm{dBm}, \mathrm{P}_{\mathrm{RF}}=-3 \mathrm{dBm}$ $(-3 d B m / t o n e$ for 2 -tone IIP3 tests, $\Delta f=2 \mathrm{MHz}$ ), $\mathrm{IF}=190 \mathrm{MHz}$, unless otherwise noted. Test circuit shown in Figure 1 .


2300MHz Conversion Gain, IIP3 and NF vs LO Power


5593 G31
Conversion Gain, IIP3 and NF vs Supply Voltage (Single Supply)


SSB NF vs RF Frequency


## 2500MHz Conversion Gain,

 IIP3 and NF vs LO Power

5593 G32

## Conversion Gain, IIP3 and RF

 Input P1dB vs Temperature

5593 G35

Channel Isolation vs RF Frequency


2700MHz Conversion Gain, IIP3 and NF vs LO Power


5593 G33

## RF Isolation and LO Leakage vs Frequency



## TYPICAL AC PGRFORmANCE CHARACTERISTICS

2.3 GHz to 2.7 GHz , high side LO, $\mathrm{I}_{\text {SEL }}=$ high (low power mode). $\mathrm{V}_{\mathrm{CC}}=3.3 \mathrm{~V}, \mathrm{~V}_{\text {CCIF }}=3.3 \mathrm{~V}, \mathrm{ENA}=\mathrm{ENB}=$ high, $\mathrm{T}_{\mathrm{C}}=25^{\circ} \mathrm{C}, \mathrm{P}_{\mathrm{LO}}=0 \mathrm{dBm}$, $P_{\mathrm{RF}}=-3 \mathrm{dBm}(-3 \mathrm{dBm} /$ tone for 2-tone IIP3 tests, $\Delta \mathrm{f}=2 \mathrm{MHz}), \mathrm{IF}=190 \mathrm{MHz}$, unless otherwise noted. Test circuit shown in Figure 1 .


## TYPICAL AC PGRFORMANC CHARACTERISTICS

2.7 GHz to 4 GHz , low side LO. $\mathrm{V}_{\mathrm{CC}}=3.3 \mathrm{~V}, \mathrm{~V}_{\text {CLIF }}=3.3 \mathrm{~V}$, ENA $=\mathrm{ENB}=$ high, $\mathrm{I}_{\mathrm{SEL}}=\operatorname{low}, \mathrm{T}_{\mathrm{C}}=25^{\circ} \mathrm{C}, \mathrm{P}_{\mathrm{LO}}=0 \mathrm{dBm}, \mathrm{P}_{\mathrm{RF}}=-3 \mathrm{dBm}$



## 3200MHz Conversion Gain, IIP3 and NF vs LO Power



Conversion Gain, IIP3 and NF vs Supply Voltage (Single Supply)


SSB NF vs RF Frequency


## 3500MHz Conversion Gain, IIP3 and NF vs LO Power



## Conversion Gain, IIP3 and RF Input P1dB vs Temperature



## Channel Isolation vs RF Frequency



## 3800MHz Conversion Gain,

 IIP3 and NF vs LO Power

RF Isolation and LO Leakage vs Frequency


## TYPICAL AC PERFORMANCE CHARACTGRISTICS

2.7 GHz to 4 GHz , low side LO, $\mathrm{I}_{\text {SEL }}=$ high (low power mode). $\mathrm{V}_{\mathrm{CC}}=3.3 \mathrm{~V}, \mathrm{~V}_{\text {CLIF }}=3.3 \mathrm{~V}, \mathrm{ENA}=\mathrm{ENB}=$ high, $\mathrm{T}_{\mathrm{C}}=25^{\circ} \mathrm{C}, \mathrm{P}_{\mathrm{LO}}=\mathrm{OdBm}$, $P_{\mathrm{RF}}=-3 \mathrm{dBm}(-3 \mathrm{dBm} /$ tone for 2-tone IIP3 tests, $\Delta \mathrm{f}=2 \mathrm{MHz}$ ), IF $=190 \mathrm{MHz}$, unless otherwise noted. Test circuit shown in Figure 1.


## 3200MHz Conversion Gain, IIP3 and NF vs LO Power



5593 G58
Conversion Gain, IIP3 and NF vs Supply Voltage (Single Supply)


SSB NF vs RF Frequency


3500MHz Conversion Gain, IIP3 and NF vs LO Power


5593 G59
Conversion Gain, IIP3 and RF Input P1dB vs Temperature


## Channel Isolation vs RF Frequency




5593 G60

## RF Isolation and LO Leakage

 vs Frequency

## TYPICAL AC PERFORMANCE CHARACTERISTICS

2.7 GHz to 4 GHz , high side LO. $\mathrm{V}_{\text {CC }}=3.3 \mathrm{~V}, \mathrm{~V}_{\text {CCIF }}=3.3 \mathrm{~V}, \mathrm{ENA}=\mathrm{ENB}=$ high, $\mathrm{I}_{\text {SEL }}=10 w, \mathrm{~T}_{\mathrm{C}}=25^{\circ} \mathrm{C}, \mathrm{P}_{\mathrm{L}}=0 \mathrm{dBm}, \mathrm{P}_{\mathrm{RF}}=-3 \mathrm{dBm}$ $(-3 \mathrm{dBm} /$ tone for 2-tone IIP3 tests, $\Delta \mathrm{f}=2 \mathrm{MHz}), \mathrm{IF}=190 \mathrm{MHz}$, unless otherwise noted. Test circuit shown in Figure 1.


5593 G 64

## 3200MHz Conversion Gain, IIP3 and NF vs LO Power



5593667
Conversion Gain, IIP3 and NF
vs Supply Voltage (Single Supply)


5593 G70

SSB NF vs RF Frequency


5593 G65
3500MHz Conversion Gain, IIP3 and NF vs LO Power


5593 G68

## Conversion Gain, IIP3 and RF Input P1dB vs Temperature



Channel Isolation vs RF Frequency


5593 G66
3800MHz Conversion Gain, IIP3 and NF vs LO Power


5593 G69

## RF Isolation and LO Leakage

 vs Frequency

## TYPICAL AC PGRFORMANCE CHARACTGRISTICS

2.7 GHz to 4 GHz , high side LO, $\mathrm{I}_{\text {SEL }}=$ high (low power mode). $\mathrm{V}_{\mathrm{CC}}=3.3 \mathrm{~V}, \mathrm{~V}_{\text {CCIF }}=3.3 \mathrm{~V}, E N A=E N B=$ high, $\mathrm{T}_{\mathrm{C}}=25^{\circ} \mathrm{C}, \mathrm{P}_{\mathrm{LO}}=0 \mathrm{dBm}$, $P_{\mathrm{RF}}=-3 \mathrm{dBm}(-3 \mathrm{dBm} /$ /tone for 2-tone IIP3 tests, $\Delta \mathrm{f}=2 \mathrm{MHz}$ ), $\mathrm{IF}=190 \mathrm{MHz}$, unless otherwise noted. Test circuit shown in Figure 1.


3200MHz Conversion Gain, IIP3 and NF vs LO Power


Conversion Gain, IIP3 and NF vs Supply Voltage (Single Supply)


SSB NF vs RF Frequency


3500 MHz Conversion Gain, IIP3 and NF vs LO Power


Conversion Gain, IIP3 and RF Input P1dB vs Temperature


Channel Isolation vs RF Frequency


3800MHz Conversion Gain, IIP3 and NF vs LO Power


RF Isolation and LO Leakage vs Frequency


## TYPICAL DC PGRFORMANCE CHARACTERISTICS

$I_{\text {SEL }}=$ low, ENA $=$ ENB $=$ high, test circuit shown in Figure 1

$I_{\text {SEL }}=$ high (low power mode), ENA = ENB = high, test circuit shown in Figure 1


Total Supply Current
vs Temperature ( $V_{\text {CC }}+V_{\text {cCIF }}$ )


## Total Supply Current

 vs Temperature ( $V_{\text {CC }}+V_{\text {cCIF }}$ )

## PIn functions

RFA, RFB (Pins 1, 6): Single-Ended RF Inputs for Channels A and B . These pins are internally connected to the primary sides of the RF input transformers, which have low DC resistance to ground. Series DC-blocking capacitors should be used to avoid damage to the integrated transformer when DC voltage is present at the RF inputs. The RF inputs are impedance matched when the LO input is driven with a $0 \pm 6 \mathrm{dBm}$ source between 2.1 GHz and 4.2GHz and the channels are enabled.

CTA, CTB (Pins 2, 5): RF Transformer Secondary CenterTap on Channels A and B . These pins may require bypass capacitors to ground to optimize IIP3 performance. Each pin has an internally generated bias voltage of 1.2 V and must be DC -isolated from ground and $\mathrm{V}_{\mathrm{C}}$.
GND (Pins 3, 4, 7, 13, 15, 24, Exposed Pad Pin 25): Ground. These pins must be soldered to the RF ground plane on the circuit board. The exposed pad metal of the package provides both electrical contact to ground and good thermal contact to the printed circuit board.
IFGNDB, IFGNDA (Pins 8, 23): DC Ground Returns for the IF Amplifiers. These pins must be connected to ground to complete the DC current paths for the IF amplifiers. Chip inductors may be used to tune LO-IF and RF-IF leakage. Typical DC current is 100 mA for each pin.
IFB+, IFB- ${ }^{-}$IFA-, IFA ${ }^{+}$(Pins 9, 10, 21, 22): Open-Collector Differential Outputs for the IF Amplifiers of Channels B and A. These pins must be connected to a DC supply through impedance matching inductors, or transformer center-taps. Typical DC current consumption is 50 mA into each pin.

IFBB, IFBA (Pins 11, 20): Bias Adjust Pins for the IF Amplifiers. These pins allow independent adjustment of the internal IF buffer currents for channels $B$ and $A$, respectively. The typical DC voltage on these pins is 2.2 V . If not used, these pins must be DC isolated from ground and $V_{C C}$.
$V_{\text {CCB }}$ and $V_{\text {CcA }}$ (Pins 12, 19): Power Supply Pins for the LO Buffers and Bias Circuits. These pins must be connected to a regulated 3.3 V supply with bypass capacitors located close to the pins. Typical current consumption is 98 mA per pin.
ENB, ENA (Pins 14, 17): Enable Pins. These pins allow Channels B and A , respectively, to be independently enabled. An applied voltage of greater than 2.5 V activates the associated channel while a voltage of less than 0.3 V disables the channel. Typical input current is less than $10 \mu \mathrm{~A}$. These pins must not be allowed to float.
LO (Pin 16): Single-Ended Local Oscillator Input. This pin is internally connected to the primary side of the LO input transformer and has a low DC resistance to ground.
Series DC-blocking capacitors should be used to avoid damage to the integrated transformer when DC voltage is present at the LO input. The LO input is internally matched to $50 \Omega$ for all states of ENA and ENB.
Isel (Pin 18): Low Power Select Pin. Whenthis pin is pulled low (<0.3V), both mixer channels are biased at the normal current level for best RF performance. When greater than 2.5 V is applied, both channels operate at reduced current, which provides reasonable performance at lower power consumption. This pin must not be allowed to float.

## LTC5593

## BLOCK DIAGRAM



## TEST CIRCUIT



| L1, L2 vs IF FREQUENCIES |  |
| :---: | :---: |
| IF (MHz) | L1A, L1B, L2A, L2B (nH) |
| 140 | 270 |
| 190 | 150 |
| 240 | 100 |
| 300 | 56 |
| 380 | 33 |
| 470 | 22 |


| REF DES | VALUE | SIZE | VENDOR |
| :---: | :---: | :---: | :---: |
| C1A, C1B, <br> C3A, C3B <br> C5A, C5B | $22 p F$ | 0402 | AVX |
| C2 | $1.5 p F$ | 0402 | AVX |
| C8A, C8B | 10 pF | 0402 | AVX |
| C4, C6 | $1 \mu F$ | 0603 | AVX |
| C7A, C7B | 1000 pF | 0402 | AVX |
| L1A, L1B <br> L2A, L2B | 150 nH | 0603 | Coilcraft |
| T1A, T1B <br> (Alternate) | TC4-1W-7ALN+ <br> (WBC4-6TLB) |  | Mini-Circuits <br> (Coilcraft) |

Figure 1. Standard Test Circuit Schematic (190MHz IF)

## APPLICATIONS InFORMATION

## Introduction

The LTC5593 consists of two identical mixer channels driven by a common LO input signal. Each high linearity mixer consists of a passive double-balanced mixer core, IF buffer amplifier, LO buffer amplifier and bias/enable circuits. See the Pin Functions and Block Diagram sections for a description of each pin. Each of the mixers can be shutdown independently to reduce power consumption and low current mode can be selected that allows a trade-off between performance and powerconsumption. The RFand LO inputs are single-ended and are internally matched to $50 \Omega$. Iow side or high side LO injection can be used. The IF outputs are differential. The evaluation circuit, shown in Figure 1, utilizes bandpass IF output matching and an IF transformer to realize a $50 \Omega$ single-ended IF output. The evaluation board layout is shown in Figure 2.


Figure 2. Evaluation Board Layout

## RF Inputs

The RF inputs of channels $A$ and $B$ are identical. The RF input of channel $A$, shown in Figure 3, is connected to the primary winding of an integrated transformer. $A 50 \Omega$ match is realized when a series external capacitor, C1A, is connected to the RF input. C1A is also needed for DC blocking if the source has DC voltage present, since the primary side of the RF transformer is internally DC-grounded. The $D C$ resistance of the primary is approximately $3.6 \Omega$.

The secondary winding of the RF transformer is internally connected to the channel A passive mixer core. The center-tap of the transformer secondary is connected to Pin 2 (CTA) to allow the connection of bypass capacitor, C8A. The value of C8A can be adjusted to improve the


Figure 3. Channel A RF Input Schematic

## APPLICATIONS INFORMATION

channel-to-channel isolation at specific RF operation frequency with minor impact to conversion gain, linearity and noise performance. The channel-to-channel isolation performance with different values of C8A is given in Figure 4. When used, it should be located within 2 mm of Pin 2 for proper high frequency decoupling. The nominal DC voltage on the CTA pin is 1.2 V .


5593 F04
Figure 4. Channel-to-Channel Isolation vs C8 Values
For the RF inputs to be properly matched, the appropriate LO signal must be applied to the LO input. A broadband input match is realized with $\mathrm{C} 1 \mathrm{~A}=22 \mathrm{pF}$. The measured input return loss is shown in Figure 5 for LO frequencies of $2.4 \mathrm{GHz}, 3.0 \mathrm{GHz}$ and 3.6 GHz . These LO frequencies correspond to lower, middle and upper values in the LO range. As shown in Figure 5, the RF input impedance is dependent on LO frequency, although a single value of C1A is adequate to cover the 2.3 GHz to 4.0 GHz RF band.


Figure 5. RF Port Return Loss

The RF input impedance and input reflection coefficient, versus RF frequency, are listed in Table 1. The reference plane for this data is Pin 1 of the IC, with no external matching, and the LO is driven at 2.31 GHz .

Table 1. RF Input Impedance and S11
(at Pin1, No External Matching, LO Input Driven at 2.31GHz)

| FREQUENCY <br> (GHZ) | RF INPUT <br> IMPEDANCE | S11 |  |
| :---: | :---: | :---: | :---: |
|  |  | ANGLE |  |
| 2.0 | $74.2+\mathrm{j} 13.6$ | 0.22 | 23.1 |
| 2.2 | $69.4-\mathrm{j} 6.4$ | 0.17 | -15.2 |
| 2.4 | $45.2-\mathrm{j} 3.0$ | 0.06 | -146.0 |
| 2.6 | $45.6+\mathrm{j} 6.5$ | 0.08 | 120.3 |
| 2.8 | $48.3+j 10.9$ | 0.11 | 92.3 |
| 3.0 | $51.5+\mathrm{j} 14.1$ | 0.14 | 75.9 |
| 3.2 | $57.1+\mathrm{j} 15.5$ | 0.16 | 57.3 |
| 3.4 | $62.6+\mathrm{j} 11.8$ | 0.15 | 37.2 |
| 3.6 | $64.3+\mathrm{j} 4.7$ | 0.13 | 16.0 |
| 3.8 | $63.6-\mathrm{j} 6.8$ | 0.13 | -23.2 |
| 4.0 | $50.8-\mathrm{j} 10.7$ | 0.11 | -79.4 |

## LO Input

The LO input, shown in Figure 6, is connected to the primary winding of an integrated transformer. A $50 \Omega$ impedance match from 2.1 GHz to 3.4 GHz is realized at the LO port by adding a 1.5 pF external series capacitor, C 2 . This capacitor is also needed for DC blocking if the LO source has DC voltage present, since the primary side of the LO transformer is DC-grounded internally. The DC resistance of the primary is approximately $1.8 \Omega$. For LO frequency


Figure 6. LO Input Schematic

## APPLICATIONS InFORMATION

from 3.4 GHz to 3.8 GHz , the LO port can be well matched by using $\mathrm{C} 2=0.6 \mathrm{pF}$ and $\mathrm{L} 4=10 \mathrm{nH}$.
The secondary of the transformer drives a pair of high speed limiting differential amplifiers for channels A and B. The LTC5593's LO amplifiers are optimized for the 2.1GHz to 4.2 GHz LO frequency range; however, LO frequencies outside this frequency range may be used with degraded performance.

The LO port is always $50 \Omega$ matched, even when one or both of the channels is disabled. This helps to reduce frequency pulling of the LO source when the mixer is switched between different operating states. Figure 7 illustrates the LO port return loss for the different operating modes.

The nominal LO input level is OdBm, though the limiting amplifiers will deliver excellent performance over $a \pm 6 \mathrm{dBm}$ input power range. Table 2 lists the LO input impedance and input reflection coefficient versus frequency.

Table 2. LO Input Impedance vs Frequency
(at Pin 16, No External Matching, ENA = ENB = High)

| FREQUENCY <br> (GHz) | INPUT <br> IMPEDANCE | S11 |  |
| :---: | :---: | :---: | :---: |
|  |  | ANGLE |  |
| 2.0 | $33.8+\mathrm{j} 22.8$ | 0.32 | 110.3 |
| 2.2 | $34.8+\mathrm{j} 22.2$ | 0.31 | 109.7 |
| 2.4 | $34.5+\mathrm{j} 21.8$ | 0.31 | 110.9 |
| 2.6 | $32.5+\mathrm{j} 22.8$ | 0.34 | 111.9 |
| 2.8 | $30.7+\mathrm{j} 25.9$ | 0.38 | 108.8 |
| 3.0 | $29.6+\mathrm{j} 30.1$ | 0.43 | 103.4 |
| 3.2 | $29.3+\mathrm{j} 34.8$ | 0.47 | 97.1 |
| 3.4 | $29.3+\mathrm{j} 38.7$ | 0.50 | 92.1 |
| 3.6 | $30.7+\mathrm{j} 43.1$ | 0.52 | 86.0 |
| 3.8 | $33.0+\mathrm{j} 46.9$ | 0.52 | 80.5 |
| 4.0 | $36.1+\mathrm{j} 49.8$ | 0.52 | 75.6 |



Figure 7. LO Input Return Loss

## IF Outputs

The IF amplifiers in channels $A$ and $B$ are identical. The IF amplifier for channel $A$, shown in Figure 8, has differential open collector outputs (IFA+ and IFA ${ }^{-}$), a DC ground return pin (IFGNDA), and a pin for adjusting the internal bias (IFBA). The IF outputs must be biased at the supply voltage (VCCIFA), which is applied through matching inductors L1A and L2A. Alternatively, the IF outputs can be biased through the center tap of a transformer (T1A). The common node of L1A and L2A can be connected to the center tap of the transformer. Each IF output pin draws approximately 50 mA of DC supply current ( 100 mA total). An external load resistor, R2A, can be used to improve impedance matching if desired.

IFGNDA (Pin 23) must be grounded or the amplifier will not draw DC current. Inductor L3A may improve LO-IF and RF-IF leakage performance in some applications, but is otherwise not necessary. Inductors should have small resistance for DC. High DC resistance in L3A will reduce the IF amplifier supply current, which will degrade RF performance.

## APPLICATIONS INFORMATION



Figure 8. IF Amplifier Schematic with Bandpass Match

For optimum single-ended performance, the differential IF output must be combined through an external IF transformer or a discrete IF balun circuit. The evaluation board (see Figures 1 and 2) uses a 4:1 IF transformer for impedance transformation and differential to single-ended conversion. It is also possible to eliminate the IFtransformer and drive differential filters or amplifiers directly.
The IF output impedance can be modeled as $260 \Omega$ in parallel with 2.3 pF . The equivalent small-signal model, including bondwire inductance, is shown in Figure 9. Frequency-dependent differential IF output impedance is listed in Table 3. This data is referenced to the package pins (with no external components) and includes the effects of IC and package parasitics.

## Bandpass IF Matching

The bandpass IF matching configuration, shown in Figures 1 and 8, is best suited for IF frequencies in the 90 MHz to 600 MHz range. Resistor R2A may be used to


Figure 9. IF Output Small-Signal Model
reduce the IF output resistance for greater bandwidth and inductors L1A and L2A resonate with the internal IF output capacitance at the desired IF frequency. The value of L1A, L2A can be estimated as follows:

$$
\mathrm{L} 1 \mathrm{~A}=\mathrm{L} 2 \mathrm{~A}=\frac{1}{\left[\left(2 \pi f_{\mathrm{IF}}\right)^{2} \cdot 2 \cdot \mathrm{C}_{\mathrm{IF}}\right]}
$$

where $\mathrm{C}_{\text {IF }}$ is the internal IF capacitance (listed in Table 3).

## APPLICATIONS InFORMATION

Table 3．IF Output Impedance vs Frequency

| FREQUENCY（MHz） | DIFFERENTIAL OUTPUT <br> IMPEDANCE（RIF $\\|$ XIF $^{\left.\left(\mathbf{C}_{\text {IF }}\right)\right)}$ |
| :---: | :---: |
| 90 | $291 \\|-\mathrm{j} 714(2.5 \mathrm{pF})$ |
| 140 | $282 \\|-\mathrm{j} 463(2.5 \mathrm{pF})$ |
| 190 | $274 \\|-\mathrm{j} 353(2.4 \mathrm{pF})$ |
| 240 | $265 \\|-\mathrm{j} 278(2.4 \mathrm{pF})$ |
| 300 | $252 \\|-\mathrm{j} 225(2.4 \mathrm{pF})$ |
| 380 | $231 \\|-\mathrm{j} 177(2.4 \mathrm{pF})$ |
| 500 | $227 \\|-\mathrm{j} 127(2.5 \mathrm{pF})$ |

Values of L1A and L2A are tabulated in Figure 1 for vari－ ous IF frequencies．The measured IF output return loss for bandpass IF matching is plotted in Figure 10.
Performances of 470MHz IF output frequency with low side LO injection using bandpass IF matching is shown in Figure 11．The test circuit schematic and components values are shown in Figure 1 with R2 open in this example． The test conditions are： $\mathrm{V}_{\text {CC }}=3.3 \mathrm{~V}, \mathrm{~V}_{\text {CCIF }}=3.3 \mathrm{~V}$ ，ENA $=$ $E N B=$ high，$I_{S E L}=$ low， $\mathrm{T}_{\mathrm{C}}=25^{\circ} \mathrm{C}$.


5593 F10
Figure 10．IF Output Return Loss with Bandpass Matching

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Figure 11．Performances of 470MHz IF Using Bandpass Matching

## Lowpass IF Matching

For IF frequencies below 90 MHz ，the inductance values become unreasonably high and the lowpass topology shown in Figure 12 is preferred．This topology also can provide improved RF to IF and LO to IF isolation．VCCIFA is supplied through the center tap of the 4：1 transformer． A lowpass impedance transformation is realized by shunt


Figure 12．IF Output with Lowpass Matching

## APPLICATIONS INFORMATION

elements R2A and C9A (in parallel with the internal RIF and CIF), and series inductors L1A and L2A. Resistor R2A is used to reduce the IF output resistance for greater bandwidth, or it can be deleted for the highest conversion gain. The final impedance transformation to $50 \Omega$ is realized by transformer T1A. The measured IF output return loss for lowpass IF matching with R2A and C9A open is plotted in Figure 13. The LTC5593 demo board (see Figure 2) has been laid out to accommodate this matching topology with only minor modifications.


5591 F13
Figure 13. IF Output Return Loss with Lowpass Matching

## IF Amplifier Bias

The IF amplifier delivers excellent performance with $V_{\text {CCIF }}$ $=3.3 \mathrm{~V}$, which allows a single supply to be used for $\mathrm{V}_{C C}$ and $V_{\text {CCIF }}$. At $V_{\text {CCIF }}=3.3 \mathrm{~V}$, the RF input P1dB of the mixer is limited by the output voltage swing. For higher P1dB, in this case, resistor R2A (Figure 1) can be used to reduce the output impedance and thus the voltage swing, thus improving P1dB. The trade-off for improved P1dB will be lower conversion gain.

With $\mathrm{V}_{\text {CCIF }}$ increased to 5 V the P 1 dB increases by over 3 dB , at the expense of higher power consumption. Mixer P1dB performance at 2500 MHz is tabulated in Table 4 for
$V_{\text {CCIF }}$ values of 3.3 V and 5 V . For the highest conversion gain, high-Q wire-wound chip inductors are recommended for L1A and L2A, especially when using $\mathrm{V}_{\text {CCIF }}=3.3 \mathrm{~V}$. Iow cost multilayer chip inductors may be substituted, with a slight reduction in conversion gain.

Table 4. Performance Comparison with $\mathrm{V}_{\text {CCIF }}=3.3 \mathrm{~V}$ and 5 V (RF = 2500MHz, Low Side LO, IF = 190MHz, ENA = ENB = High)

| $\mathbf{V}_{\text {CCIF }}$ <br> $(\mathbf{V})$ | R2A <br> $(\boldsymbol{\Omega})$ | $\mathbf{I}_{\mathbf{C C I F}}$ <br> $(\mathbf{m A})$ | $\mathbf{G}_{\mathbf{C}}$ <br> $(\mathbf{d B})$ | $\mathbf{P 1 d B}$ <br> $(\mathbf{d B m})$ | IIP3 <br> $(\mathbf{d B m})$ | $\mathbf{N F}$ <br> $(\mathbf{d B})$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 953 | 200 | 8.5 | 10.4 | 27.7 | 9.5 |
|  | 0 pen | 200 | 9.6 | 9.6 | 27.2 | 9.5 |
| 5 | 953 | 207 | 8.4 | 13.7 | 28.5 | 9.7 |
|  | Open | 207 | 9.5 | 13.3 | 27.4 | 9.7 |

The IFBA pin (Pin 20) is available for reducing the DC current consumption of the IF amplifier, at the expense of IIP3. The nominal DC voltage at Pin 20 is 2.1 V , and this pin should be left open-circuited for optimum performance. The internal bias circuit produces a 4 mA reference for the IF amplifier, which causes the amplifier to draw approximately 100 mA . If resistor R1A is connected to Pin 20 as shown in Figure 8, a portion of the reference current can be shunted to ground, resulting in reduced IF amplifier current. For example, R1A $=470 \Omega$ will shunt away 1.4 mA from Pin 20 and the IF amplifier current will be reduced by $35 \%$ to approximately 65 mA . Table 5 summarizes RF performance versus total IF amplifier current when both channels are enabled.

Table 5. Mixer Performance with Reduced IF Amplifier Current $R F=2500 \mathrm{MHz}$, Low Side LO, IF $=190 \mathrm{MHz}, \mathrm{V}_{\text {CC }}=\mathrm{V}_{\text {CCIF }}=3.3 \mathrm{~V}$

| R1A, R1B | $\mathbf{I}_{\text {CCIF }}$ <br> $(\mathbf{m A})$ | $\mathbf{G}_{\mathbf{C}}$ <br> $(\mathbf{d B})$ | IIP3 <br> $(\mathbf{d B m})$ | $\mathbf{P 1 d B}$ <br> $(\mathbf{d B m})$ | $\mathbf{N F}$ <br> $(\mathbf{d B})$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Open | 200 | 8.5 | 27.7 | 10.4 | 9.5 |
| $3.3 \mathrm{k} \Omega$ | 176 | 8.4 | 26.7 | 10.5 | 9.5 |
| $1.0 \mathrm{k} \Omega$ | 151 | 8.1 | 24.9 | 10.5 | 9.4 |
| $470 \Omega$ | 130 | 8.0 | 23.5 | 10.4 | 9.3 |

## APPLICATIONS InFORMATION

## Low Power Mode

Both mixer channels can be set to low power mode using the $I_{\text {SEL }}$ pin. This allows flexibility to choose a reduced current mode of operation when lower RF performance is acceptable. Figure 14 shows a simplified schematic of the $I_{\text {SEL }}$ pin interface. When $I_{\text {SEL }}$ is set low ( $<0.3 \mathrm{~V}$ ), both channels operate at nominal DC current. When $\mathrm{I}_{\text {SEL }}$ is set high ( $>2.5 \mathrm{~V}$ ), the DC currents in both channels are reduced, thus reducing power consumption. The performance in low power mode and normal power mode are compared in Table 6.

Table 6. Performance Comparison Between Different Power Mode RF = 2500MHz, Low Side LO, IF = 190MHz, ENA = ENB = High

| $\mathbf{I}_{\text {SEL }}$ | $\mathbf{I}_{\text {TotaL }}$ <br> $(\mathbf{m A})$ | $\mathbf{G}_{\mathbf{C}}$ <br> $(\mathbf{d B})$ | IIP3 <br> $(\mathbf{d B m})$ | $\mathbf{P 1 d B}$ <br> $(\mathbf{d B m})$ | $\mathbf{N F}$ <br> $(\mathbf{d B})$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Low | 396 | 8.5 | 27.7 | 10.4 | 9.5 |
| High | 247 | 7.8 | 21.6 | 10.0 | 9.2 |

## Enable Interface

Figure 15 shows a simplified schematic of the ENA pin interface (ENB is identical). To enable channel $A$, the ENA voltage must be greater than 2.5 V . If the enable function is not required, the enable pin can be connected directly to $\mathrm{V}_{\mathrm{CC}}$. The voltage at the enable pin should never exceed the power supply voltage $\left(\mathrm{V}_{\mathrm{CC}}\right)$ by more than 0.3 V . If this should occur, the supply current could be sourced through the ESD diode, potentially damaging the IC.

The Enable pins must be pulled high or low. If left floating, the on/off state of the IC will be indeterminate. If a three-state condition can exist at the enable pins, then a pull-up or pull-down resistor must be used.


Figure 14. ISEL Interface Schematic

## Supply Voltage Ramping

Fast ramping of the supply voltage can cause a current glitch in the internal ESD protection circuits. Depending on the supply inductance, this could result in a supply voltage transient that exceeds the maximum rating. A supply voltage ramp time of greater than 1 ms is recommended.

## Spurious Output Levels

Mixer spurious output levels versus harmonics of the RF and LO are tabulated in Table 7. The spur levels were measured on a standard evaluation board using the test circuit shown in Figure 1. The spur frequencies can be calculated using the following equation:

$$
f_{S P U R}=\left(M \bullet f_{R F}\right)-\left(N \bullet f_{L O}\right)
$$

Table 7. IF Output Spur Levels (dBc)
$R F=2500 \mathrm{MHz}, \mathrm{F}_{\mathrm{RF}}=-3 \mathrm{dBm}, \mathrm{F}_{\mathrm{LO}}=0 \mathrm{dBm}, \mathrm{F}_{\mathrm{IF}} 190 \mathrm{MHz}$, Low Side LO,
$\mathrm{V}_{\mathrm{CC}}=3.3 \mathrm{~V}, \mathrm{~V}_{\text {CCIF }}=3.3 \mathrm{~V}, \mathrm{ENA}=$ ENB $=$ High, $\mathrm{I}_{\text {SEL }}=$ Low, $\mathrm{T}_{\mathrm{C}}=25^{\circ} \mathrm{C}$

| N |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|  | 0 |  | -40 | -48 | -60 | -51 | -83 | -62 | -74 | * |
|  | 1 | -48 | -0 | -75 | -62 | -69 | -69 | * | * | * |
|  | 2 | -74 | -78 | -61 | -85 | -82 | -87 | -89 | * | * |
| $\cdots$ | 3 | * | * | * | -65 | * | * | * | * | * |
|  | 4 | * | * | * | * | * | * | * | * | * |
|  | 5 |  | * | * | * | * | * | * | * | * |
|  | 6 |  |  | * | * | * | * | * | * | * |

*Less than -90 dBc


Figure 15. ENA Interface Schematic

PACKAGE DESCRIPTION
Please refer to http://www.linear.com/designtools/packaging/ for the most recent package drawings.

## UH Package

24-Lead Plastic QFN ( $5 \mathrm{~mm} \times 5 \mathrm{~mm}$ )
(Reference LTC DWG \# 05-08-1747 Rev A)


NOTE:

1. DRAWING IS NOT A JEDEC PACKAGE OUTLINE
2. DRAWING NOT TO SCALE
3. ALL DIMENSIONS ARE IN MILLIMETERS
4. DIMENSIONS OF EXPOSED PAD ON BOTTOM OF PACKAGE DO NOT INCLUDE MOLD FLASH. MOLD FLASH, IF PRESENT, SHALL NOT EXCEED 0.20 mm ON ANY SIDE
5. EXPOSED PAD SHALL BE SOLDER PLATED
6. SHADED AREA IS ONLY A REFERENCE FOR PIN 1 LOCATION ON THE TOP AND BOTTOM OF PACKAGE

## LTC5593

TYPICAL APPLICATIOी Extended frequency range 3.7 GHz to 4.5 GHz , low side $L 0, \mathrm{~V}_{\mathrm{Cc}}=3.3 \mathrm{~V}, \mathrm{~V}_{\text {ccIF }}=3.3 \mathrm{~V}$,
$E N A=$ high, $E N B=I_{S E L}=\operatorname{low}, \mathrm{T}_{\mathrm{C}}=25^{\circ} \mathrm{C}, \mathrm{P}_{\mathrm{LO}}=0 \mathrm{dBm}, \mathrm{P}_{\mathrm{RF}}=-3 \mathrm{dBm}(-3 \mathrm{dBm} /$ tone for 2-tone IIP3 Tests, $\Delta \mathrm{f}=2 \mathrm{MHz}), \mathrm{IF}=305 \mathrm{MHz}$


## RELATED PARTS

| PART NUMBER | DESCRIPTION | COMMENTS |
| :---: | :---: | :---: |
| Infrastructure |  |  |
| LTC5569 | 300MHz to 4GHz Dual Active Downconverting Mixer | 2dB Gain, 26.7dBm IIP3 and 11.7dB NF at 1950MHz, 3.3V/180mA Supply |
| LT5527 | 400MHz to 3.7GHz, 5V Downconverting Mixer | 2.3 dB Gain, 23.5dBm IIP3 and 12.5dB NF at 1900MHz, 5V/78mA Supply |
| LT5557 | 400MHz to 3.8GHz, 3.3V Downconverting Mixer | 2.9dB Gain, 24.7dBm IIP3 and 11.7dB NF at 1950MHz, 3.3V/82mA Supply |
| LTC6416 | 2GHz 16-Bit ADC Buffer | 40dBm OIP3 to 300MHz, Programmable Fast Recovery Output Clamping |
| LTC6412 | 31dB Linear Analog VGA | 35dBm OIP3 at 240MHz, Continuous Gain Range -14dB to 17dB |
| LTC554X | 600MHz to 4GHz Downconverting Mixer Family | 8dB Gain, >25dBm IIP3, 10dB NF, 3.3V/200mA Supply |
| LT5554 | Ultralow Distort IF Digital VGA | 48dBm OIP3 at 200MHz, 2dB to 18dB Gain Range, 0.125dB Gain Steps |
| LT5578 | 400MHz to 2.7GHz Upconverting Mixer | 27 dBm OIP3 at 900MHz, 24.2dBm at 1.95GHz, Integrated RF Transformer |
| LT5579 | 1.5GHz to 3.8 GHz Upconverting Mixer | 27.3 dBm OIP3 at 2.14GHz, NF = 9.9dB, 3.3V Supply, Single-Ended LO and RF Ports |
| LTC5590 | Dual 600MHz to 1.7GHz Downconverting Mixer | 8.7dB Gain, 26dBm IIP3, 9.7dB Noise Figure |
| LTC5591 | Dual 1.3GHz to 2.3GHz Downconverting Mixer | 8.5dB Gain, 26.2dBm IIP3, 9.9dB Noise Figure |
| LTC5592 | Dual 1.6GHz to 2.7GHz Downconverting Mixer | 8.3dB Gain, 27.3dBm IIP3, 9.8dB Noise Figure |

## RF Power Detectors

| LT5534 | 50MHz to 3GHz Log Detector | $\pm 1 \mathrm{~dB}$ over Temperature, 38ns Response Time, 60dB Dynamic Range |
| :--- | :--- | :--- |
| LT5581 | 6GHz Low Power RMS Detector | 40dB Dynamic Range, $\pm 1 \mathrm{~dB}$ Accuracy Over Temperature, 1.5mA Supply Current |
| LTC5583 | Dual 6GHz RMS Detector | Up to 60dB Dynamic Range, $>50 \mathrm{~dB}$ Isolation, Difference Output for <br> VSWR Measurement |


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| :--- | :--- | :--- |
| ADCs | 72.4dB SNR, >88dB SFDR, 790mW Power Consumption |  |
| LTC2285 | 14-Bit, 125Msps Dual ADC | 76.8 dB SNR, 185mW/Channel Power Consumption |
| LTC2185 | 16-Bit, 125Msps Dual ADC Ultralow Power | 65.4dB SNR, 78dB SFDR, 740mW Power Consumption |

