



### FEATURES

#### Rail-to-rail input/output

Low power: 0.625 mA typical per amplifier at  $\pm 15$  V

Gain bandwidth product: 15.9 MHz at  $A_v = 100$  typical

Unity-gain crossover: 9.9 MHz typical

-3 dB closed-loop bandwidth: 13.9 MHz typical at  $\pm 15$  V

Low offset voltage: 100  $\mu$ V maximum (SOIC)

Unity-gain stable

High slew rate: 4.6 V/ $\mu$ s typical

Low noise: 3.9 nV/ $\sqrt{\text{Hz}}$  typical at 1 kHz

Long-term offset voltage drift (10,000 hours): 3  $\mu$ V typical

Temperature hysteresis: 4  $\mu$ V typical

### APPLICATIONS

Battery-powered instrumentation

High-side and low-side sensing

Power supply control and protection

Telecommunications

Digital-to-analog converter (DAC) output amplifiers

Analog-to-digital converter (ADC) input buffers

### GENERAL DESCRIPTION

The ADA4084-1 (single), ADA4084-2 (dual), and ADA4084-4 (quad) are single-supply, 10 MHz bandwidth amplifiers featuring rail-to-rail inputs and outputs. They are guaranteed to operate from +3 V to +30 V (or  $\pm 1.5$  V to  $\pm 15$  V).

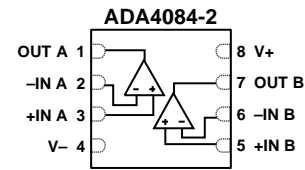
These amplifiers are well suited for single-supply applications requiring both ac and precision dc performance. The combination of wide bandwidth, low noise, and precision makes the ADA4084-1/ADA4084-2/ADA4084-4 useful in a wide variety of applications, including filters and instrumentation.

Other applications for these amplifiers include portable telecommunications equipment, power supply control and protection, and use as amplifiers or buffers for transducers with wide output ranges. Sensors requiring a rail-to-rail input amplifier include Hall effect, piezoelectric, and resistive transducers.

The ability to swing rail to rail at both the input and output enables designers to build multistage filters in single-supply systems and to maintain high signal-to-noise ratios.

The ADA4084-1/ADA4084-2/ADA4084-4 are specified over the industrial temperature range of  $-40^\circ\text{C}$  to  $+125^\circ\text{C}$ .

### PIN CONNECTION DIAGRAM



NOTES  
1. FOR THE LFCSP PACKAGE, THE EXPOSED PAD MUST BE CONNECTED TO V-.

08237-001

Figure 1. ADA4084-2, 8-Lead LFCSP (CP); for Additional Packages and Models, See the Pin Configurations and Function Descriptions Section

The single ADA4084-1 is available in the 5-lead SOT-23 and 8-lead SOIC; the dual ADA4084-2 is available in the 8-lead SOIC, 8-lead MSOP, and 8-lead LFCSP surface-mount packages; and the ADA4084-4 is offered in the 14-lead TSSOP and 16-lead LFCSP.

The ADA4084-1/ADA4084-2/ADA4084-4 are members of a growing series of high voltage, low noise op amps offered by Analog Devices, Inc. (see Table 1).

Table 1. Low Noise Op Amps

Single	Dual	Quad	Voltage Noise
AD8597	AD8599		1.1 nV/Hz
ADA4004-1	ADA4004-2	ADA4004-4	1.8 nV/Hz
AD8675	AD8676		2.8 nV/Hz rail-to-rail output
AD8671	AD8672	AD8674	2.8 nV/Hz
OP27, OP37			3.2 nV/Hz
ADA4084-1	ADA4084-2	ADA4084-4	3.9 nV/Hz rail-to-rail input/output

Rev. I

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**REVISION HISTORY**

**5/2017—Rev. H to Rev. I**

Changed CP-8-12 to CP-8-11 ..... Throughout  
 Changed CP-16-26 to CP-16-17 ..... Throughout  
 Changes to Features Section ..... 1  
 Added Long-Term Drift Section, Temperature Hysteresis Section, Figure 112, Figure 113, and Figure 114; Renumbered Sequentially ..... 32  
 Updated Outline Dimensions ..... 34  
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**8/2015—Rev. G to Rev. H**

Added 5-Lead SOT-23 ..... Universal  
 Changes to Pin Connection Diagram Section, Figure 1, and General Description Section ..... 1  
 Deleted Figure 3; Renumbered Sequentially ..... 1  
 Changes to Large Signal Voltage Gain Parameter, Table 2 ..... 4  
 Changes to Large Signal Voltage Gain Parameter, Table 3 ..... 5  
 Changes to Large Signal Voltage Gain Parameter, Table 4 ..... 6  
 Changes to Table 6 ..... 7  
 Moved Figure 3 ..... 8  
 Added Pin Configurations and Function Descriptions Section, Figure 4, Figure 5, Table 7, Table 8, and Table 9; Renumbered Sequentially ..... 8  
 Added Figure 6, Figure 7, Figure 8, Table 10, and Table 11 ..... 9  
 Moved Figure 9 ..... 10  
 Added Table 12 ..... 10  
 Added Figure 11 and Figure 15 ..... 11  
 Added Figure 42 and Figure 46 ..... 17  
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**6/2015—Rev. F to Rev. G**

Changes to Figure 96 and Figure 97 ..... 24

**1/2015—Rev. E to Rev. F**

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**7/2014—Rev. D to Rev. E**

Added ADA4084-1 ..... Universal  
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**11/2013—Rev. C to Rev. D**

Added 14-Lead TSSOP and 16-Lead LFCSP Packages..... Universal	
Added ADA4084-4..... Universal	
Change to Features Section and Applications Section .....	1
Added Figure 2 and Figure 3; Renumbered Sequentially .....	1
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**4/2013—Rev. B to Rev. C**

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**6/2012—Rev. A to Rev. B**

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**2/2012—Rev. 0 to Rev. A**

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**10/2011—Revision 0: Initial Version**

# SPECIFICATIONS

## ELECTRICAL CHARACTERISTICS

$V_{SY} = 3\text{ V}$ ,  $V_{CM} = 1.5\text{ V}$ ,  $T_A = 25^\circ\text{C}$ , unless otherwise noted.

Table 2.

Parameter	Symbol	Test Conditions/Comments	Min	Typ	Max	Unit
<b>INPUT CHARACTERISTICS</b>						
Offset Voltage	$V_{OS}$	SOIC package		20	100	$\mu\text{V}$
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$			200	$\mu\text{V}$
		SOT-23, MSOP, TSSOP packages		50	130	$\mu\text{V}$
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$			250	$\mu\text{V}$
		ADA4084-2 LFCSP package		80	200	$\mu\text{V}$
Offset Voltage Drift	$\Delta t/\Delta T$	$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$		0.5	1.75	$\mu\text{V}/^\circ\text{C}$
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$				300
Offset Voltage Matching		$T_A = 25^\circ\text{C}$			150	$\mu\text{V}$
Input Bias Current	$I_B$	ADA4084-4 LFCSP package			200	$\mu\text{V}$
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$		140	250	nA
Input Offset Current	$I_{OS}$	$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$			400	nA
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$		5	25	nA
Input Voltage Range	CMRR	$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$			50	nA
		$V_{CM} = 0\text{ V to }3\text{ V}$	0		3	V
Common-Mode Rejection Ratio	CMRR	$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	64	88		dB
		$R_L = 2\text{ k}\Omega$ , $0.5\text{ V} \leq V_{OUT} \leq 2.5\text{ V}$	60			dB
Large Signal Voltage Gain	$A_{VO}$	$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	100	104		dB
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	97			dB
Input Impedance		Differential		100  1.1		k $\Omega$   pF
		Common Mode		80  2.9		M $\Omega$   pF
<b>OUTPUT CHARACTERISTICS</b>						
Output Voltage High	$V_{OH}$	$R_L = 10\text{ k}\Omega$ to $V_{CM}$	2.90	2.95		V
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	2.80			V
		$R_L = 2\text{ k}\Omega$ to $V_{CM}$	2.85	2.9		V
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	2.70			V
Output Voltage Low	$V_{OL}$	$R_L = 10\text{ k}\Omega$ to $V_{CM}$		10	20	mV
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$			40	mV
		$R_L = 2\text{ k}\Omega$ to $V_{CM}$		20	30	mV
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$			50	mV
Short-Circuit Current	$I_{SC}$			-17/+10		mA
Closed-Loop Output Impedance	$Z_{OUT}$	$f = 1\text{ kHz}$ , $A_V = 1$		0.1		$\Omega$
<b>POWER SUPPLY</b>						
Power Supply Rejection Ratio	PSRR	$V_{SY} = \pm 1.25\text{ V to } \pm 1.75\text{ V}$	100	110		dB
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	90			dB
Supply Current per Amplifier	$I_{SY}$	$I_{OUT} = 0\text{ mA}$		0.565	0.650	mA
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$			0.950	mA
<b>DYNAMIC PERFORMANCE</b>						
Slew Rate	SR	$R_L = 2\text{ k}\Omega$	2.0	2.6		V/ $\mu\text{s}$
Gain Bandwidth Product	GBP	$V_{IN} = 5\text{ mV p-p}$ , $R_L = 10\text{ k}\Omega$ , $A_V = 100$		15.4		MHz
Unity-Gain Crossover	UGC	$V_{IN} = 5\text{ mV p-p}$ , $R_L = 10\text{ k}\Omega$ , $A_V = 1$		8.08		MHz
Phase Margin	$\Phi_M$			86		Degrees
-3 dB Closed-Loop Bandwidth	-3 dB	$A_V = 1$ , $V_{IN} = 5\text{ mV p-p}$		12.3		MHz
Settling Time	$t_s$	$A_V = 10$ , $V_{IN} = 2\text{ V p-p}$ , 0.1%		4		$\mu\text{s}$
Total Harmonic Distortion Plus Noise	THD + N	$V_{IN} = 300\text{ mV rms}$ , $R_L = 2\text{ k}\Omega$ , $f = 1\text{ kHz}$		0.009		%
<b>NOISE PERFORMANCE</b>						
Voltage Noise	$e_n$ p-p	0.1 Hz to 10 Hz		0.14		$\mu\text{V p-p}$
Voltage Noise Density	$e_n$	$f = 1\text{ kHz}$		3.9		nV/ $\sqrt{\text{Hz}}$
Current Noise Density	$i_n$	$f = 1\text{ kHz}$		0.55		pA/ $\sqrt{\text{Hz}}$

$V_{SY} = \pm 5.0\text{ V}$ ,  $V_{CM} = 0\text{ V}$ ,  $T_A = 25^\circ\text{C}$ , unless otherwise noted.

Table 3.

Parameter	Symbol	Test Conditions/Comments	Min	Typ	Max	Unit	
INPUT CHARACTERISTICS							
Offset Voltage	$V_{OS}$	SOIC package		30	100	$\mu\text{V}$	
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$			200	$\mu\text{V}$	
		SOT-23, MSOP, TSSOP packages		60	130	$\mu\text{V}$	
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$			250	$\mu\text{V}$	
		ADA4084-2 LFCSP package		90	200	$\mu\text{V}$	
Offset Voltage Drift	$\Delta V_{OS}/\Delta T$	$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$		0.5	1.75	$\mu\text{V}/^\circ\text{C}$	
		$T_A = 25^\circ\text{C}$			150	$\mu\text{V}$	
Offset Voltage Matching		ADA4084-4 LFCSP package			200	$\mu\text{V}$	
Input Bias Current	$I_B$	$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$		140	250	nA	
Input Offset Current	$I_{OS}$	$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$		5	25	nA	
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$			50	nA	
Input Voltage Range			-5		+5	V	
Common-Mode Rejection Ratio	CMRR	$V_{CM} = \pm 4\text{ V}$ , $-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	106	124		dB	
		$V_{CM} = \pm 5\text{ V}$				76	dB
		$V_{CM} = \pm 5\text{ V}$ , $-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$				70	dB
Large Signal Voltage Gain	$A_{VO}$	$R_L = 2\text{ k}\Omega$ , $-4\text{ V} \leq V_{OUT} \leq 4\text{ V}$	108	112		dB	
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$				103	dB
Input Impedance							
Differential				100  1.1		k $\Omega$   pF	
Common Mode				200  2.5		M $\Omega$   pF	
OUTPUT CHARACTERISTICS							
Output Voltage High	$V_{OH}$	$R_L = 10\text{ k}\Omega$ to $V_{CM}$	4.9	4.95		V	
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$				4.8	V
		$R_L = 2\text{ k}\Omega$ to $V_{CM}$	4.8	4.85			V
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$				4.7	V
Output Voltage Low	$V_{OL}$	$R_L = 10\text{ k}\Omega$ to $V_{CM}$		-4.95	-4.9	V	
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$				-4.8	V
		$R_L = 2\text{ k}\Omega$ to $V_{CM}$		-4.95	-4.8		V
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$				-4.7	V
Short-Circuit Current	$I_{SC}$		-24/+17			mA	
Closed-Loop Output Impedance	$Z_{OUT}$	$f = 1\text{ kHz}$ , $A_V = 1$		0.1		$\Omega$	
POWER SUPPLY							
Power Supply Rejection Ratio	PSRR	$V_{SY} = \pm 2\text{ V}$ to $\pm 18\text{ V}$	110	120		dB	
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$				105	dB
Supply Current per Amplifier	$I_{SY}$	$I_{OUT} = 0\text{ mA}$		0.595	0.700	mA	
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$			1.00	mA	
DYNAMIC PERFORMANCE							
Slew Rate	SR	$R_L = 2\text{ k}\Omega$ to $V_{CM}$	2.4	3.7		V/ $\mu\text{s}$	
Gain Bandwidth Product	GBP	$V_{IN} = 5\text{ mV p-p}$ , $R_L = 10\text{ k}\Omega$ , $A_V = 100$		15.9		MHz	
Unity-Gain Crossover	UGC	$V_{IN} = 5\text{ mV p-p}$ , $R_L = 10\text{ k}\Omega$ , $A_V = 1$		9.6		MHz	
Phase Margin	$\Phi_M$			85		Degrees	
-3 dB Closed-Loop Bandwidth	-3 dB	$A_V = 1$ , $V_{IN} = 5\text{ mV p-p}$		13.9		MHz	
Settling Time	$t_s$	$A_V = 10$ , $V_{IN} = 8\text{ V p-p}$ , 0.1%		4		$\mu\text{s}$	
Total Harmonic Distortion Plus Noise	THD + N	$V_{IN} = 2\text{ V rms}$ , $R_L = 2\text{ k}\Omega$ , $f = 1\text{ kHz}$		0.003		%	
NOISE PERFORMANCE							
Voltage Noise	$e_n$ p-p	0.1 Hz to 10 Hz		0.14		$\mu\text{V p-p}$	
Voltage Noise Density	$e_n$	$f = 1\text{ kHz}$		3.9		nV/ $\sqrt{\text{Hz}}$	
Current Noise Density	$i_n$	$f = 1\text{ kHz}$		0.55		pA/ $\sqrt{\text{Hz}}$	

$V_{SY} = \pm 15.0\text{ V}$ ,  $V_{CM} = 0\text{ V}$ ,  $T_A = 25^\circ\text{C}$ , unless otherwise noted.

Table 4.

Parameter	Symbol	Test Conditions/Comments	Min	Typ	Max	Unit
<b>INPUT CHARACTERISTICS</b>						
Offset Voltage	$V_{OS}$	SOIC package		40	100	$\mu\text{V}$
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$			200	$\mu\text{V}$
		SOT-23, MSOP, TSSOP packages		70	130	$\mu\text{V}$
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$			250	$\mu\text{V}$
		ADA4084-2 LFCSP package		100	200	$\mu\text{V}$
Offset Voltage Drift	$\Delta V_{OS}/\Delta T$	$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$		0.5	1.75	$\mu\text{V}/^\circ\text{C}$
Offset Voltage Matching		$T_A = 25^\circ\text{C}$			150	$\mu\text{V}$
Input Bias Current	$I_B$	ADA4084-4 LFCSP package		140	250	$\text{nA}$
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$			400	$\text{nA}$
Input Offset Current	$I_{OS}$	$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$		5	25	$\text{nA}$
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$			50	$\text{nA}$
Input Voltage Range			-15		+15	$\text{V}$
Common-Mode Rejection Ratio	CMRR	$V_{CM} = \pm 14\text{ V}$ , $-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	106	124		$\text{dB}$
		$V_{CM} = \pm 15\text{ V}$	85			$\text{dB}$
		$V_{CM} = \pm 15\text{ V}$ , $-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	80			$\text{dB}$
Large Signal Voltage Gain	$A_{VO}$	$R_L = 2\text{ k}\Omega$ , $-13.5\text{ V} \leq V_{OUT} \leq +13.5\text{ V}$	110	117		$\text{dB}$
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	105			$\text{dB}$
Input Impedance				100  1.1		$\text{k}\Omega  \text{pF}$
				200  2.5		$\text{M}\Omega  \text{pF}$
<b>OUTPUT CHARACTERISTICS</b>						
Output Voltage High	$V_{OH}$	$R_L = 10\text{ k}\Omega$ to $V_{CM}$	14.85	14.9		$\text{V}$
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	14.8			$\text{V}$
		$R_L = 2\text{ k}\Omega$ to $V_{CM}$	14.5	14.6		$\text{V}$
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	14.0			$\text{V}$
Output Voltage Low	$V_{OL}$	$R_L = 10\text{ k}\Omega$ to $V_{CM}$		-14.95	-14.9	$\text{V}$
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$			-14.8	$\text{V}$
		$R_L = 2\text{ k}\Omega$ to $V_{CM}$		-14.9	-14.8	$\text{V}$
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$			-14.7	$\text{V}$
Short-Circuit Current	$I_{SC}$		$\pm 30$			$\text{mA}$
Closed-Loop Output Impedance	$Z_{OUT}$	$f = 1\text{ kHz}$ , $A_V = +1$		0.1		$\Omega$
<b>POWER SUPPLY</b>						
Power Supply Rejection Ratio	PSRR	$V_{SY} = \pm 2\text{ V}$ to $\pm 18\text{ V}$	110	120		$\text{dB}$
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$	105			$\text{dB}$
Supply Current per Amplifier	$I_{SY}$	$I_{OUT} = 0\text{ mA}$		0.625	0.750	$\text{mA}$
		$-40^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$			1.050	$\text{mA}$
<b>DYNAMIC PERFORMANCE</b>						
Slew Rate	SR	$R_L = 2\text{ k}\Omega$	2.4	4.6		$\text{V}/\mu\text{s}$
Gain Bandwidth Product	GBP	$V_{IN} = 5\text{ mV p-p}$ , $R_L = 10\text{ k}\Omega$ , $A_V = 100$		15.9		$\text{MHz}$
Unity-Gain Crossover	UGC	$V_{IN} = 5\text{ mV p-p}$ , $R_L = 10\text{ k}\Omega$ , $A_V = 1$		9.9		$\text{MHz}$
Phase Margin	$\Phi_M$			86		Degrees
-3 dB Closed-Loop Bandwidth	-3 dB	$A_V = 1$ , $V_{IN} = 5\text{ mV p-p}$		13.9		$\text{MHz}$
Settling Time	$t_S$	$A_V = 10$ , $V_{IN} = 10\text{ V p-p}$ , 0.1%		4		$\mu\text{s}$
Total Harmonic Distortion Plus Noise	THD + N	$V_{IN} = 5\text{ V rms}$ , $R_L = 2\text{ k}\Omega$ , $f = 1\text{ kHz}$		0.003		%
<b>NOISE PERFORMANCE</b>						
Voltage Noise	$e_n$ p-p	0.1 Hz to 10 Hz		0.1		$\mu\text{V p-p}$
Voltage Noise Density	$e_n$	$f = 1\text{ kHz}$		3.9		$\text{nV}/\sqrt{\text{Hz}}$
Current Noise Density	$i_n$	$f = 1\text{ kHz}$		0.55		$\text{pA}/\sqrt{\text{Hz}}$

## ABSOLUTE MAXIMUM RATINGS

Table 5.

Parameter	Rating
Supply Voltage	±18 V
Input Voltage	$V- \leq V_{IN} \leq V+$
Differential Input Voltage <sup>1</sup>	±0.6 V
Output Short-Circuit Duration to GND	Indefinite
Storage Temperature Range	-65°C to +150°C
Operating Temperature Range	-40°C to +125°C
Junction Temperature Range	-65°C to +150°C
Lead Temperature (Soldering 60 sec)	300°C
ESD	
Human Body Model <sup>2</sup>	4.5 kV
Machine Model <sup>3</sup>	200 V
Field-Induced Charged-Device Model (FICDM) <sup>4</sup>	1.25 kV

<sup>1</sup> For input differential voltages greater than 0.6 V, limit the input current to less than 5 mA to prevent degradation or destruction of the input devices.

<sup>2</sup> Applicable standard: MIL-STD-883, Method 3015.7.

<sup>3</sup> Applicable standard: JESD22-A115-A (ESD machine model standard of JEDEC).

<sup>4</sup> Applicable standard: JESD22-C101-C (ESD FICDM standard of JEDEC).

Stresses at or above those listed under Absolute Maximum Ratings may cause permanent damage to the product. This is a stress rating only; functional operation of the product at these or any other conditions above those indicated in the operational section of this specification is not implied. Operation beyond the maximum operating conditions for extended periods may affect product reliability.

## THERMAL RESISTANCE

$\theta_{JA}$  is specified for the device soldered on a 4-layer JEDEC standard printed circuit board (PCB) with zero airflow.

Table 6. Thermal Resistance

Package Type	$\theta_{JA}$	$\theta_{JC}$	Unit
5-Lead SOT-23 (RJ-5)	219.4	155.6	°C/W
8-Lead SOIC_N (R-8)	121	43	°C/W
8-Lead MSOP (RM-8)	142	45	°C/W
8-Lead LFCSP (CP-8-11) <sup>1,3</sup>	84	40	°C/W
14-Lead TSSOP (RU-14)	112	43	°C/W
16-Lead LFCSP (CP-16-17) <sup>2,3</sup>	55	30	°C/W

<sup>1</sup> Values are based on 4-layer (252P) JEDEC standard PCB, with four thermal vias. Exposed pad soldered to PCB.

<sup>2</sup> Values are based on 4-layer (252P) JEDEC standard PCB, with nine thermal vias. Exposed pad soldered to PCB.

<sup>3</sup>  $\theta_{JC}$  measured on top of package.

## ESD CAUTION



### ESD (electrostatic discharge) sensitive device.

Charged devices and circuit boards can discharge without detection. Although this product features patented or proprietary protection circuitry, damage may occur on devices subjected to high energy ESD. Therefore, proper ESD precautions should be taken to avoid performance degradation or loss of functionality.

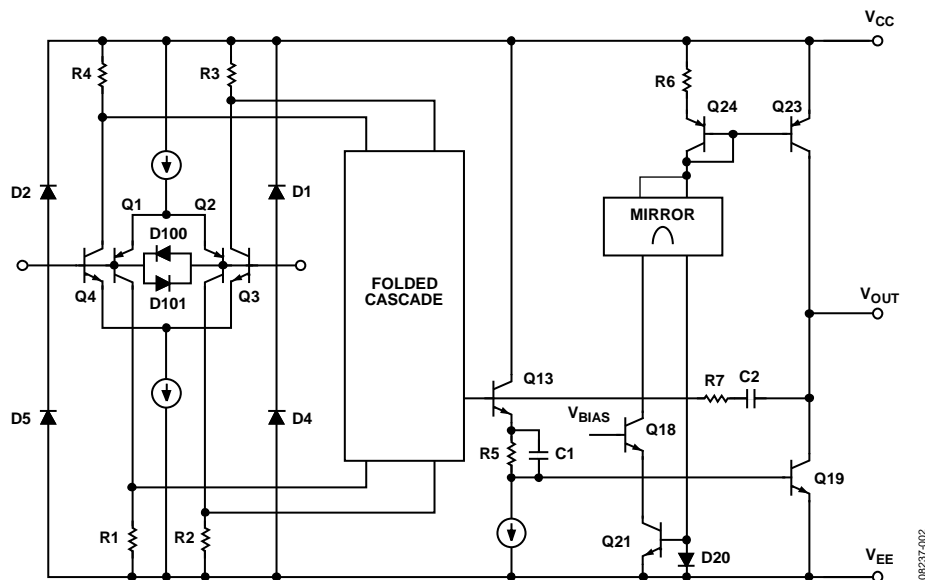


Figure 2. Simplified Schematic

## PIN CONFIGURATIONS AND FUNCTION DESCRIPTIONS

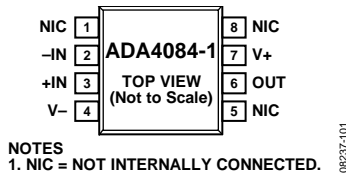


Figure 3. ADA4084-1, 8-Lead SOIC (R)

Table 7. 8-Lead SOIC, ADA4084-1 Pin Function Descriptions

Pin No.	Mnemonic	Description
1	NIC	Not Internally Connected
2	-IN	Negative Input
3	+IN	Positive Input
4	V-	Negative Supply
5	NIC	Not Internally Connected
6	OUT	Output
7	V+	Positive Supply
8	NIC	Not Internally Connected

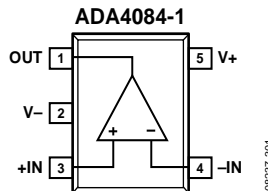


Figure 4. ADA4084-1, 5-Lead SOT-23 (RJ)

Table 8. 5-Lead SOT-23, ADA4084-1 Pin Function Descriptions

Pin No.	Mnemonic	Description
1	OUT	Output
2	V-	Negative Supply
3	+IN	Positive Input
4	-IN	Negative Input
5	V+	Positive Supply

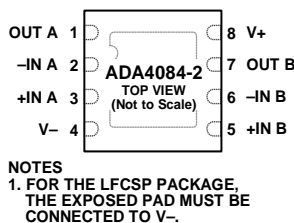


Figure 5. ADA4084-2, 8-Lead LFCSP (CP)

Table 9. 8-Lead LFCSP, ADA4084-2 Pin Function Descriptions

Pin No.	Mnemonic	Description
1	OUT A	Output, Channel A
2	-IN A	Negative Input, Channel A
3	+IN A	Positive Input, Channel A
4	V-	Negative Supply
5	+IN B	Positive Input, Channel B
6	-IN B	Negative Input, Channel B
7	OUT B	Output, Channel B
8	V+	Positive Supply
	EPAD	Exposed Pad. For the LFCSP package, the exposed pad must be connected to V-.



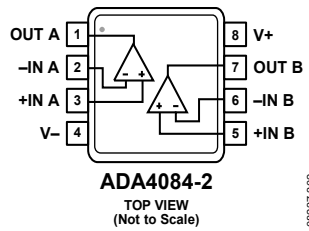


Figure 6. ADA4084-2, 8-Lead MSOP (RM)

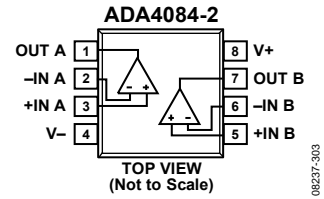


Figure 7. ADA4084-2, 8-Lead SOIC (R)

Table 10. 8-Lead MSOP, 8-Lead SOIC, ADA4084-2 Pin Function Descriptions

Pin No.	Mnemonic	Description
1	OUT A	Output, Channel A
2	-IN A	Negative Input, Channel A
3	+IN A	Positive Input, Channel A
4	V-	Negative Supply
5	+IN B	Positive Input, Channel B
6	-IN B	Negative Input, Channel B
7	OUT B	Output, Channel B
8	V+	Positive Supply B

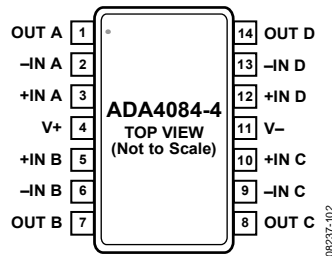
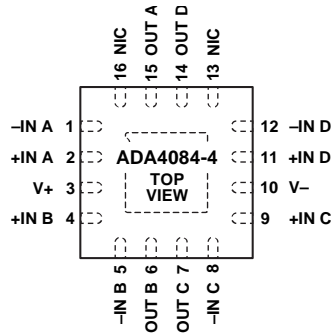


Figure 8. ADA4084-4, 14-Lead TSSOP (RU)

Table 11. 14-Lead TSSOP, ADA4804-4 Pin Function Descriptions

Pin No.	Mnemonic	Description
1	OUT A	Output, Channel A
2	-IN A	Negative Input, Channel A
3	+IN A	Positive Input, Channel A
4	V+	Positive Supply
5	+IN B	Positive Input, Channel B
6	-IN B	Negative Input, Channel B
7	OUT B	Output, Channel B
8	OUT C	Output, Channel C
9	-IN C	Negative Input, Channel C
10	+IN C	Positive Input, Channel C
11	V-	Negative Supply
12	+IN D	Positive Input, Channel D
13	-IN D	Negative Input, Channel D
14	OUT D	Output, Channel D



**NOTES**  
 1. NIC = NOT INTERNALLY CONNECTED.  
 2. FOR THE LFCSP PACKAGE, THE EXPOSED PAD MUST BE CONNECTED TO V-.

08237r-03

Figure 9. ADA4084-4, 16-Lead LFCSP (CP)

Table 12. 16-Lead LFCSP, ADA4084-4 Pin Function Descriptions

Pin No.	Mnemonic	Description
1	-IN A	Negative Input Channel A
2	+IN A	Positive Input, Channel A
3	V+	Positive Supply
4	+IN B	Positive Input, Channel B
5	-IN B	Negative Input, Channel B
6	OUT B	Output, Channel B
7	OUT C	Output, Channel C
8	-IN C	Negative Input, Channel C
9	+IN C	Positive Input, Channel C
10	V-	Negative Supply
11	+IN D	Positive Input, Channel D
12	-IN D	Negative Input, Channel D
13	NIC	Not Internally Connected
14	OUT D	Output, Channel D
15	OUT A	Output, Channel A
16	NIC	Not Internally Connected

# TYPICAL PERFORMANCE CHARACTERISTICS

$T_A = 25^\circ\text{C}$ , unless otherwise noted.

## $\pm 1.5\text{ V}$ CHARACTERISTICS

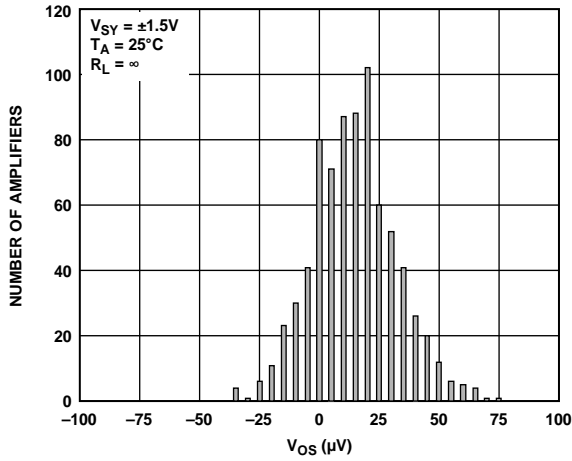


Figure 10. Input Offset Voltage ( $V_{os}$ ) Distribution, SOIC

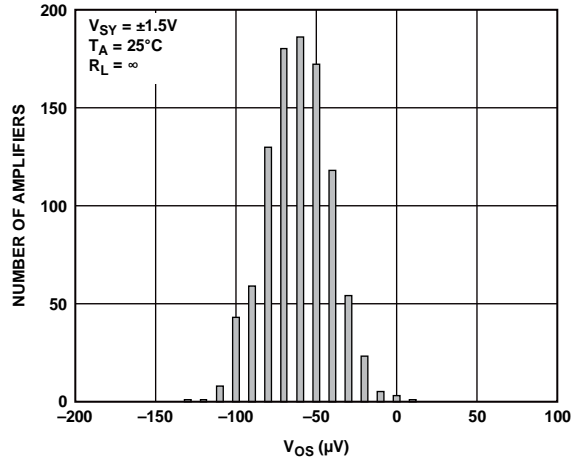


Figure 13. Input Offset Voltage ( $V_{os}$ ) Distribution, LFCSP

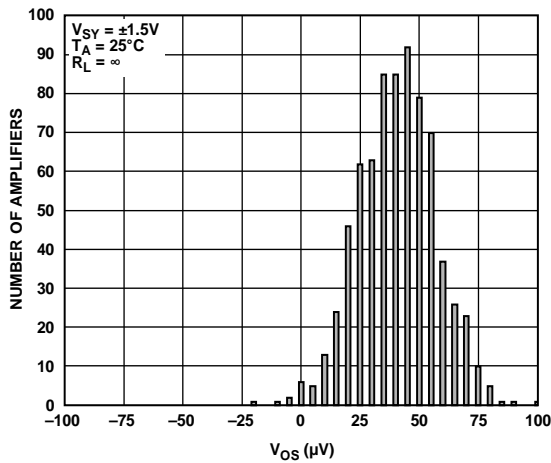


Figure 11. Input Offset Voltage ( $V_{os}$ ) Distribution, SOT-23

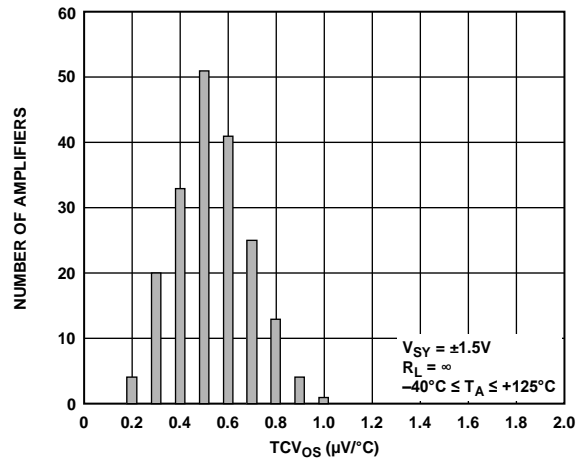


Figure 14.  $TCV_{os}$  Distribution, SOIC, MSOP, and TSSOP

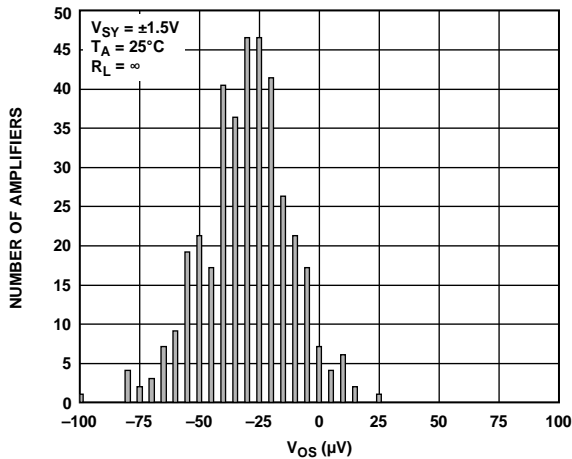


Figure 12. Input Offset Voltage ( $V_{os}$ ) Distribution, MSOP and TSSOP

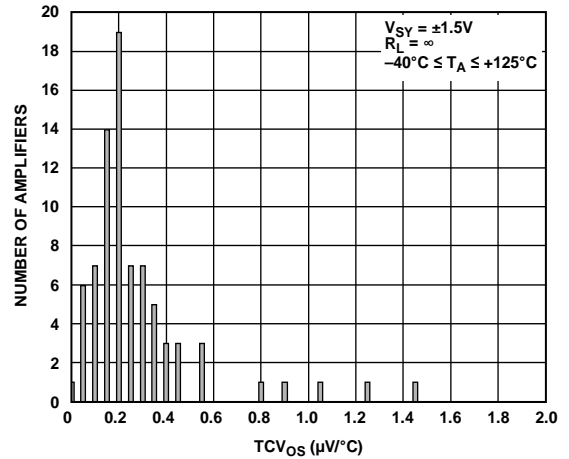


Figure 15.  $TCV_{os}$  Distribution, SOT-23

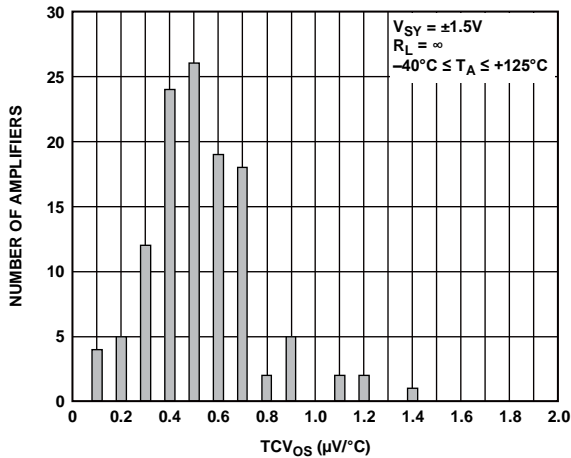


Figure 16.  $TCV_{OS}$  Distribution, LFCSP

08237-082

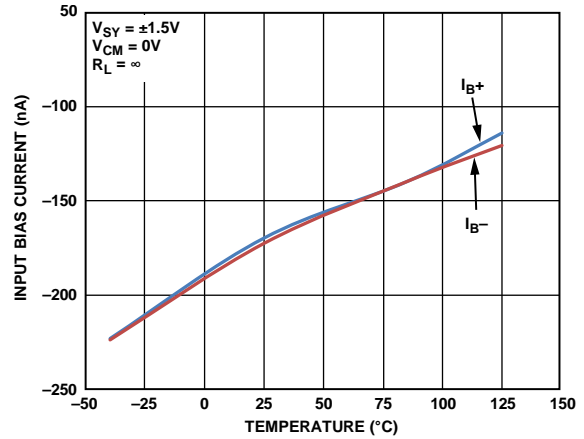


Figure 19. Input Bias Current vs. Temperature

08237-213

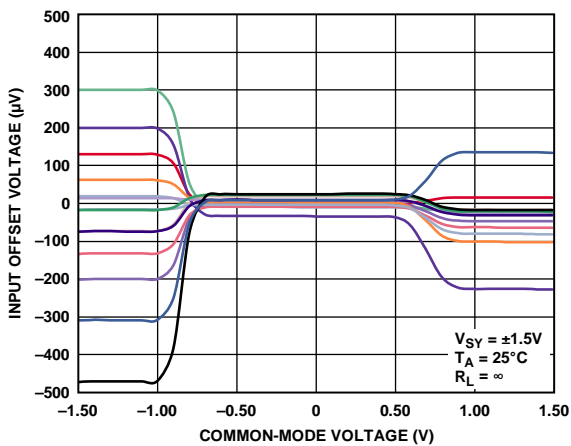


Figure 17. Input Offset Voltage vs. Common-Mode Voltage

08237-506

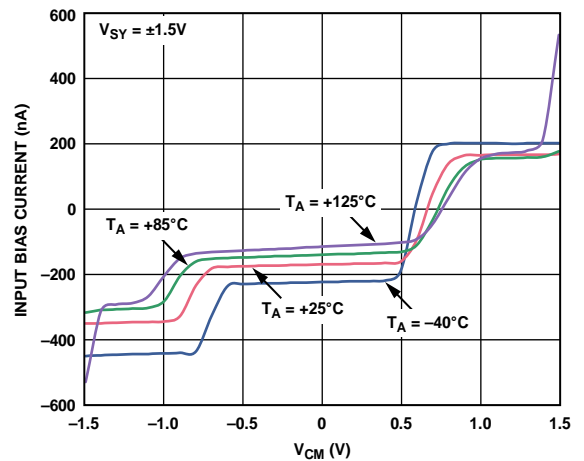


Figure 20. Input Bias Current vs.  $V_{CM}$  for Various Temperatures

08237-008

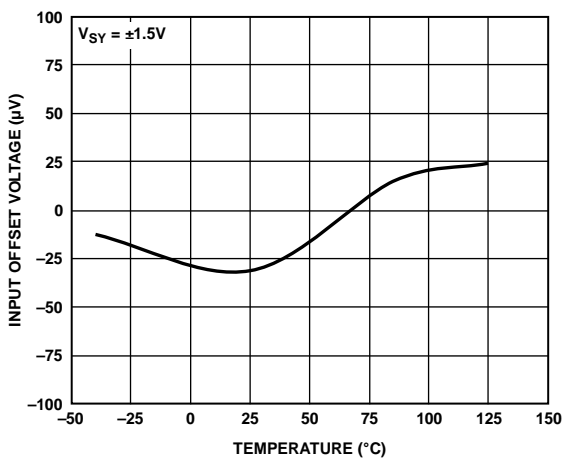


Figure 18. Input Offset Voltage vs. Temperature

08237-108

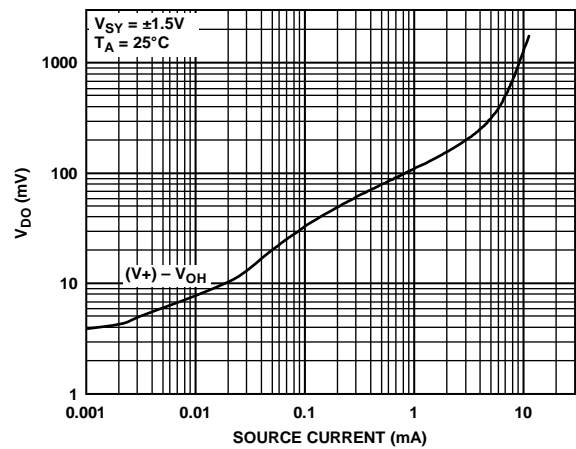


Figure 21. Dropout Voltage ( $V_{DO}$ ) vs. Source Current

08237-509

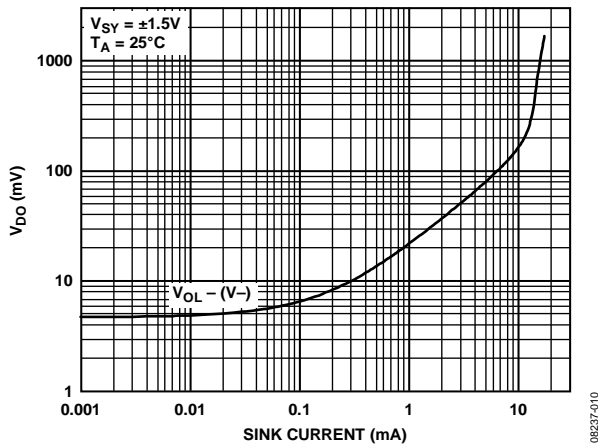


Figure 22. Dropout Voltage ( $V_{Do}$ ) vs. Sink Current

08237-010

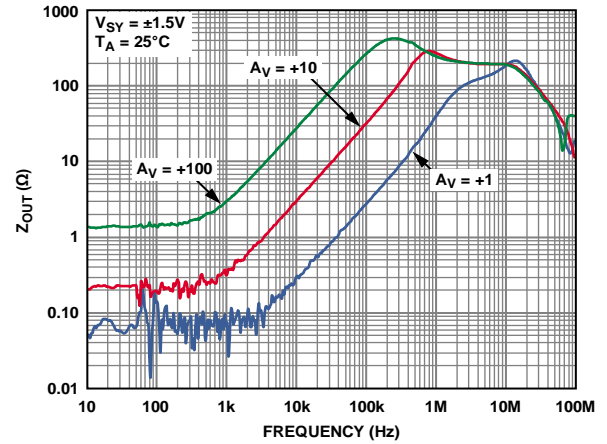


Figure 25. Output Impedance ( $Z_{OUT}$ ) vs. Frequency

08237-013

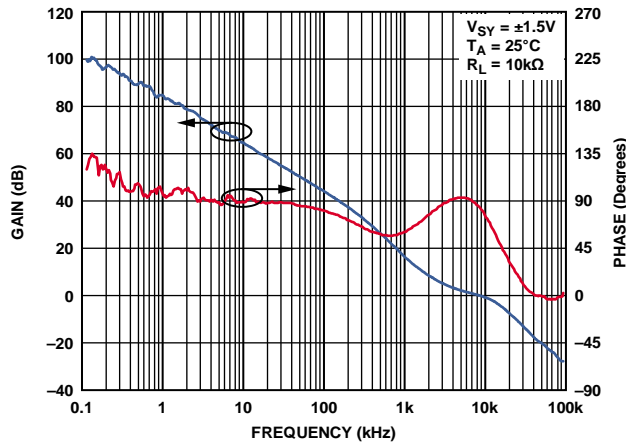


Figure 23. Open-Loop Gain and Phase vs. Frequency

08237-011

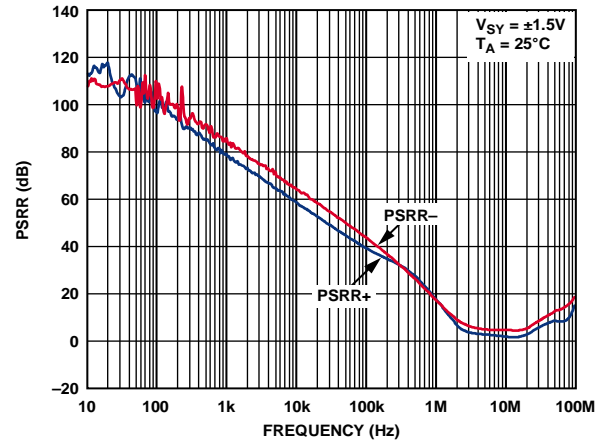


Figure 26. PSRR vs. Frequency

08237-014

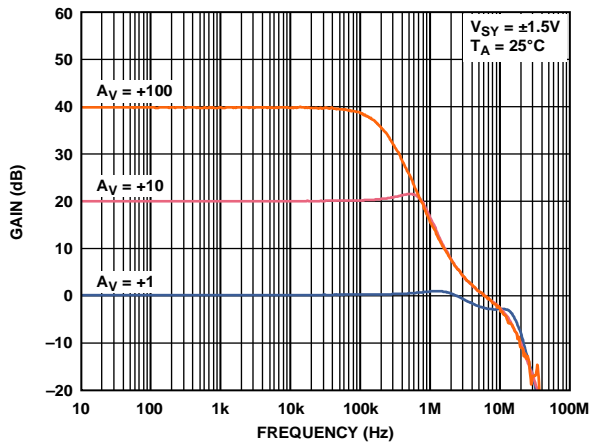


Figure 24. Closed-Loop Gain vs. Frequency

08237-012

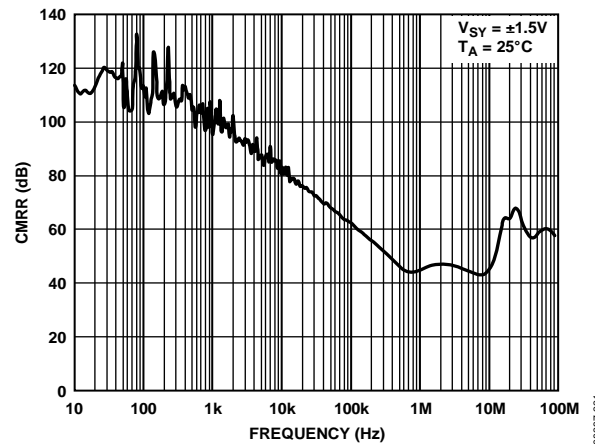


Figure 27. CMRR vs. Frequency

08237-221

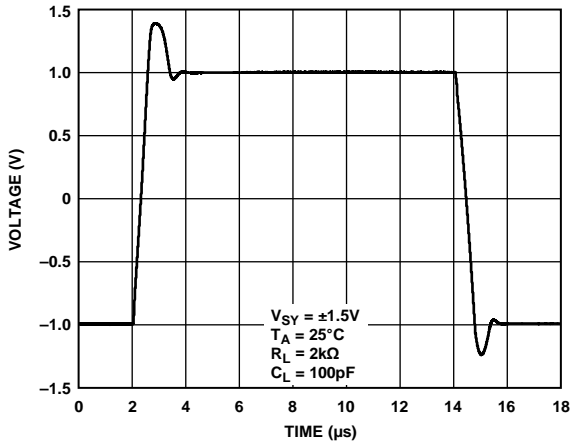


Figure 28. Large Signal Transient Response

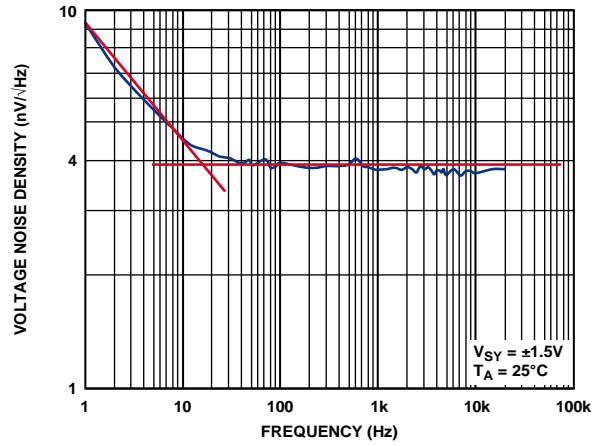


Figure 31. Voltage Noise Density vs. Frequency

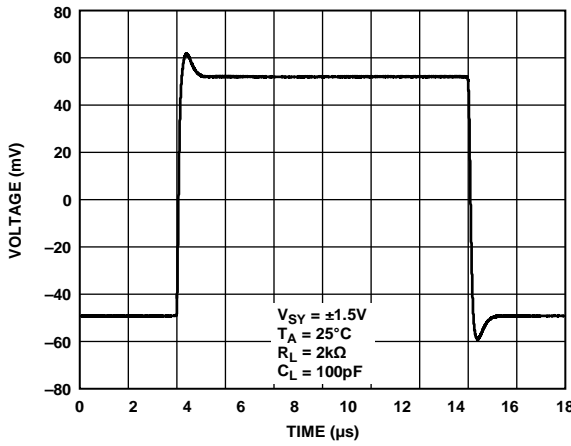


Figure 29. Small Signal Transient Response

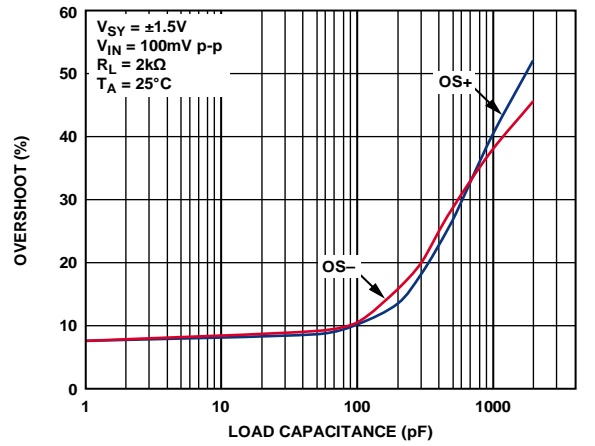


Figure 32. Overshoot vs. Load Capacitance

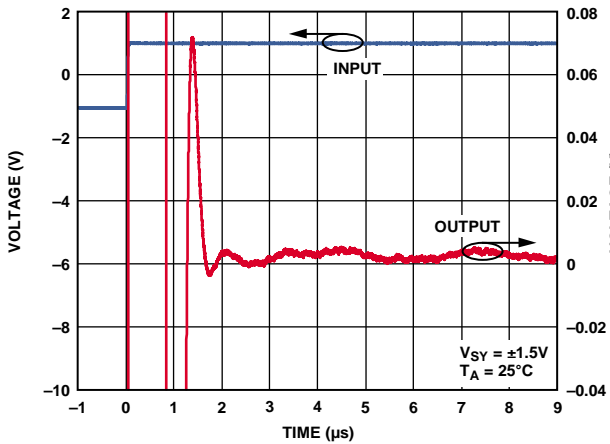


Figure 30. Settling Time

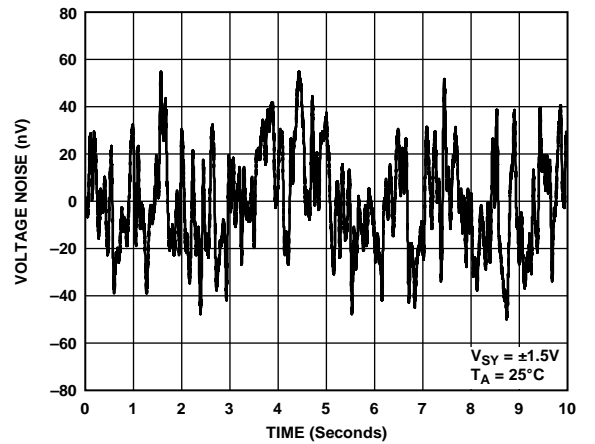


Figure 33. Voltage Noise, 0.1 Hz to 10 Hz

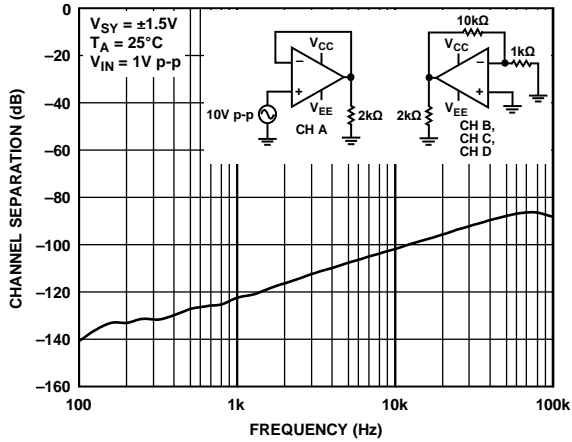


Figure 34. Channel Separation vs. Frequency

08237-022

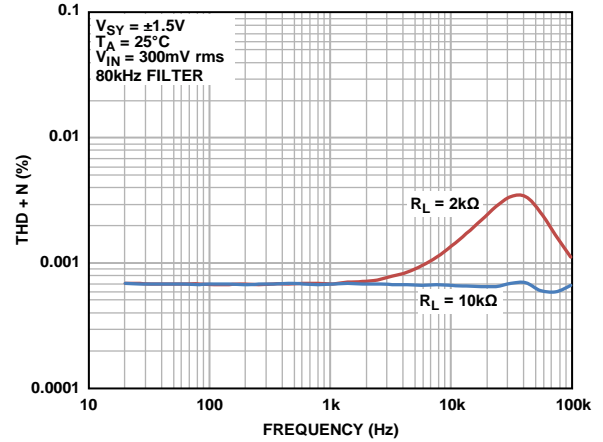


Figure 37. THD + N vs. Frequency, 80 kHz Filter

08237-231

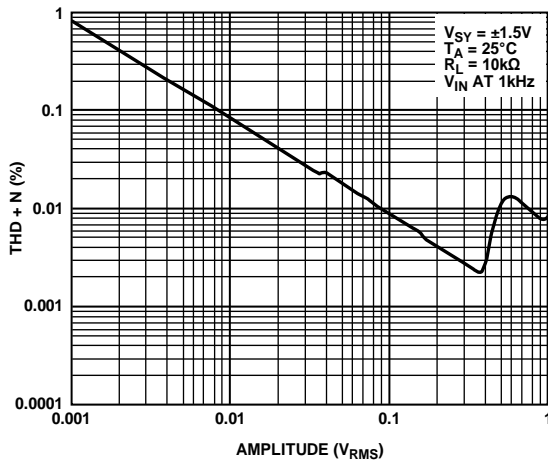


Figure 35. THD + N vs. Amplitude

08237-125

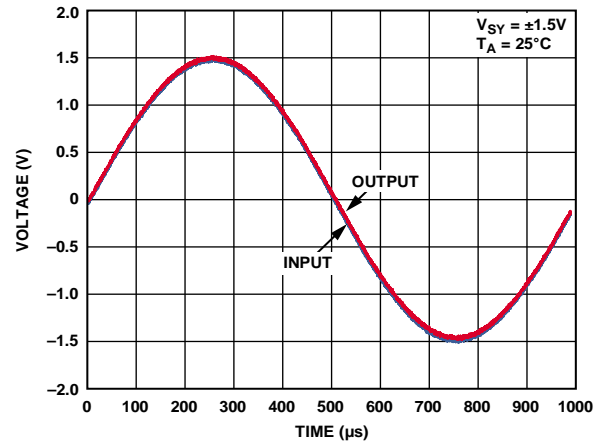


Figure 38. No Phase Reversal

08237-025

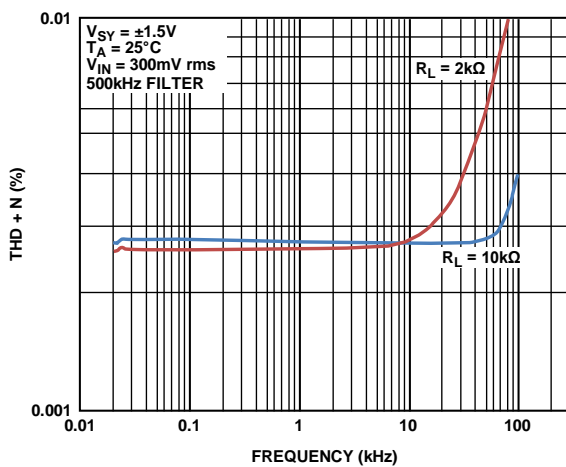


Figure 36. THD + N vs. Frequency, 500 kHz Filter

08237-126

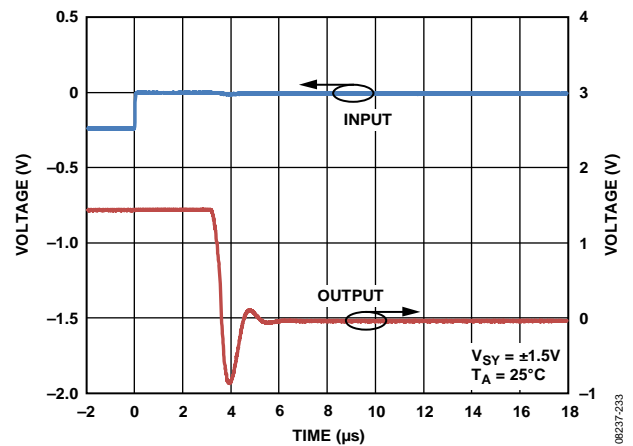


Figure 39. Positive 50% Overload Recovery

08237-233

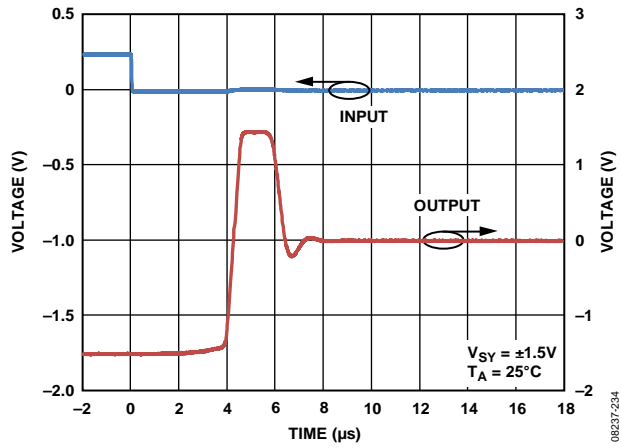


Figure 40. Negative 50% Overload Recovery



**±5 V CHARACTERISTICS**

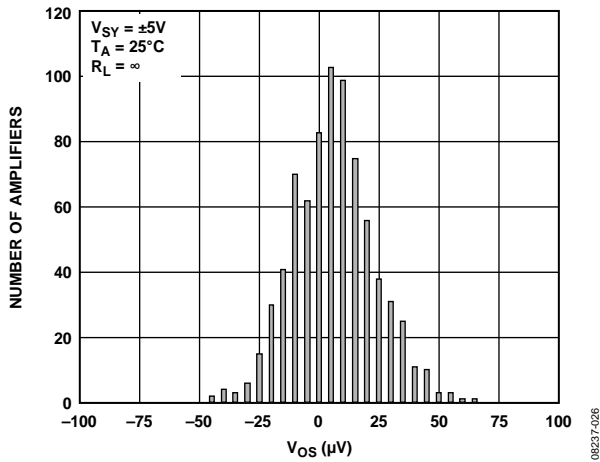


Figure 41. Input Offset Voltage ( $V_{OS}$ ) Distribution, SOIC

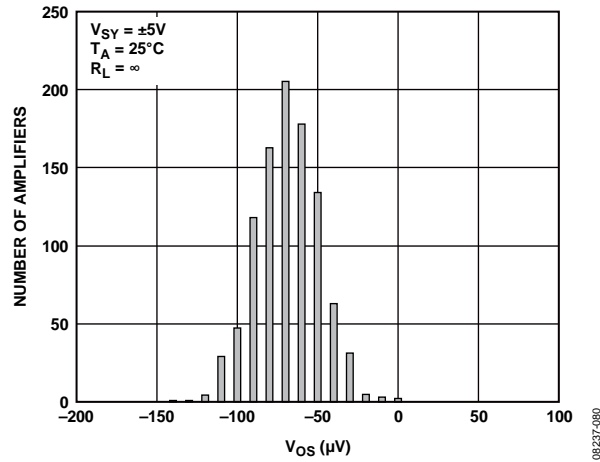


Figure 44. Input Offset Voltage ( $V_{OS}$ ) Distribution, LFCSP

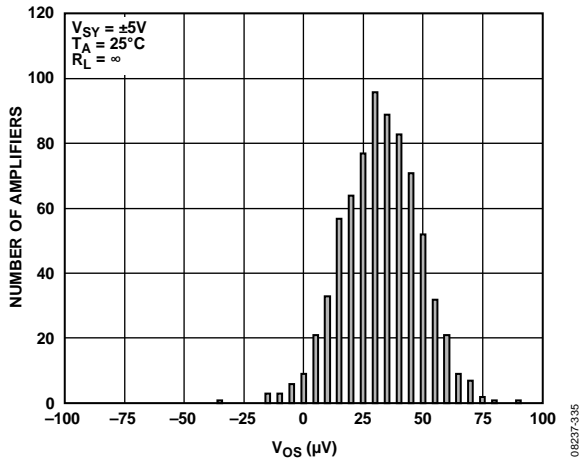


Figure 42. Input Offset Voltage ( $V_{OS}$ ) Distribution, SOT-23

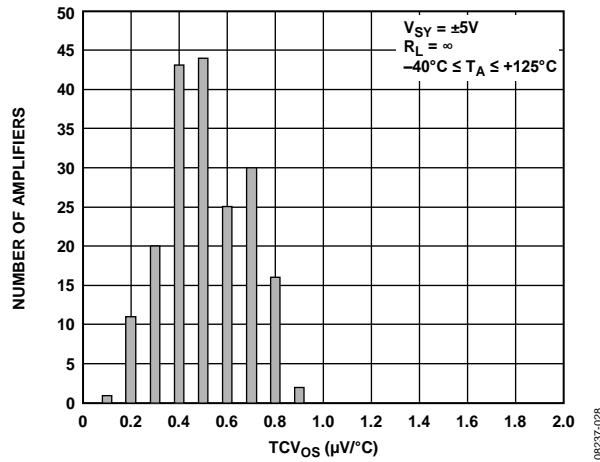


Figure 45.  $TCV_{OS}$  Distribution, SOIC, MSOP, and TSSOP

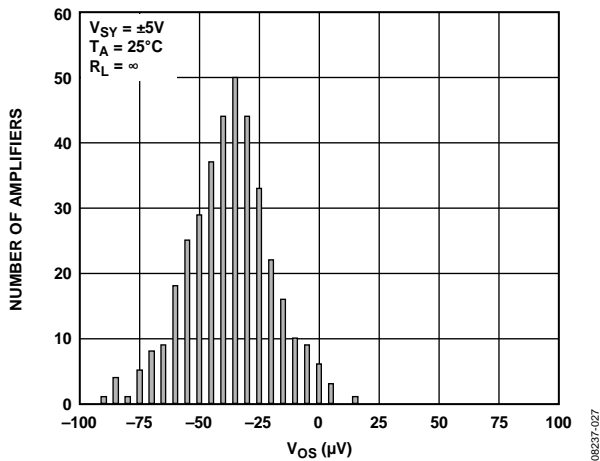


Figure 43. Input Offset Voltage ( $V_{OS}$ ) Distribution, MSOP and TSSOP

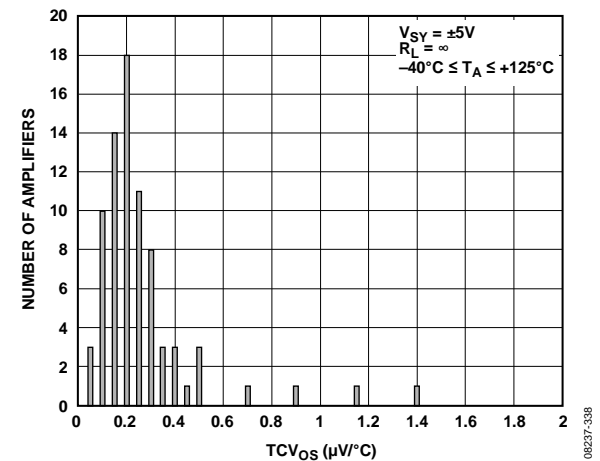


Figure 46.  $TCV_{OS}$  Distribution for SOT-23

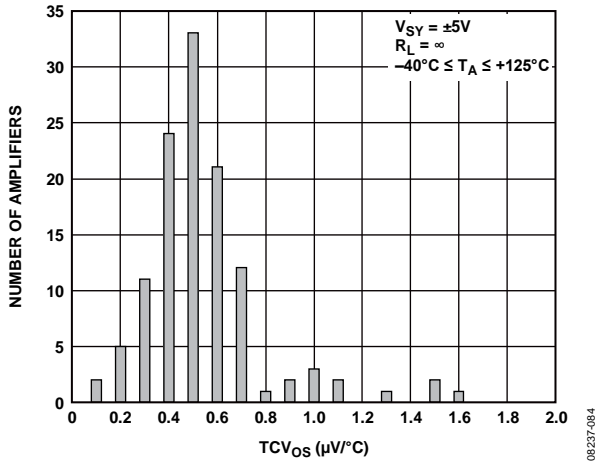


Figure 47.  $TCV_{0S}$  Distribution, LFCSP

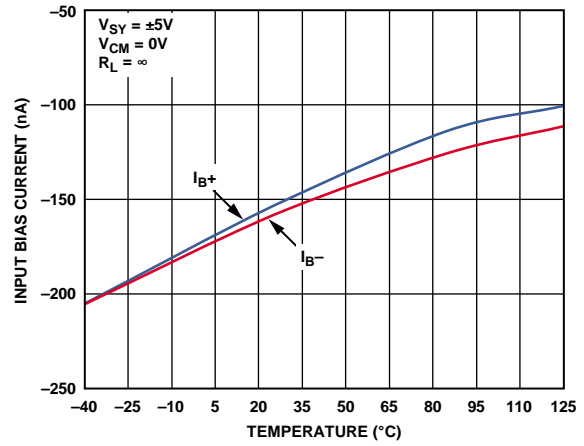


Figure 50. Input Bias Current vs. Temperature

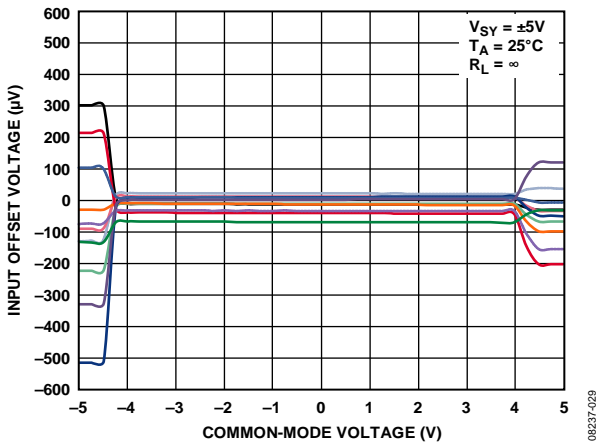


Figure 48. Input Offset Voltage vs. Common-Mode Voltage

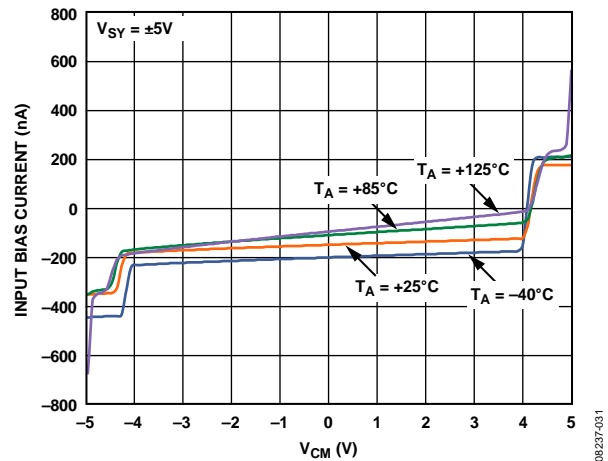


Figure 51. Input Bias Current vs.  $V_{CM}$  for Various Temperatures

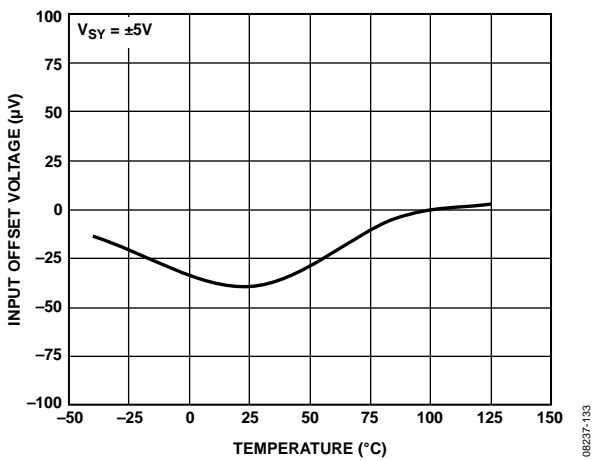


Figure 49. Input Offset Voltage vs. Temperature

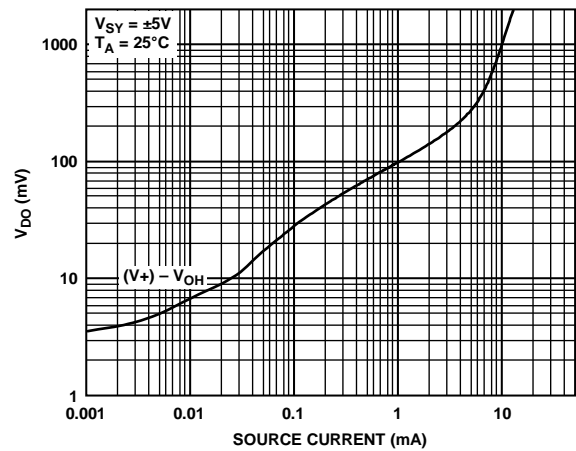


Figure 52. Dropout Voltage ( $V_{DO}$ ) vs. Source Current

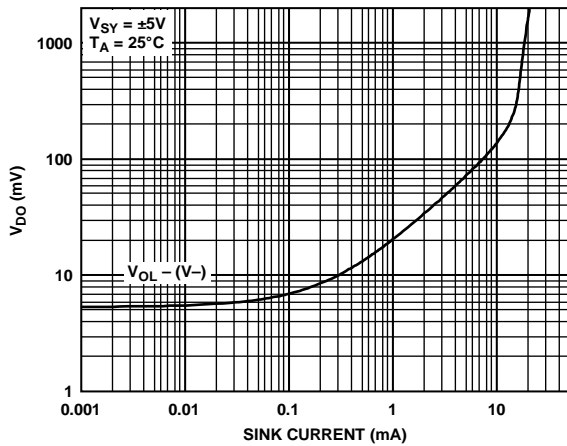


Figure 53. Dropout Voltage ( $V_{Do}$ ) vs. Sink Current

08237-033

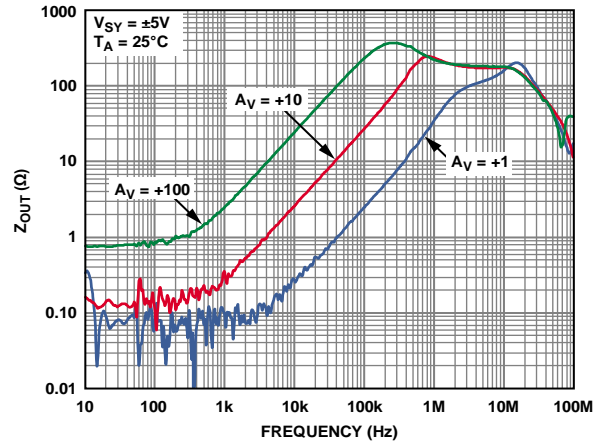


Figure 56. Output Impedance ( $Z_{OUT}$ ) vs. Frequency

08237-036

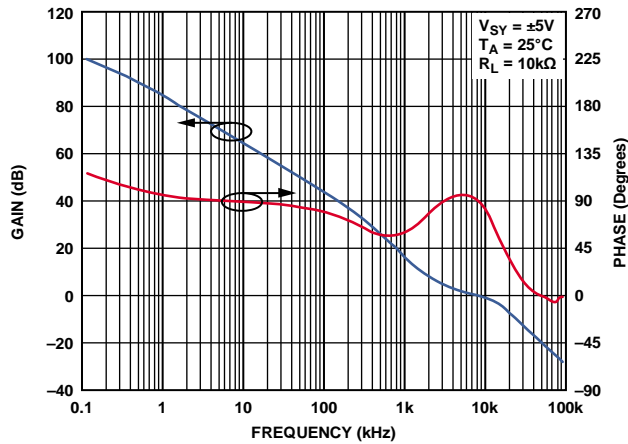


Figure 54. Open-Loop Gain and Phase vs. Frequency

08237-034

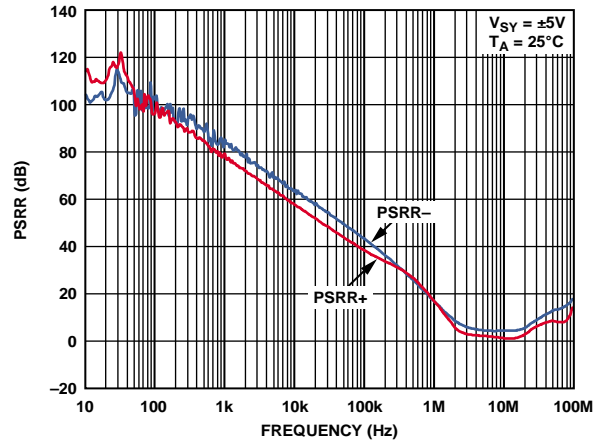


Figure 57. PSRR vs. Frequency

08237-037

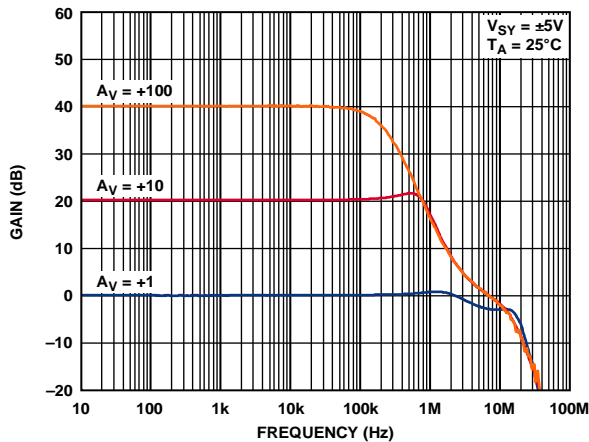


Figure 55. Closed-Loop Gain vs. Frequency

08237-035

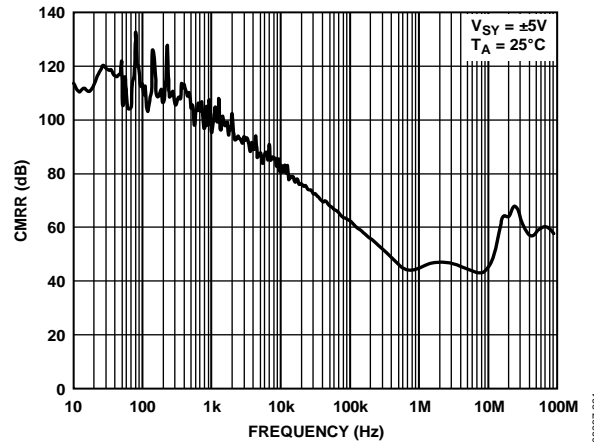


Figure 58. CMRR vs. Frequency

08237-221

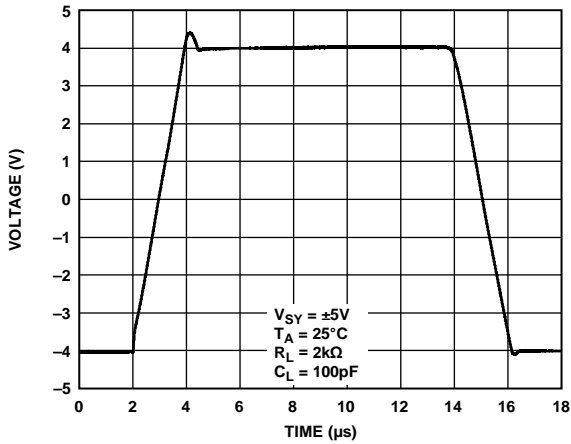


Figure 59. Large Signal Transient Response

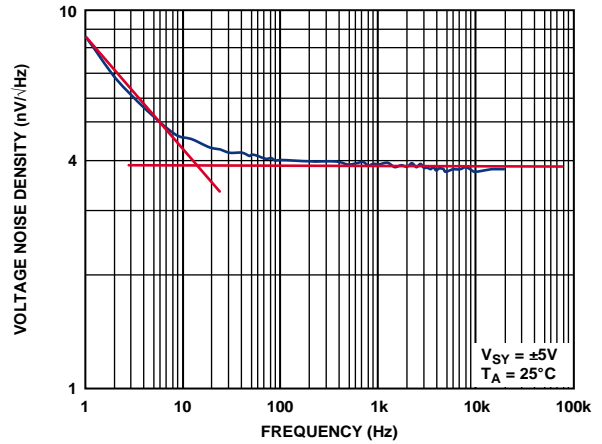


Figure 62. Voltage Noise Density vs. Frequency

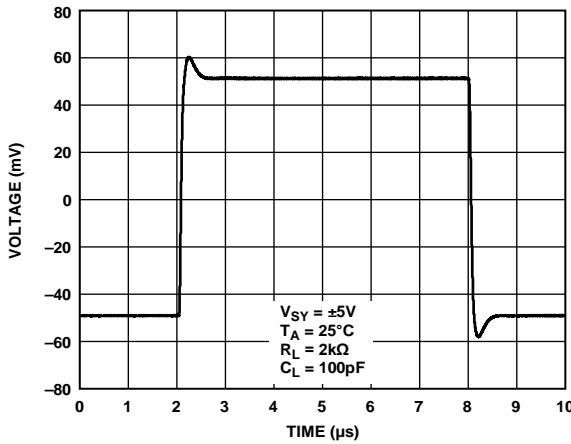


Figure 60. Small Signal Transient Response

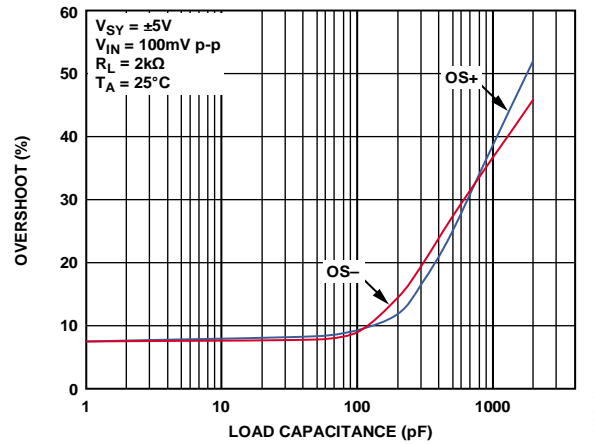


Figure 63. Overshoot vs. Load Capacitance

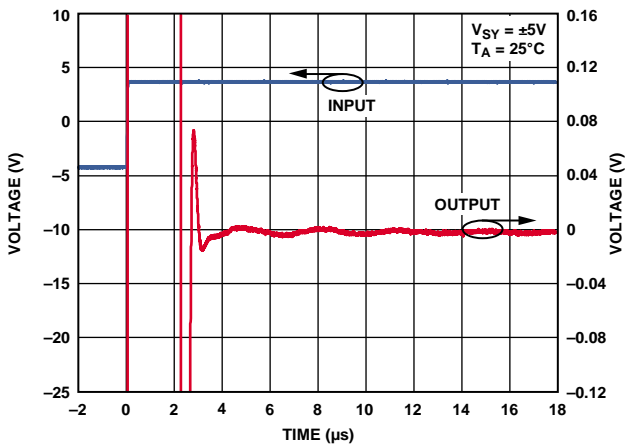


Figure 61. Settling Time

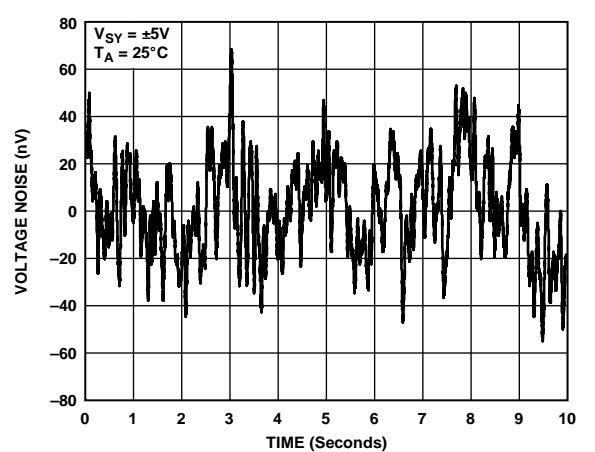


Figure 64. Voltage Noise, 0.1 Hz to 10 Hz

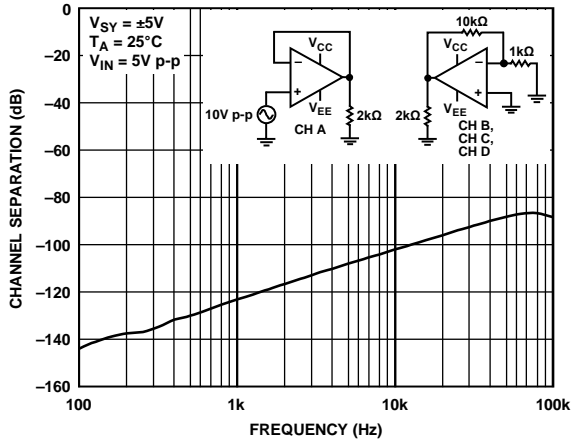


Figure 65. Channel Separation vs. Frequency

08237-045

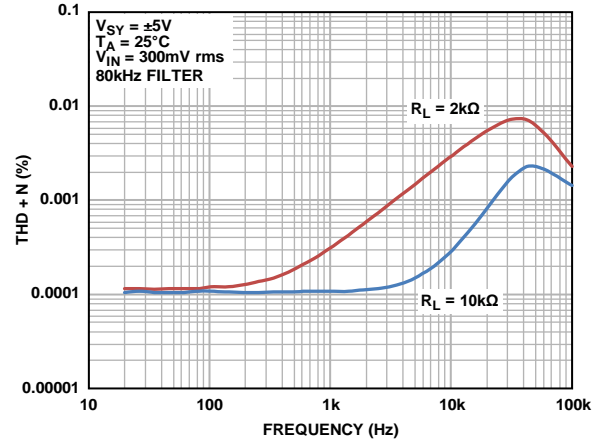


Figure 68. THD + N vs. Frequency, 80 kHz Filter

08237-260

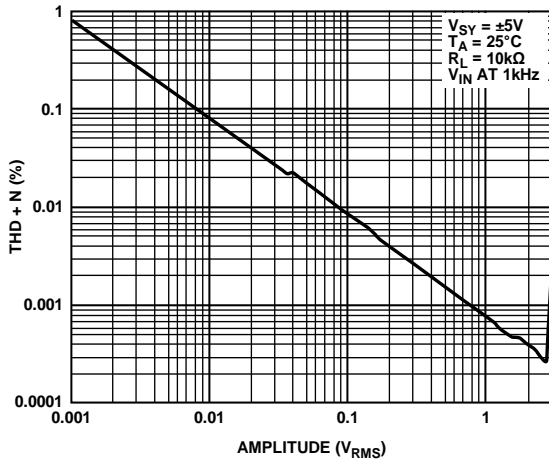


Figure 66. THD + N vs. Amplitude

08237-150

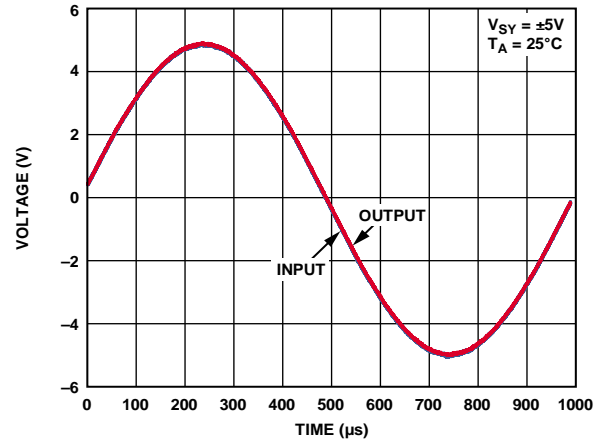


Figure 69. No Phase Reversal

08237-048

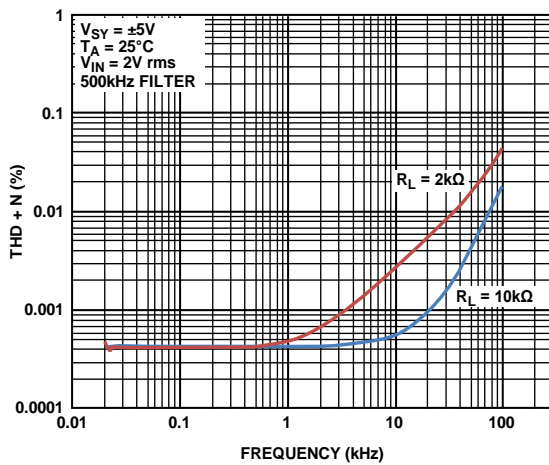


Figure 67. THD + N vs. Frequency, 500 kHz Filter

08237-151

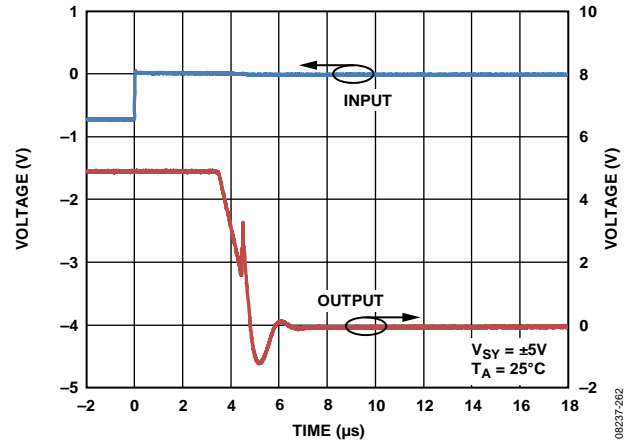


Figure 70. Positive 50% Overload Recovery

08237-262

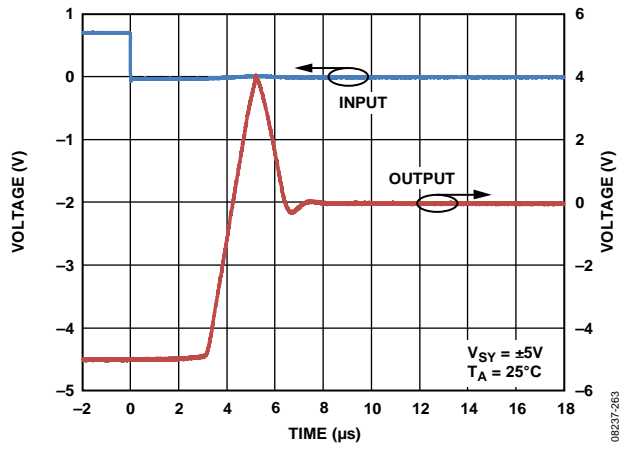


Figure 71. Negative 50% Overload Recovery

**±15 V CHARACTERISTICS**

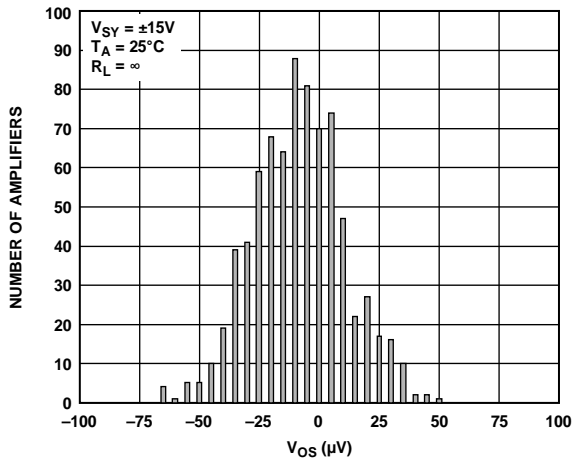


Figure 72. Input Offset Voltage ( $V_{OS}$ ) Distribution, SOIC

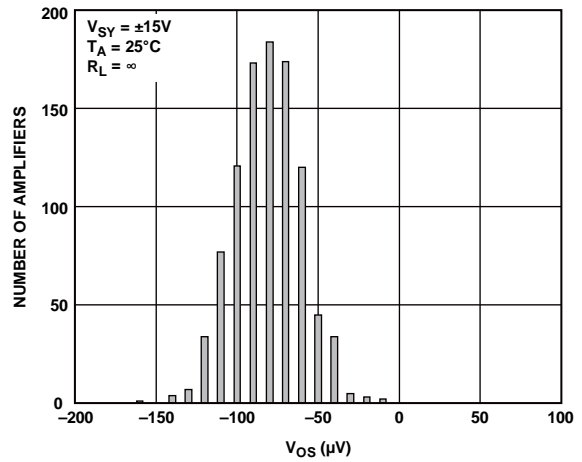


Figure 75. Input Offset Voltage ( $V_{OS}$ ) Distribution, LFCSP

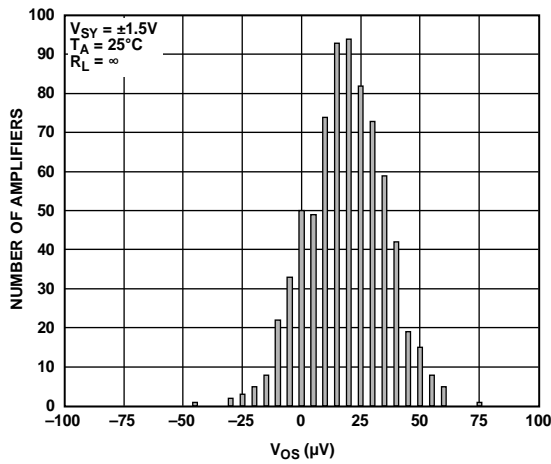


Figure 73. Input Offset Voltage ( $V_{OS}$ ) Distribution, SOT-23

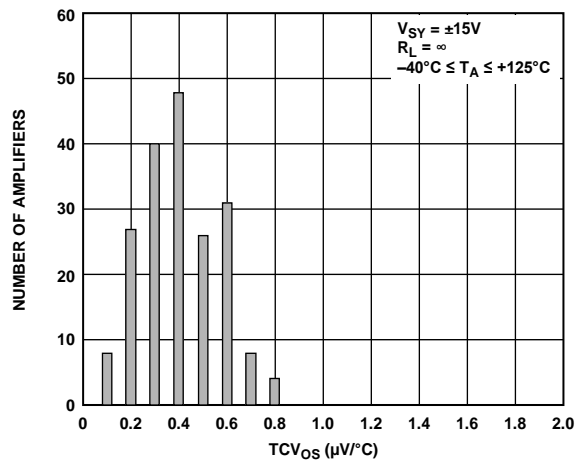


Figure 76.  $TCV_{OS}$  Distribution, SOIC, MSOP, and TSSOP

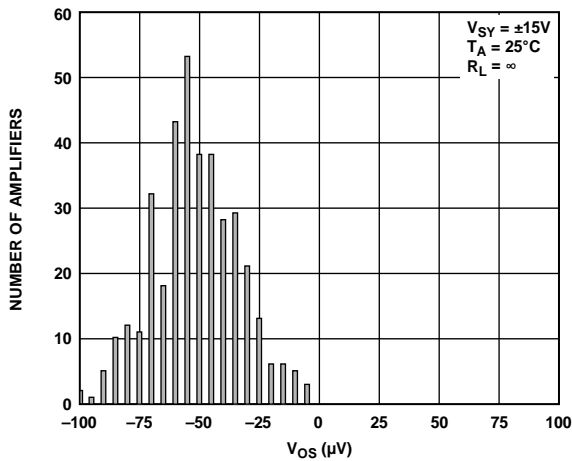


Figure 74. Input Offset Voltage ( $V_{OS}$ ) Distribution, MSOP and TSSOP

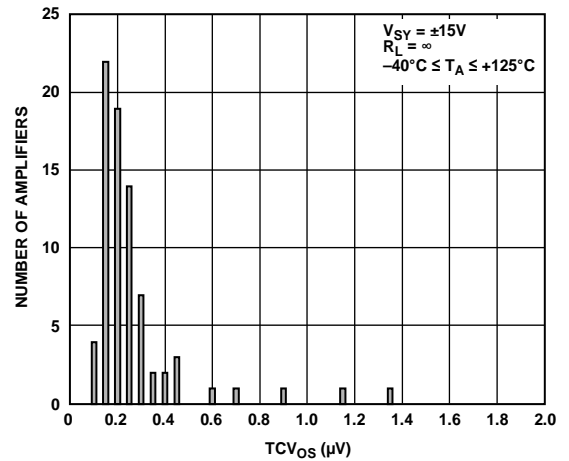


Figure 77.  $TCV_{OS}$  Distribution, SOT-23

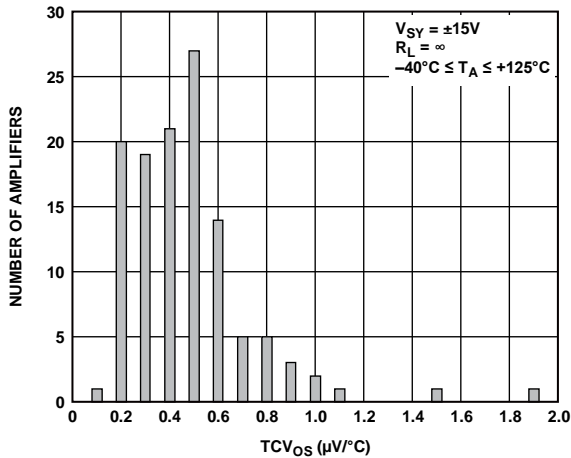


Figure 78.  $TCV_{OS}$  Distribution, LFCSP

08237-085

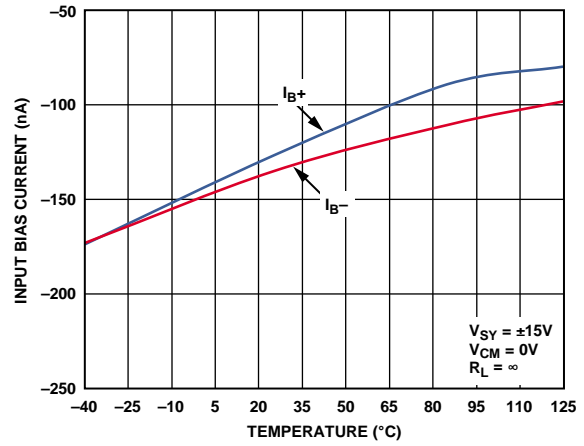


Figure 81. Input Bias Current vs. Temperature

08237-053

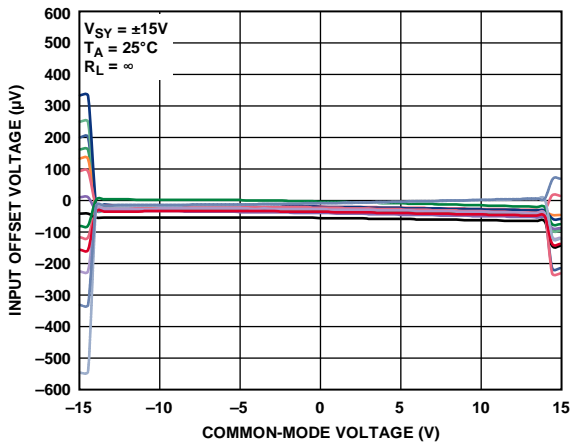


Figure 79. Input Offset Voltage vs. Common-Mode Voltage

08237-052

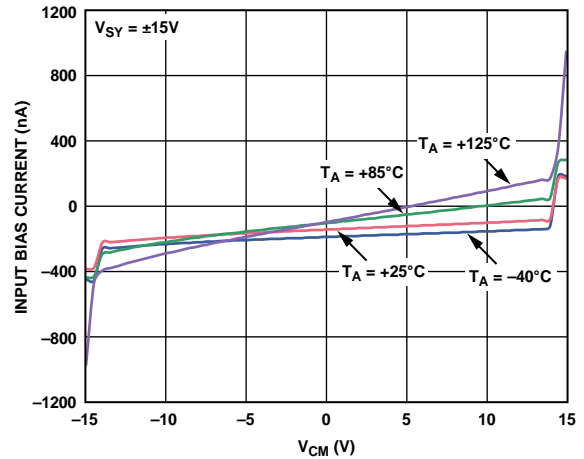


Figure 82. Input Bias Current vs.  $V_{CM}$  for Various Temperatures

08237-054

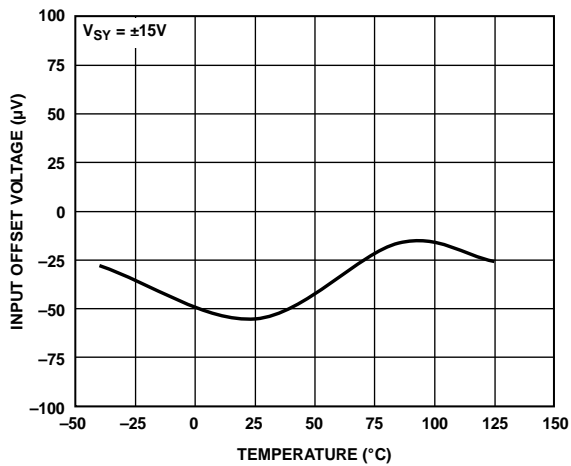


Figure 80. Input Offset Voltage vs. Temperature

08237-165

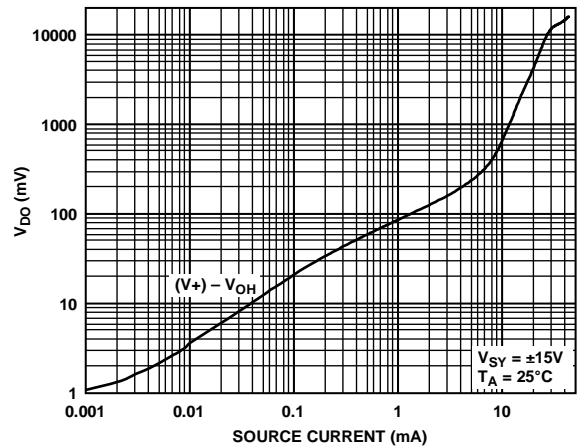


Figure 83. Dropout Voltage ( $V_{D0}$ ) vs. Source Current

08237-055



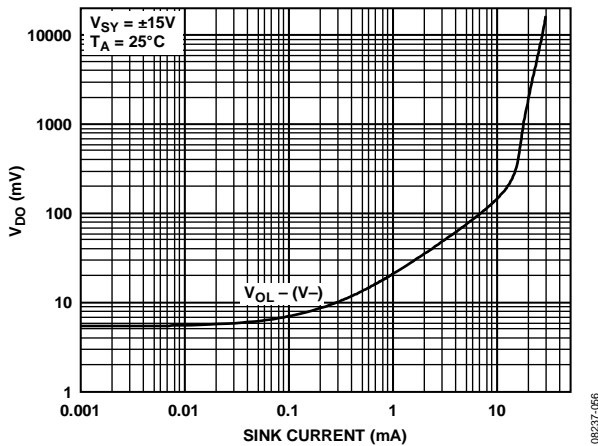


Figure 84. Dropout Voltage ( $V_{DO}$ ) vs. Sink Current

08237-056

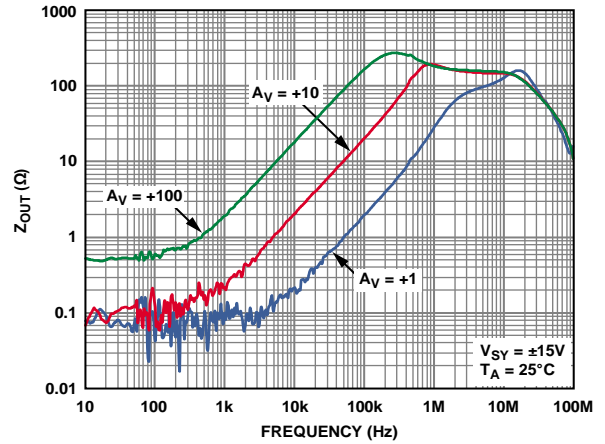


Figure 87. Output Impedance ( $Z_{OUT}$ ) vs. Frequency

08237-059

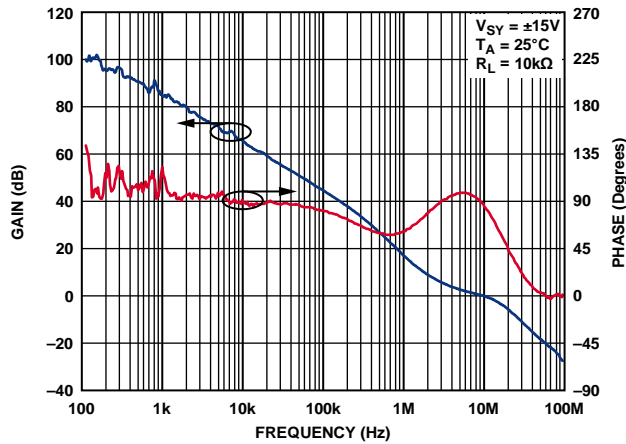


Figure 85. Open-Loop Gain and Phase vs. Frequency

08237-057

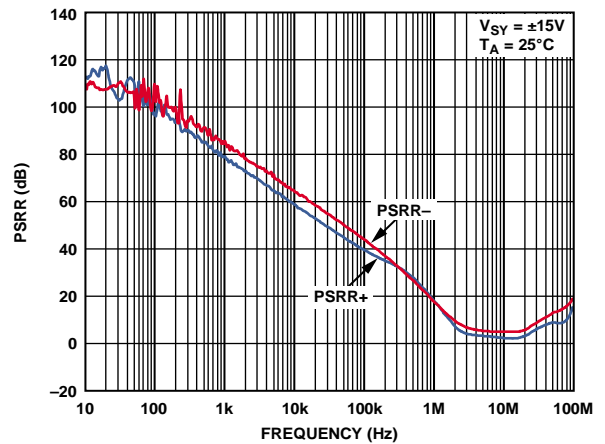


Figure 88. PSRR vs. Frequency

08237-060

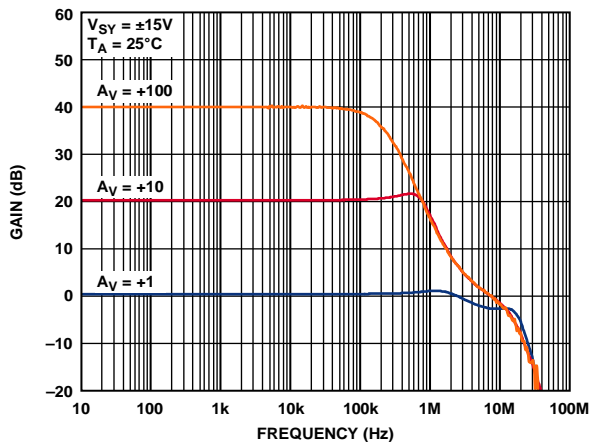


Figure 86. Closed-Loop Gain vs. Frequency

08237-058

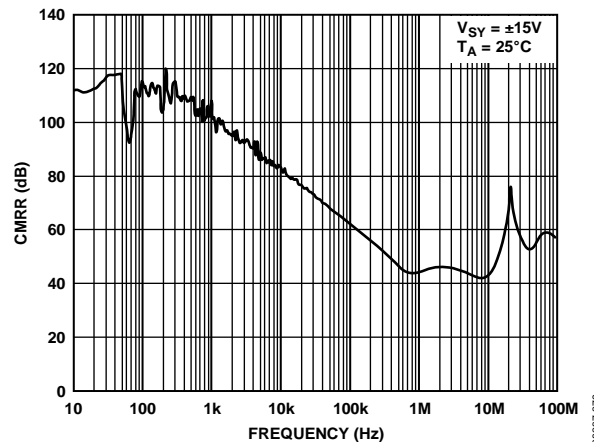


Figure 89. CMRR vs. Frequency

08237-279

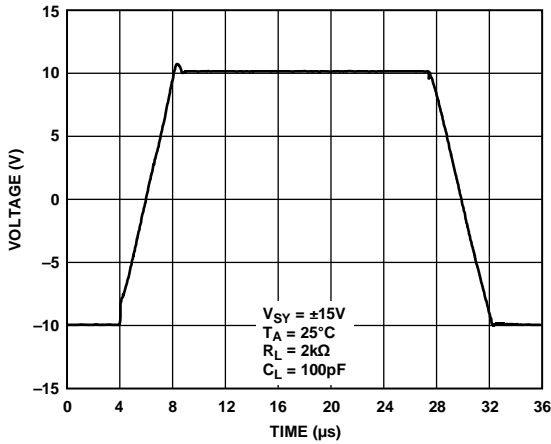


Figure 90. Large Signal Transient Response

08237-062

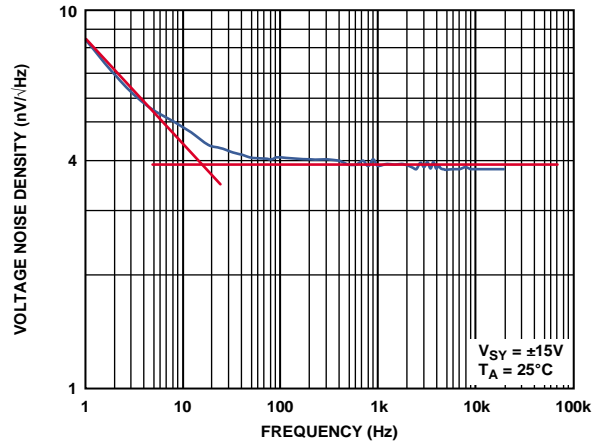


Figure 93. Voltage Noise Density vs. Frequency

08237-065

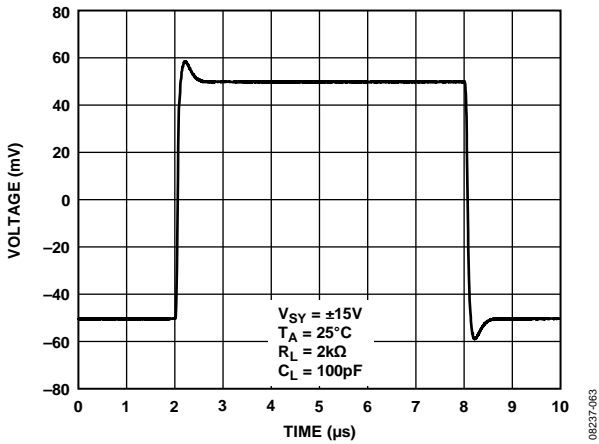


Figure 91. Small Signal Transient Response

08237-063

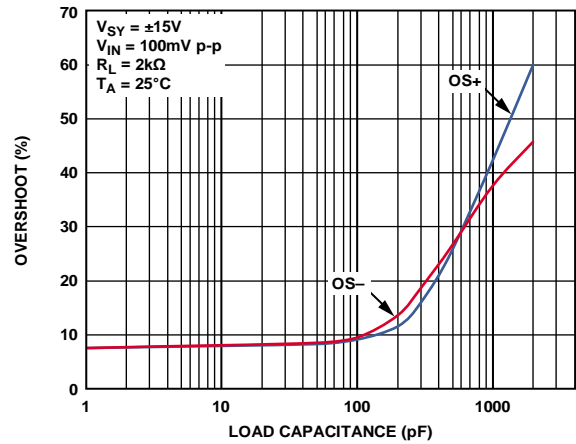


Figure 94. Overshoot vs. Load Capacitance

08237-066

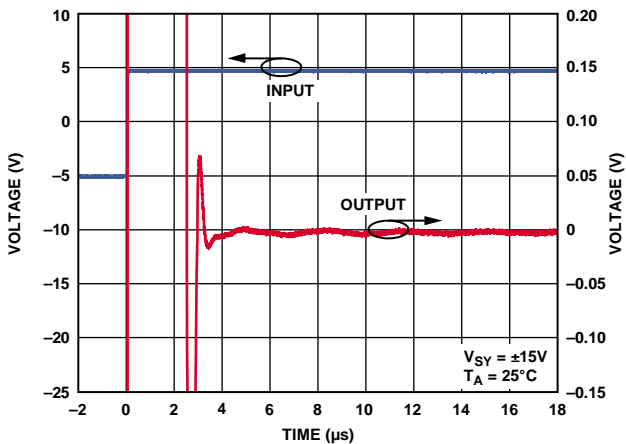


Figure 92. Settling Time

08237-064

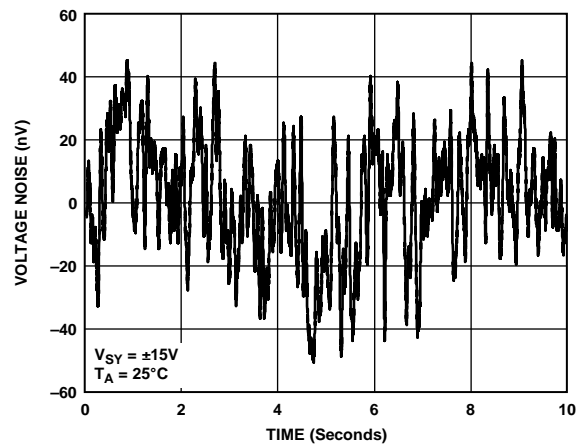


Figure 95. Voltage Noise 0.1 Hz to 10 Hz

08237-067

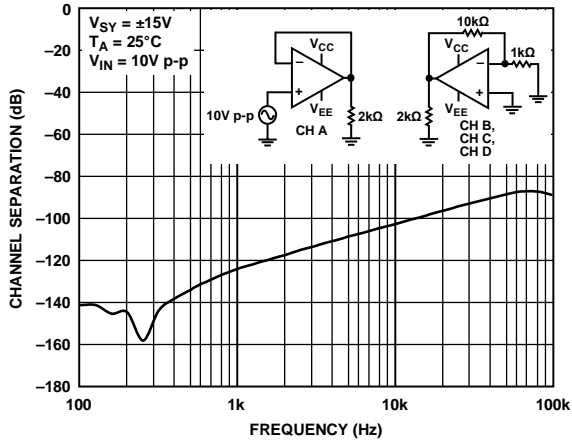


Figure 96. Channel Separation vs. Frequency

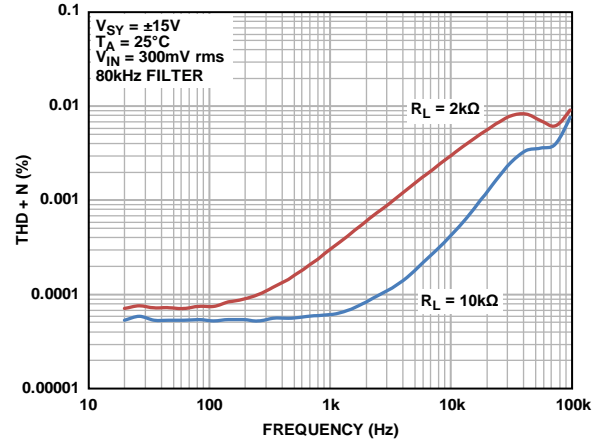


Figure 99. THD + N vs. Frequency, 80 kHz Filter

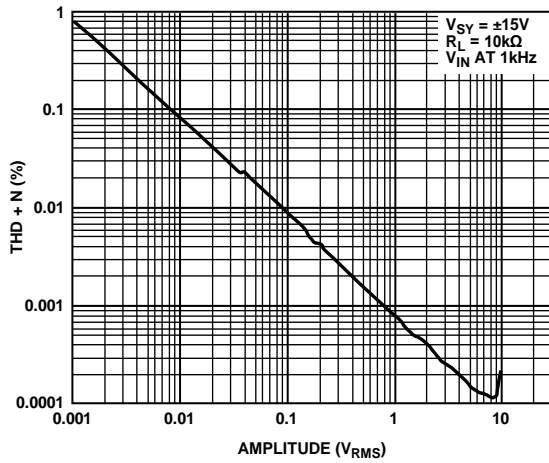


Figure 97. THD + N vs. Amplitude

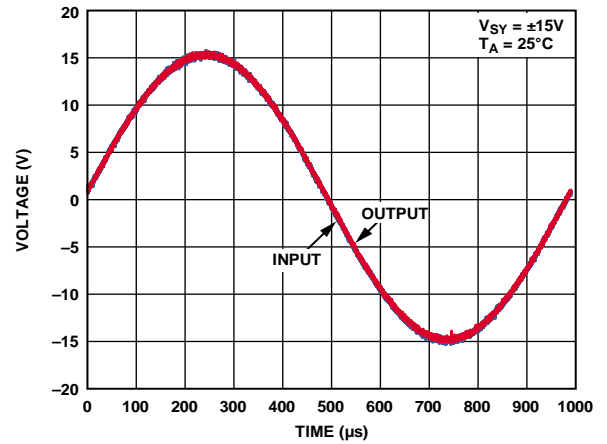


Figure 100. No Phase Reversal

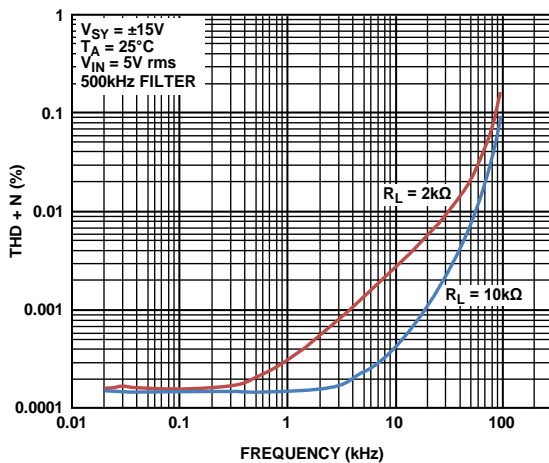


Figure 98. THD + N vs. Frequency, 500 kHz Filter

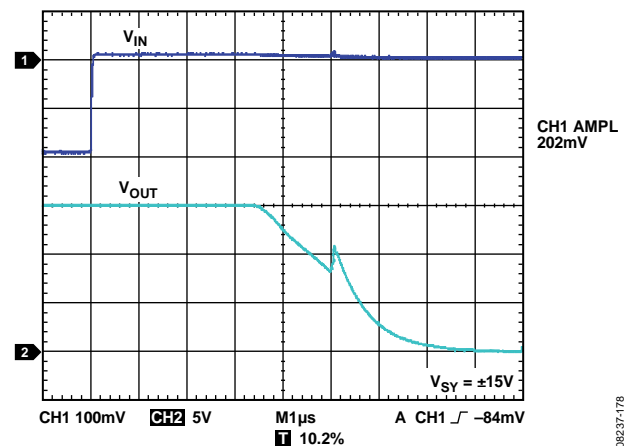


Figure 101. Positive 50% Overload Recovery

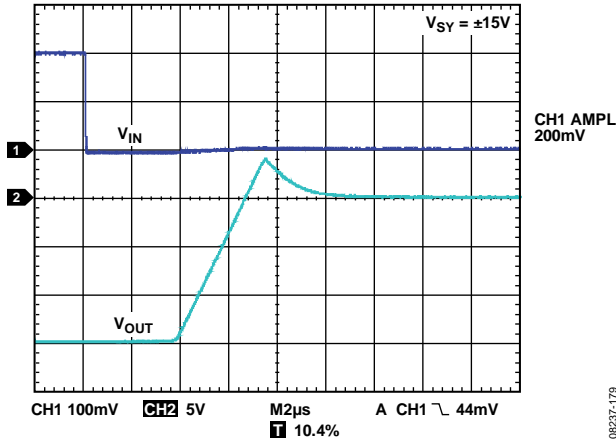


Figure 102. Negative 50% Overload Recovery

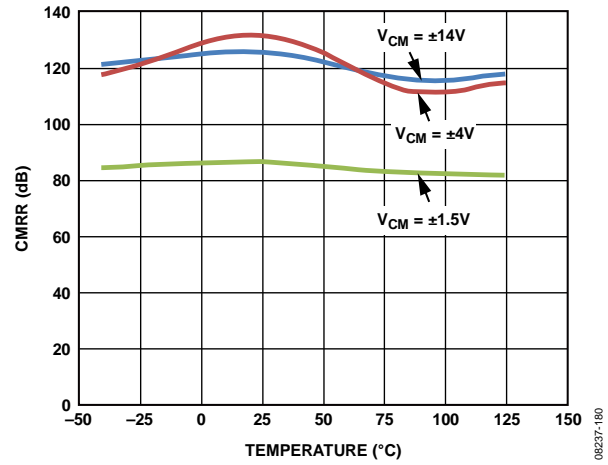


Figure 104. CMRR vs. Temperature

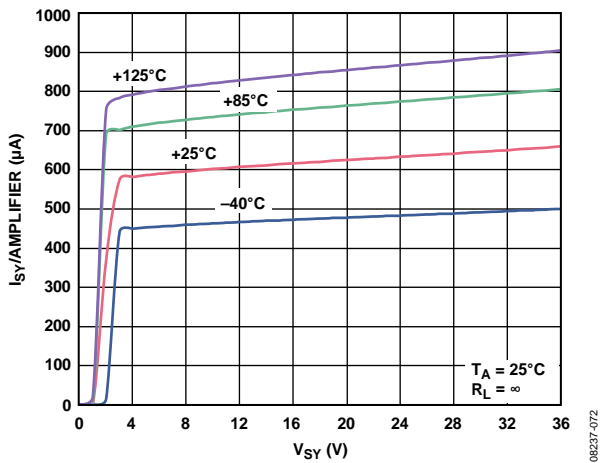


Figure 103. Supply Current ( $I_{SY}$ ) per Amplifier vs. Supply Voltage ( $V_{SY}$ ) for Various Temperatures

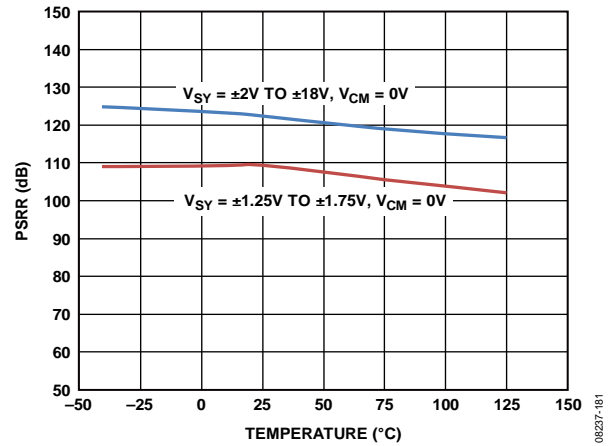


Figure 105. PSRR vs. Temperature

## APPLICATIONS INFORMATION

### FUNCTIONAL DESCRIPTION

The ADA4084-1/ADA4084-2/ADA4084-4 devices are precision single-supply, rail-to-rail operational amplifiers. Intended for portable instrumentation, the ADA4084-1/ADA4084-2/ADA4084-4 devices combine the attributes of precision, wide bandwidth, and low noise, making them an ideal choice in single-supply applications that require both ac and precision dc performance. Other low supply voltage applications for which the ADA4084-1/ADA4084-2/ADA4084-4 devices are well suited include active filters, audio microphone preamplifiers, power supply control, and telecommunications. To combine all of these attributes with rail-to-rail input/output operation, novel circuit design techniques are used.

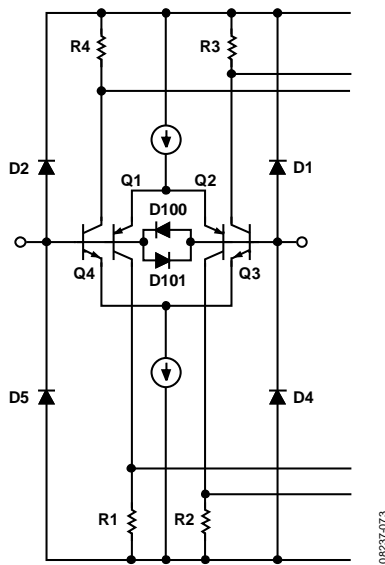


Figure 106. Equivalent Input Circuit

For example, Figure 106 illustrates a simplified equivalent circuit for the input stage of the ADA4084-1/ADA4084-2/ADA4084-4. It comprises a PNP differential pair, Q1 and Q2, and an NPN differential pair, Q3 and Q4, operating concurrently. Diode D100 and Diode D101 serve to clamp the applied differential input voltage to the ADA4084-1/ADA4084-2/ADA4084-4, thereby protecting the input transistors against Zener breakdown of the emitter-base junctions. Input stage voltage gains are kept low for input rail-to-rail operation. The two pairs of differential output voltages are connected to the second stage of the ADA4084-1/ADA4084-2/ADA4084-4, which is a modified compound folded cascade gain stage. It is also in the second gain stage that the two pairs of differential output voltages are combined into a single-ended output signal voltage used to drive the output stage.

A key issue in the input stage is the behavior of the input bias currents over the input common-mode voltage range. Input bias currents in the ADA4084-1/ADA4084-2/ADA4084-4 are the arithmetic sum of the base currents in Q1 and Q4 and in Q2 and Q3. As a result of this design approach, the input bias currents in the ADA4084-1/ADA4084-2/ADA4084-4 not only exhibit different amplitudes, but they also exhibit different polarities. This effect is best shown in Figure 19, Figure 20, Figure 50, Figure 51, Figure 81, and Figure 82. It is, therefore, important that the effective source impedances that are connected to the ADA4084-1/ADA4084-2/ADA4084-4 inputs be balanced for optimum dc and ac performance.

To achieve rail-to-rail output, the ADA4084-1/ADA4084-2/ADA4084-4 output stage design employs a unique topology for both sourcing and sinking current. This circuit topology is shown in Figure 107. The output stage is voltage driven from the second gain stage. The signal path through the output stage is inverting; that is, for positive input signals, Q13 provides the base current drive to Q19 so that it conducts (sinks) current. For negative input signals, the signal path via Q18 to the mirror to Q24 provides the base current drive for Q23 to conduct (source) current. Both transistors provide output current until they are forced into saturation.

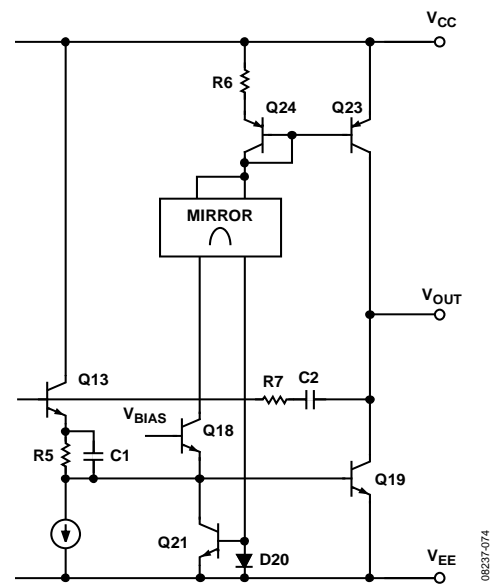


Figure 107. Equivalent Output Circuit

Thus, the saturation voltage of the output transistors sets the limit on the ADA4084-1/ADA4084-2/ADA4084-4 maximum output voltage swing. Output short-circuit current limiting is determined by the maximum signal current into the base of Q13 from the second gain stage. The output stage also exhibits voltage gain. This is accomplished by the use of common-emitter amplifiers, and, as a result, the voltage gain of the output stage (thus, the open-loop gain of the device) exhibits a dependence on the total load resistance at the output of the ADA4084-1/ADA4084-2/ADA4084-4.

**START-UP CHARACTERISTICS**

The ADA4084-1/ADA4084-2/ADA4084-4 are specified to operate from 3 V to 30 V ( $\pm 1.5$  V to  $\pm 15$  V) under nominal power supplies. During power-up as the supply voltage increases from 0 V to the nominal power supply voltage, the supply current ( $I_{SY}$ ) increases as well, to the point at which it stabilizes and the amplifier is ready to operate. The stabilization varies with temperature, as shown in Figure 103. For example, at  $-40^{\circ}\text{C}$ , it requires a higher voltage and stabilizes at a lower supply current than at hot temperatures. At hot temperatures, it requires a lower voltage but stabilizes at a higher current. In all cases, the ADA4084-1/ADA4084-2/ADA4084-4 are specified to start up and operate at a minimum of 3 V under all temperature conditions.

**INPUT PROTECTION**

As with any semiconductor device, if conditions exist where the applied input voltages to the device exceed either supply voltage, the input overvoltage I-to-V characteristic of the device must be considered. When an overvoltage occurs, the amplifier may be damaged, depending on the magnitude of the applied voltage and the magnitude of the fault current.

The D1, D2, D4, and D5 diodes conduct when the input common-mode voltage exceeds either supply pin by a diode drop. This diode drop voltage varies with temperature and is in the range of 0.3 V to 0.8 V. As shown in the simplified equivalent input circuit of Figure 106, the ADA4084-1/ADA4084-2/ADA4084-4 do not have any internal current limiting resistors; thus, fault currents can quickly rise to damaging levels.

This input current is not inherently damaging to the device, provided that it is limited to 5 mA or less. If a fault condition causes more than 5 mA to flow, add an external series resistor at the expense of additional thermal noise. Figure 108 shows a typical noninverting configuration for an overvoltage protected amplifier, where the series resistance (R1) is chosen, such that

$$RI = \frac{V_{IN(MAX)} - V_{SUPPLY}}{5 \text{ mA}}$$

For example, a 1 k $\Omega$  resistor protects the ADA4084-1/ADA4084-2/ADA4084-4 against input signals up to 5 V above and below the supplies. Note that the thermal noise of a 1 k $\Omega$  resistor at room temperature is 4 nV/ $\sqrt{\text{Hz}}$ , which exceeds the voltage noise of the ADA4084-1/ADA4084-2/ADA4084-4. For other configurations in which both inputs are used, add a series resistor to limit the input current. To ensure optimum dc and ac performance, balance the source impedance levels.

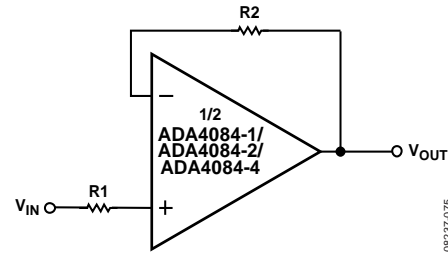


Figure 108. Resistance in Series with the Input Limits Overvoltage Currents to Safe Values

To protect the Q1/Q2 and Q3/Q4 pairs from large differential voltages that may result in Zener breakdown of the emitter-base junction, D100 and D101 are connected between the two inputs. This precludes operation as a comparator. For a more complete description, see the MT-035 Tutorial, *Op Amp Inputs, Outputs, Single-Supply, and Rail-to-Rail Issues*; the MT-083 Tutorial, *Comparators*; the MT-084 Tutorial, *Using Op Amps as Comparators*; and the AN-849 Application Note, *Using Op Amps as Comparators*.

**OUTPUT PHASE REVERSAL**

Some operational amplifiers designed for single-supply operation exhibit an output voltage phase reversal when their inputs are driven beyond their useful common-mode range. Typically, for single-supply bipolar op amps, the negative supply determines the lower limit of their common-mode range. With these devices, external clamping diodes, with the anode connected to ground and the cathode to the inputs, prevent input signal excursions from exceeding the negative supply of the device (that is, GND), preventing a condition that causes the output voltage to change phase. JFET input amplifiers can also exhibit phase reversal, and, if so, a series input resistor is usually required to prevent it.

The ADA4084-1/ADA4084-2/ADA4084-4 are free from reasonable input voltage range restrictions, provided that input voltages no greater than the supply voltages are applied (see Figure 38, Figure 69, and Figure 100).

Although device output does not change phase, large currents can flow through the input protection diodes. Therefore, apply the technique recommended in the Input Protection section to those applications where the likelihood of input voltages exceeding the supply voltages is high.

**DESIGNING LOW NOISE CIRCUITS IN SINGLE-SUPPLY APPLICATIONS**

In single-supply applications, devices like the [ADA4084-1/ADA4084-2/ADA4084-4](#) extend the dynamic range of the application through the use of rail-to-rail operation. Referring to the op amp noise model circuit configuration illustrated in Figure 109, the expression for the total equivalent input noise voltage of an amplifier for a source resistance level,  $R_S$ , is given by

$$e_{nT} = \sqrt{2[(e_{nR})^2 + (i_{nOA} \times R_S)^2] + (e_{nOA})^2}, \text{ units in } \frac{V}{\sqrt{\text{Hz}}}$$

where:

$(e_{nR})^2$  is the source resistance thermal noise voltage power ( $4kTR$ ).

$k$  is the Boltzmann's constant,  $1.38 \times 10^{-23}$  J/K.

$T$  is the ambient temperature in Kelvin of the circuit,  $273.15 + T_A$  ( $^{\circ}\text{C}$ ).

$(i_{nOA})^2$  is the op amp equivalent input noise current spectral power (1 Hz bandwidth).

$R_S = 2R$ , the effective, or equivalent, circuit source resistance.

$(e_{nOA})^2$  is the op amp equivalent input noise voltage spectral power (1 Hz bandwidth).

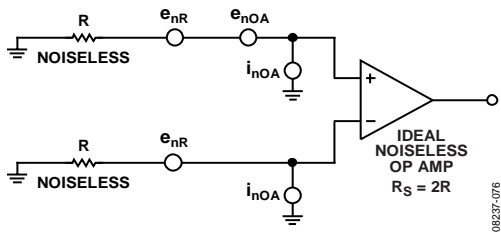


Figure 109. Op Amp Noise Circuit Model Used to Determine Total Circuit Equivalent Input Noise Voltage and Noise Figure

As a design aid, Figure 110 shows the equivalent thermal noise of the [ADA4084-1/ADA4084-2/ADA4084-4](#) vs. the total source resistance. Note that for source resistance less than 1 k $\Omega$ , the equivalent input noise voltage of the [ADA4084-1/ADA4084-2/ADA4084-4](#) is dominant.

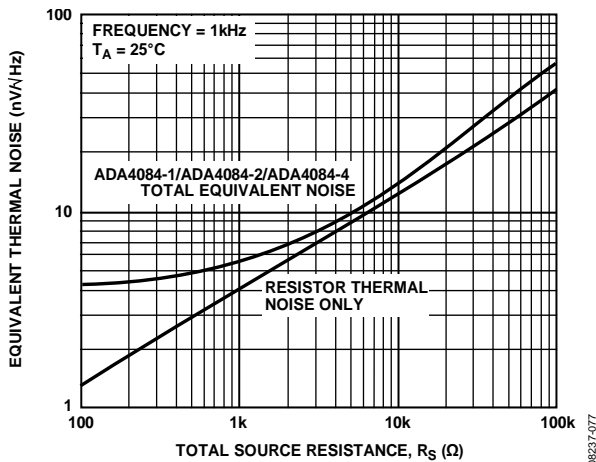


Figure 110. Equivalent Thermal Noise vs. Total Source Resistance

Because circuit SNR is the critical parameter in the final analysis, the noise behavior of a circuit is sometimes expressed in terms of its noise figure (NF). The noise figure is defined as the ratio of the signal-to-noise output of a circuit to its signal-to-noise input.

Noise figure is generally used for RF and microwave circuit analysis in a 50  $\Omega$  system. This is not very useful for op amp circuits where the input and output impedances can vary greatly. For a more complete description of noise figure, see the [MT-052 Tutorial, Op Amp Noise Figure: Don't be Misled](#).

Signal levels in the application invariably increase to maximize circuit SNR, which is not an option in low voltage, single-supply applications.

Therefore, to achieve optimum circuit SNR in single-supply applications, choose an operational amplifier with the lowest equivalent input noise voltage, along with source resistance levels that are consistent with maintaining low total circuit noise.

**COMPARATOR OPERATION**

Although op amps are quite different from comparators, occasionally an unused section of a dual or a quad op amp can be used as a comparator; however, this is not recommended for any rail-to-rail output op amps. For rail-to-rail output op amps, the output stage is generally a ratioed current mirror with bipolar or MOSFET transistors. With the device operating open-loop, the second stage increases the current drive to the ratioed mirror to close the loop. However, the loop cannot close, which results in an increase in supply current. With the op amp configured as a comparator, the supply current can be significantly higher (see Figure 111). Configure an unused section as a voltage follower with the noninverting input connected to a voltage within the input voltage range. The [ADA4084-1/ADA4084-2/ADA4084-4](#) have unique second stage and output stage designs that greatly reduce the excess supply current when the op amp is operating open-loop.

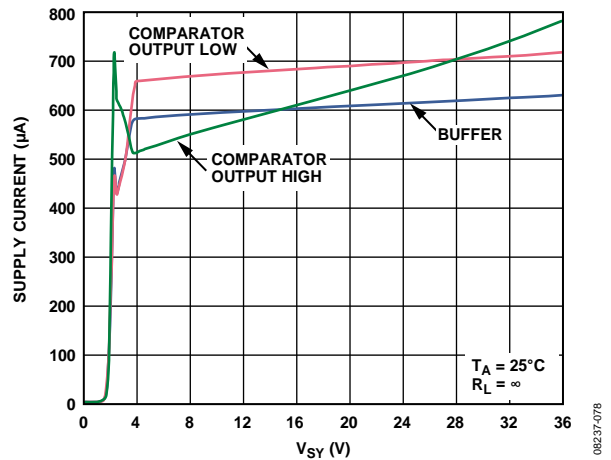


Figure 111. Supply Current vs. Supply Voltage ( $V_S$ )



**LONG-TERM DRIFT**

The stability of a precision signal path over its lifetime or between calibration procedures is dependent on the long-term stability of the analog components in the path, such as op amps, references, and data converters. To help system designers predict the long-term drift of circuits that use the ADA4084-1/ADA4084-2/ADA4084-4, Analog Devices measured the offset voltage of multiple units for 10,000 hours (more than 13 months) using a high precision measurement system, including an ultrastable oil bath. To replicate real-world system performance, the devices under test (DUTs) were soldered onto an FR4 PCB using a standard reflow profile (as defined in the JEDEC J-STD-020D standard), as opposed to testing them in sockets. This manner of testing is important because expansion and contraction of the PCB can apply stress to the integrated circuit (IC) package and contribute to shifts in the offset voltage.

The ADA4084-1/ADA4084-2/ADA4084-4 have extremely low long-term drift, as shown in Figure 112. The red, blue, and green traces show sample units. Note that the mean drift of the ADA4084-1/ADA4084-2/ADA4084-4 over 10,000 hours is less than 3  $\mu\text{V}$ , or less than 3% of their maximum specified offset voltage of 100  $\mu\text{V}$  at room temperature.

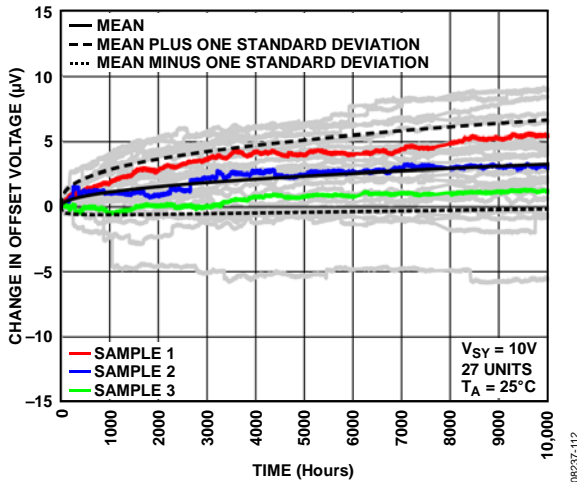


Figure 112. Measured Long-Term Drift of the ADA4084-1/ADA4084-2/ADA4084-4 Offset Voltage over 10,000 Hours

**TEMPERATURE HYSTERESIS**

In addition to stability over time as described in the Long-Term Drift section, it is useful to know the temperature hysteresis, that is, the stability vs. cycling of temperature. Hysteresis is an important parameter because it tells the system designer how closely the signal returns to its starting amplitude after the ambient temperature changes and subsequent return to room temperature. Figure 113 shows the change in input offset voltage as the temperature cycles three times from room temperature to +125°C to -40°C and back to room temperature. The dotted line is an initial preconditioning cycle to eliminate the original temperature-induced offset shift from exposure to production solder reflow temperatures. In the three full cycles, the offset hysteresis is typically only 4  $\mu\text{V}$ , or 2% of its 200  $\mu\text{V}$  maximum offset voltage over the full operating temperature range. The histogram in Figure 114 shows that the hysteresis is larger when the device is cycled through only a half cycle, from room temperature to 125°C and back to room temperature.

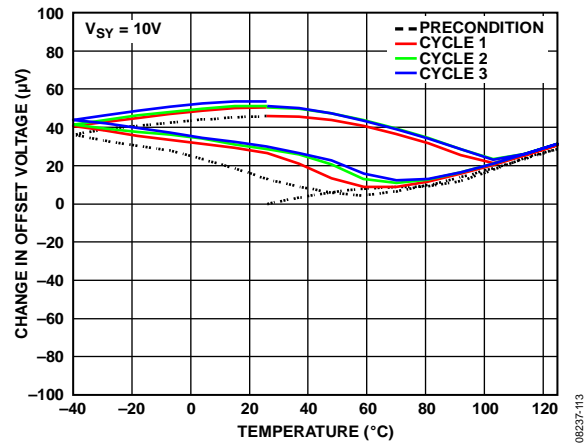


Figure 113. Change in Offset Voltage over Three Full Temperature Cycles

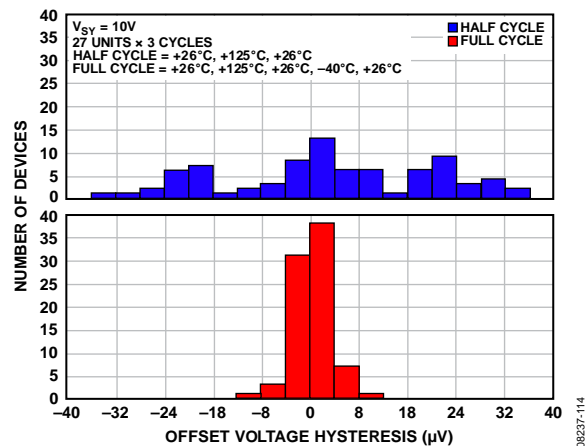
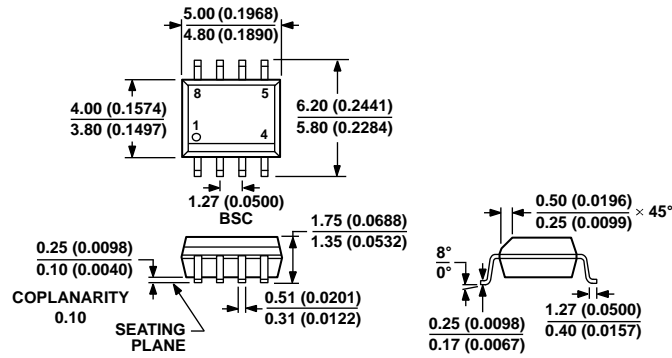


Figure 114. Histogram Showing the Temperature Hysteresis of the Offset Voltage over Three Full Cycles and over Three Half Cycles



# OUTLINE DIMENSIONS

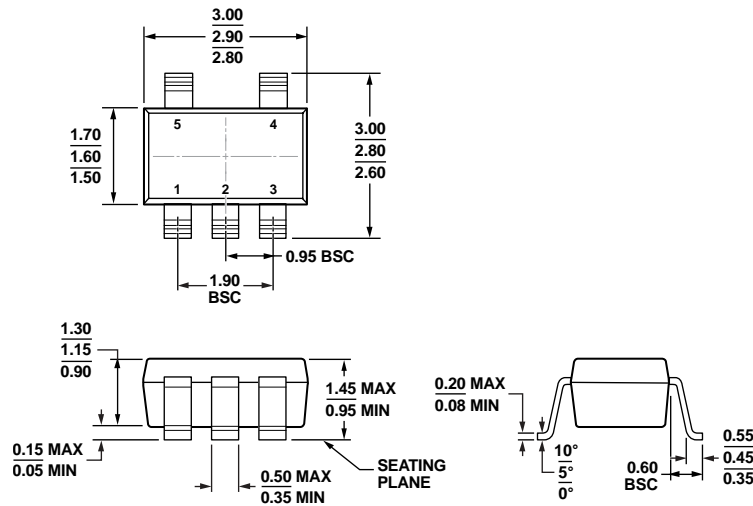


COMPLIANT TO JEDEC STANDARDS MS-012-AA  
CONTROLLING DIMENSIONS ARE IN MILLIMETERS; INCH DIMENSIONS (IN PARENTHESES) ARE ROUNDED-OFF MILLIMETER EQUIVALENTS FOR REFERENCE ONLY AND ARE NOT APPROPRIATE FOR USE IN DESIGN.

012A07-A

Figure 115. 8-Lead Standard Small Outline Package [SOIC\_N] Narrow Body (R-8)

Dimensions shown in millimeters and (inches)

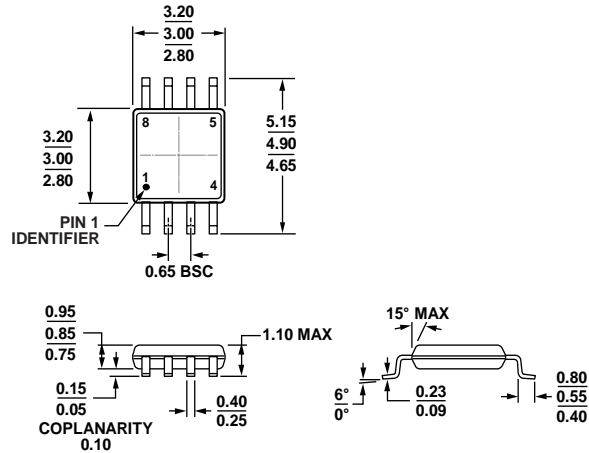


COMPLIANT TO JEDEC STANDARDS MO-178-AA

Figure 116. 5-Lead Small Outline Transistor Package [SOT-23] (RJ-5)

Dimensions shown in millimeters

11-01-2010-A

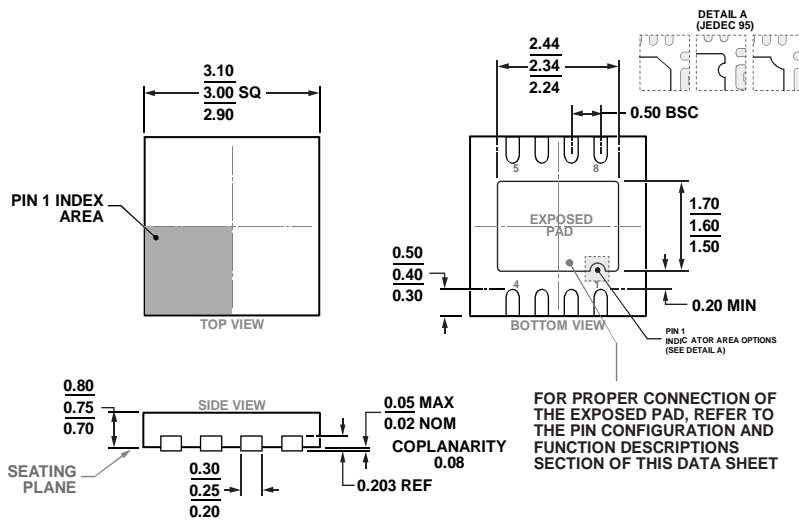


COMPLIANT TO JEDEC STANDARDS MO-187-AA

Figure 117. 8-Lead Mini Small Outline Package [MSOP] (RM-8)

Dimensions shown in millimeters

10-07-2009-B

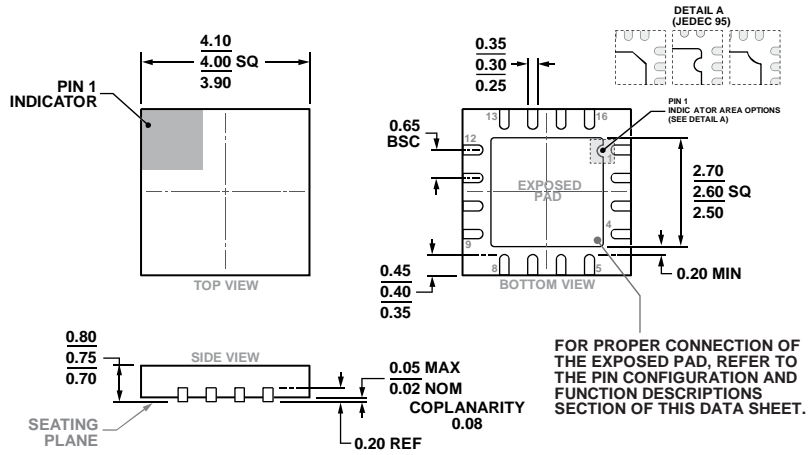


COMPLIANT TO JEDEC STANDARDS MO-229-W3030D-4

Figure 118. 8-Lead Lead Frame Chip Scale Package [LFCSP] 3 mm x 3 mm Body and 0.75 mm Package Height (CP-8-11)

Dimensions shown in millimeters

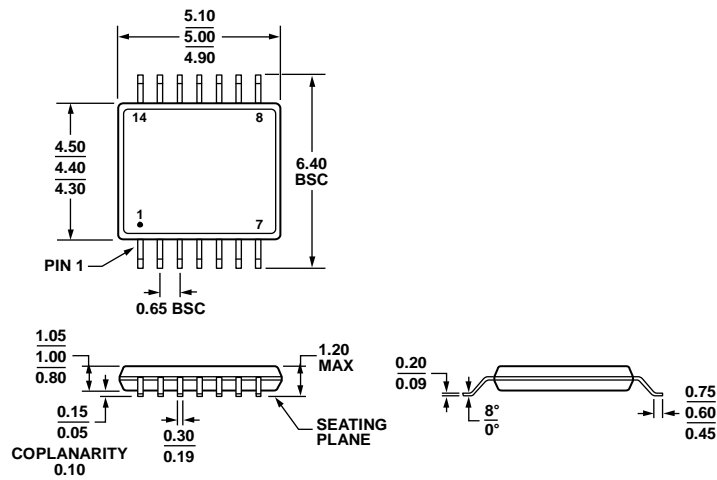
02-10-2017-C



COMPLIANT TO JEDEC STANDARDS MO-220-WGGC.

Figure 119. 16-Lead Lead Frame Chip Scale Package [LFCSFP]  
4 mm × 4 mm Body and 075 mm Package Height  
(CP-16-17)

Dimensions shown in millimeters



COMPLIANT TO JEDEC STANDARDS MO-153-AB-1

Figure 120. 14-Lead Thin Shrink Small Outline Package [TSSOP]  
(RU-14)

Dimensions shown in millimeters

**ORDERING GUIDE**

Model <sup>1</sup>	Temperature Range	Package Description	Package Option	Branding
ADA4084-1ARZ	-40°C to +125°C	8-Lead Standard Small Outline Package [SOIC_N]	R-8	
ADA4084-1ARZ-R7	-40°C to +125°C	8-Lead Standard Small Outline Package [SOIC_N]	R-8	
ADA4084-1ARZ-RL	-40°C to +125°C	8-Lead Standard Small Outline Package [SOIC_N]	R-8	
ADA4084-1ARJZ-R2	-40°C to +125°C	5-Lead Small Outline Transistor Package [SOT-23]	RJ-5	A38
ADA4084-1ARJZ-R7	-40°C to +125°C	5-Lead Small Outline Transistor Package [SOT-23]	RJ-5	A38
ADA4084-1ARJZ-RL	-40°C to +125°C	5-Lead Small Outline Transistor Package [SOT-23]	RJ-5	A38
ADA4084-2ARMZ	-40°C to +125°C	8-Lead Mini Small Outline Package [MSOP]	RM-8	A2Q
ADA4084-2ARMZ-R7	-40°C to +125°C	8-Lead Mini Small Outline Package [MSOP]	RM-8	A2Q
ADA4084-2ARMZ-RL	-40°C to +125°C	8-Lead Mini Small Outline Package [MSOP]	RM-8	A2Q
ADA4084-2ARZ	-40°C to +125°C	8-Lead Standard Small Outline Package [SOIC_N]	R-8	
ADA4084-2ARZ-R7	-40°C to +125°C	8-Lead Standard Small Outline Package [SOIC_N]	R-8	
ADA4084-2ARZ-RL	-40°C to +125°C	8-Lead Standard Small Outline Package [SOIC_N]	R-8	
ADA4084-2ACPZ-R7	-40°C to +125°C	8-Lead Lead Frame Chip Scale Package [LFCSP]	CP-8-11	A2Q
ADA4084-2ACPZ-RL	-40°C to +125°C	8-Lead Lead Frame Chip Scale Package [LFCSP]	CP-8-11	A2Q
ADA4084-4ACPZ-R7	-40°C to +125°C	16-Lead Lead Frame Chip Scale Package [LFCSP]	CP-16-17	
ADA4084-4ACPZ-RL	-40°C to +125°C	16-Lead Lead Frame Chip Scale Package [LFCSP]	CP-16-17	
ADA4084-4ARUZ	-40°C to +125°C	14-Lead Thin Shrink Small Outline Package [TSSOP]	RU-14	
ADA4084-4ARUZ-RL	-40°C to +125°C	14-Lead Thin Shrink Small Outline Package [TSSOP]	RU-14	

<sup>1</sup> Z = RoHS Compliant Part.