## Data Sheet

 AD8597/AD8599
## FEATURES

Low noise: $1.1 \mathrm{nV} / \sqrt{ } \mathrm{Hz}$ at 1 kHz Low distortion: - $\mathbf{1 2 0} \mathbf{d B}$ THD at $\mathbf{1 k H z}$
Input noise, 0.1 Hz to $10 \mathrm{~Hz}:<76 \mathrm{nV}$ p-p
Slew rate: $14 \mathrm{~V} / \mu \mathrm{s}$
Wide bandwidth: 10 MHz
Supply current: $\mathbf{4 . 8} \mathbf{~ m A / a m p ~ t y p i c a l ~}$
Low offset voltage: $10 \boldsymbol{\mu V}$ typical
CMRR: 120 dB
Unity-gain stable
$\pm 15$ V operation

## APPLICATIONS

Professional audio preamplifiers
ATE/precision testers
Imaging systems
Medical/physiological measurements
Precision detectors/instruments
Precision data conversion

## PIN CONFIGURATIONS



Figure 1. AD8597 8-Lead SOIC (R-8)


NOTES

1. NC = NO CONNECT.
2. IT IS RECOMMENDED THAT THE $\stackrel{\square}{\circ}$

EXPOSED PAD BE CONNECTED TO V-.
Figure 2. AD8597 8-Lead LFCSP (CP-8-13)

Figure 3. AD8599 8-Lead SOIC (R-8)


## GENERAL DESCRIPTION

The AD8597/AD8599 are very low noise, low distortion operational amplifiers ideal for use as preamplifiers. The low noise of $1.1 \mathrm{nV} / \sqrt{ } \mathrm{Hz}$ and low harmonic distortion of -120 dB (or better) at audio bandwidths give the AD8597/AD8599 the wide dynamic range necessary for preamplifiers in audio, medical, and instrumentation applications. The excellent slew rate of $14 \mathrm{~V} / \mu \mathrm{s}$ and 10 MHz gain bandwidth make them highly suitable for medical applications. The low distortion and fast settling time make them ideal for buffering of high resolution data converters.

The AD8597 is available in 8-lead SOIC and LFCSP packages, while the AD8599 is available in an 8 -lead SOIC package. They are both specified over a $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ temperature range. The AD8597 and AD8599 are members of a growing series of low noise op amps offered by Analog Devices, Inc. (see Table 1).

Table 1. Low Noise Op Amps

| Package | $\mathbf{0 . 9} \mathbf{n V}$ | $\mathbf{1 . 1} \mathbf{n V}$ | $\mathbf{1 . 8} \mathbf{n V}$ | $\mathbf{2 . 8} \mathbf{n V}$ | $\mathbf{3 . 8} \mathbf{n V}$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Single | AD797 | AD8597 | ADA4004-1 | AD8675 | AD8671 |
| Dual |  | AD8599 | ADA4004-2 | AD8676 | AD8672 |
| Quad |  |  | ADA4004-4 |  | AD8674 |

Rev. F

## AD8597/AD8599

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## SPECIFICATIONS

$\mathrm{V}_{\mathrm{SY}}= \pm 5 \mathrm{~V}, \mathrm{~V}_{\mathrm{CM}}=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{O}}=0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise specified.
Table 2.

| Parameter | Symbol | Conditions | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INPUT CHARACTERISTICS Offset Voltage | Vos | $-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C}$ |  | 15 | $\begin{aligned} & 120 \\ & 180 \end{aligned}$ | $\begin{aligned} & \mu \mathrm{V} \\ & \mu \mathrm{~V} \end{aligned}$ |
| Offset Voltage Drift Input Bias Current | $\begin{aligned} & \Delta \mathrm{V}_{\mathrm{os}} / \Delta \mathrm{T} \\ & \mathrm{I}_{\mathrm{B}} \end{aligned}$ | $\begin{aligned} & -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C} \\ & -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C} \end{aligned}$ |  | $\begin{aligned} & 0.8 \\ & 40 \end{aligned}$ | $\begin{aligned} & 2.2 \\ & 210 \\ & 340 \end{aligned}$ | $\begin{aligned} & \mu \mathrm{V} /{ }^{\circ} \mathrm{C} \\ & \mathrm{nA} \\ & \mathrm{nA} \end{aligned}$ |
| Input Offset Current | los | $-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C}$ |  | 65 | $\begin{aligned} & 250 \\ & 340 \end{aligned}$ | $\begin{aligned} & \mathrm{nA} \\ & \mathrm{nA} \end{aligned}$ |
| Input Voltage Range | IVR |  | -2.0 |  | +2.0 | V |
| Common-Mode Rejection Ratio | CMRR | $\begin{aligned} & -2.0 \mathrm{~V} \leq \mathrm{V}_{\mathrm{CM}} \leq+2.0 \mathrm{~V} \\ & -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C} \end{aligned}$ | $\begin{aligned} & 120 \\ & 105 \end{aligned}$ | 135 |  | dB <br> dB |
| Large Signal Voltage Gain | Avo | $\begin{aligned} & \mathrm{R}_{\mathrm{L}} \geq 600 \Omega, \mathrm{~V}_{\mathrm{O}}=-11 \mathrm{~V} \text { to }+11 \mathrm{~V} \\ & -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C} \end{aligned}$ | $\begin{aligned} & 105 \\ & 100 \end{aligned}$ | 110 |  | $\mathrm{dB}$ $\mathrm{dB}$ |
| Input Capacitance Differential Capacitance Common-Mode Capacitance | $\begin{aligned} & \mathrm{C}_{\text {DIFF }} \\ & \mathrm{C}_{\mathrm{CM}} \\ & \hline \end{aligned}$ |  |  | $\begin{aligned} & 15.4 \\ & 5.5 \end{aligned}$ |  | pF <br> pF |
| OUTPUT CHARACTERISTICS |  |  |  |  |  |  |
| Output Voltage High | Vor | $\begin{aligned} & \mathrm{R}_{\mathrm{L}}=600 \Omega \\ & -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C} \\ & \mathrm{R}_{\mathrm{L}}=2 \mathrm{k} \Omega \\ & -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C} \end{aligned}$ | $\begin{aligned} & 3.5 \\ & 3.3 \\ & 3.7 \\ & 3.5 \end{aligned}$ | $\begin{aligned} & 3.7 \\ & 3.8 \end{aligned}$ |  | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~V} \\ & \mathrm{~V} \\ & \mathrm{~V} \end{aligned}$ |
| Output Voltage Low | Vol | $\begin{aligned} & \mathrm{R}_{\mathrm{L}}=600 \Omega \\ & -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C} \\ & \mathrm{R}_{\mathrm{L}}=2 \mathrm{k} \Omega \\ & -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C} \end{aligned}$ |  | $\begin{aligned} & -3.6 \\ & -3.7 \end{aligned}$ | $\begin{aligned} & -3.4 \\ & -3.3 \\ & -3.5 \\ & -3.4 \end{aligned}$ | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~V} \\ & \mathrm{~V} \\ & \mathrm{~V} \end{aligned}$ |
| Output Short-Circuit Current Closed-Loop Output Impedance | $\begin{aligned} & \text { Isc } \\ & \text { Zout } \end{aligned}$ | At $1 \mathrm{MHz}, \mathrm{A}_{\mathrm{v}}=1$ |  | $\begin{aligned} & \pm 52 \\ & 5 \end{aligned}$ |  | $\begin{aligned} & \mathrm{mA} \\ & \Omega \end{aligned}$ |
| POWER SUPPLY <br> Power Supply Rejection Ratio <br> Supply Current per Amplifier | PSRR <br> Isy | $\begin{aligned} & \mathrm{V}_{\mathrm{SY}}= \pm 18 \mathrm{~V} \text { to } \pm 4.5 \mathrm{~V} \\ & -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C} \\ & -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C} \end{aligned}$ | $\begin{aligned} & 120 \\ & 118 \end{aligned}$ | $\begin{aligned} & 140 \\ & 4.8 \end{aligned}$ | $\begin{aligned} & 5.5 \\ & 6.5 \end{aligned}$ | dB <br> dB <br> mA <br> mA |
| DYNAMIC PERFORMANCE <br> Slew Rate <br> Settling Time <br> Gain Bandwidth Product Phase Margin | SR <br> ts <br> GBP <br> $Ф_{M}$ | $\begin{aligned} & A_{v}=-1, R_{L}=2 \mathrm{k} \Omega \\ & A_{V}=1, R_{L}=2 \mathrm{k} \Omega \\ & \text { To } 0.01 \% \text {, step }=10 \mathrm{~V} \end{aligned}$ |  | $\begin{aligned} & 14 \\ & 14 \\ & 2 \\ & 10 \\ & 60 \end{aligned}$ |  | $\mathrm{V} / \mu \mathrm{s}$ <br> V/ $\mu \mathrm{s}$ <br> $\mu \mathrm{s}$ <br> MHz <br> Degrees |
| NOISE PERFORMANCE <br> Peak-to-Peak Noise Voltage Noise Density <br> Correlated Current Noise <br> Uncorrelated Current Noise <br> Total Harmonic Distortion + Noise Channel Separation | $e_{n} p-p$ <br> $\mathrm{e}_{\mathrm{n}}$ $\begin{aligned} & \text { THD + N } \\ & \text { CS } \end{aligned}$ | $\begin{aligned} & 0.1 \mathrm{~Hz} \text { to } 10 \mathrm{~Hz} \\ & \mathrm{f}=1 \mathrm{kHz} \\ & \mathrm{f}=10 \mathrm{~Hz} \\ & \mathrm{f}=1 \mathrm{kHz} \\ & \mathrm{f}=10 \mathrm{~Hz} \\ & \mathrm{f}=1 \mathrm{kHz} \\ & \mathrm{f}=10 \mathrm{~Hz} \\ & \mathrm{G}=1, \mathrm{R} \geq 1 \mathrm{k} \Omega, \mathrm{f}=1 \mathrm{kHz}, \mathrm{~V}_{\mathrm{RMS}}=1 \mathrm{~V} \\ & \mathrm{f}=10 \mathrm{kHz} \end{aligned}$ |  | $\begin{aligned} & 76 \\ & 1.07 \\ & \\ & 2.0 \\ & 4.2 \\ & 2.4 \\ & 5.2 \\ & -120 \\ & -120 \end{aligned}$ | $\begin{aligned} & 1.15 \\ & 1.5 \end{aligned}$ | nV p-p <br> $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ <br> $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ <br> $\mathrm{pA} / \sqrt{ } \mathrm{Hz}$ <br> $\mathrm{pA} / \sqrt{ } \mathrm{Hz}$ <br> $\mathrm{pA} / \sqrt{ } \mathrm{Hz}$ <br> $\mathrm{pA} / \sqrt{ } \mathrm{Hz}$ <br> dB <br> dB |

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$\mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}, \mathrm{~V}_{\mathrm{CM}}=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{O}}=0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise specified.
Table 3.


## AD8597/AD8599

## ABSOLUTE MAXIMUM RATINGS

Table 4.

| Parameter | Rating |
| :--- | :--- |
| Supply Voltage | $\pm 18 \mathrm{~V}$ |
| Input Voltage | $-\mathrm{V} \leq \mathrm{V}$ IN $\leq+\mathrm{V}$ |
| Differential Input Voltage ${ }^{1}$ | $\pm 1 \mathrm{~V}$ |
| Output Short-Circuit to GND | Indefinite |
| Storage Temperature Range | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Operating Temperature Range | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| Lead Temperature Range (Soldering 60 sec$)$ | $300^{\circ} \mathrm{C}$ |
| Junction Temperature | $150^{\circ} \mathrm{C}$ |

${ }^{1}$ If the differential input voltage exceeds 1 V , limit the current to 5 mA .
Stresses at or above those listed under Absolute Maximum Ratings may cause permanent damage to the product. This is a stress rating only; functional operation of the product at these or any other conditions above those indicated in the operational section of this specification is not implied. Operation beyond the maximum operating conditions for extended periods may affect product reliability.

## THERMAL RESISTANCE

$\theta_{\mathrm{JA}}$ is specified with the device soldered on a circuit board with its exposed paddle soldered to a pad (if applicable) on a 4-layer JEDEC standard PCB with zero air flow.

Table 5.

| Package Type | $\boldsymbol{\theta}_{\mathbf{J A}}$ | $\boldsymbol{\theta}_{\mathbf{J c}}$ | Unit |
| :--- | :--- | :--- | :--- |
| 8-Lead LFCSP (CP-8-13) | 78 | 20 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| 8-Lead SOIC (R-8) (AD8597) | 140 | 39 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| 8-Lead SOIC (R-8) (AD8599) | 120 | 36 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

## POWER SEQUENCING

Apply the op amp supplies simultaneously. The op amp supplies must be stable before any input signals are applied. In any case, the input current must be limited to 5 mA .

## ESD CAUTION

|  | ESD (electrostatic discharge) sensitive device. <br> Charged devices and circuit boards can discharge <br> without detection. Although this product features <br> patented or proprietary protection circuitry, damage <br> may occur on devices subjected to high energy ESD. <br> Therefore, proper ESD precautions should be taken to <br> avoid performance degradation or loss of functionality. |
| :--- | :--- |

## TYPICAL PERFORMANCE CHARACTERISTICS

$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.


Figure 4. Input Offset Voltage Distribution


Figure 5. $\mathrm{TCV}_{\text {os }}$ Distribution, $-40^{\circ} \mathrm{C} \leq T_{A} \leq+125^{\circ} \mathrm{C}$


Figure 6. TCVos Distribution, $-40^{\circ} \mathrm{C} \leq T_{A} \leq+85^{\circ} \mathrm{C}$


Figure 7. Input Offset Voltage Distribution


Figure 8. TCV os Distribution, $-40^{\circ} \mathrm{C} \leq T_{A} \leq+125^{\circ} \mathrm{C}$


Figure 9. TCVos Distribution, $-40^{\circ} \mathrm{C} \leq T_{A} \leq+85^{\circ} \mathrm{C}$


Figure 10. Offset Voltage vs. VCM


Figure 11. Input Bias Current vs. Temperature


Figure 12. Input Offset Voltage vs. Temperature


Figure 13. Offset Voltage vs. $V_{C M}$


Figure 14. Input Bias Current vs. Temperature


Figure 15. Input Bias Current vs. Common-Mode Voltage (VCM) Over Temperature


Figure 16. Input Offset Current vs. Temperature


Figure 17. Large Signal Voltage Gain vs. Temperature


Figure 18. Supply Current vs. Supply Voltage


Figure 19. Input Offset Current vs. Temperature


Figure 20. Large Signal Voltage Gain vs. Temperature


Figure 21. Input Bias Current vs. VCM


Figure 22. Isc vs. Temperature


Figure 23. Output Dropout Voltage vs. Current Load


Figure 24. Output Saturation Voltage vs. Temperature


Figure 25. Isc vs. Temperature


Figure 26. Output Dropout Voltage vs. Current Load


Figure 27. Output Saturation Voltage vs. Temperature


Figure 28. Output Saturation Voltage vs. Temperature


Figure 29. Output Voltage Low vs. Temperature


Figure 30. Gain and Phase vs. Frequency


Figure 31. Output Saturation Voltage vs. Temperature


Figure 32. Output Voltage High vs. Temperature


Figure 33. Gain and Phase vs. Frequency


Figure 34. Closed-Loop Gain vs. Frequency


Figure 35. Closed-Loop Output Impedance vs. Frequency


Figure 36. Common-Mode Rejection Ratio vs. Frequency


Figure 37. Closed-Loop Gain vs. Frequency


Figure 38. Closed-Loop Output Impedance vs. Frequency


Figure 39. Power Supply Rejection Ratio vs. Frequency


Figure 40. Voltage Noise Density at 10 Hz


Figure 41. Voltage Noise Density vs. Frequency


Figure 42. $T H D+N$ vs. Amplitude


Figure 43. Voltage Noise Density at 1 kHz


Figure 44. Current Noise Density vs. Frequency


Figure 45. THD $+N$ vs. Amplitude


Figure 46. THD $+N$ vs. Frequency


Figure 47. Large Signal Response


Figure 48. Small Signal Response


Figure 49. THD + N vs. Frequency


Figure 50. Large Signal Response


Figure 51. Overshoot vs. Capacitance


Figure 52. Overshoot vs. Capacitive Load


Figure 53. Channel Separation vs. Frequency


Figure 54. Peak-to-Peak Noise


Figure 55. Overshoot vs. Capacitive Load


Figure 56. Supply Current vs. Temperature


Figure 57. Supply Current vs. Temperature

## FUNCTIONAL OPERATION

## INPUT VOLTAGE RANGE

The AD8597/AD8599 are not rail-to-rail input amplifiers; therefore, care is required to ensure that both inputs do not exceed the input voltage range. Under normal negative feedback operating conditions, the amplifier corrects its output to ensure that the two inputs are at the same voltage. However, if either input exceeds the input voltage range, the loop opens and large currents begin to flow through the ESD protection diodes in the amplifier.
These diodes are connected between the inputs and each supply rail to protect the input transistors against an electrostatic discharge event and they are normally reverse-biased. However, if the input voltage exceeds the supply voltage, these ESD diodes can become forward-biased. Without current limiting, excessive amounts of current may flow through these diodes, causing permanent damage to the device. If inputs are subject to overvoltage, insert appropriate series resistors to limit the diode current to less than 5 mA maximum.

The input stage has two diodes between the input pins to protect the differential pair. Under high slew rate conditions, when the op amp is connected as a voltage follower, the diodes may become forward-biased and the source may try to drive the output.
Place a small resistor in the feedback loop and in the noninverting input. The noise of a $100 \Omega$ resistor at room temperature is $\sim 1.25 \mathrm{nV} / \sqrt{ } \mathrm{Hz}$, which is higher than the AD8597/AD8599. Thus, there is a tradeoff between noise performance and protection. If possible, place limiting earlier in the signal path. For further details, see the Amplifier Input Protection... Friend or Foe? article at http://www.analog.com/amplifier_input.

Because of the large transistors used to achieve low noise, the input capacitance may seem rather high. To take advantage of the low noise performance, impedance around the op amp must be low, less than $500 \Omega$. Under these conditions, the pole from the input capacitance must be greater than 50 MHz , which does not affect the signal bandwidth.

## OUTPUT PHASE REVERSAL

Output phase reversal occurs in some amplifiers when the input common-mode voltage range is exceeded. As the common-mode voltage is moved outside the input voltage range, the outputs of these amplifiers can suddenly jump in the opposite direction to the supply rail. This is the result of the differential input pair shutting down that causes a radical shifting of internal voltages that results in the erratic output behavior.

The AD8597/AD8599 amplifiers are carefully designed to prevent any output phase reversal if both inputs are maintained within the specified input voltage range. If one or both inputs exceed the input voltage range but remain within the supply rails, the op amp specifications, such as CMRR, are not guaranteed, but the output remains close to the correct value.

## NOISE AND SOURCE IMPEDANCE CONSIDERATIONS

The AD8597/AD8599 ultralow voltage noise of $1.1 \mathrm{nV} / \sqrt{ } \mathrm{Hz}$ is achieved with special input transistors running at high collector current. Therefore, it is important to consider the total inputreferred noise ( $e_{\mathrm{N}}$ total), which includes contributions from voltage noise ( $\mathrm{e}_{\mathrm{N}}$ ), current noise ( $\mathrm{i}_{\mathrm{N}}$ ), and resistor noise ( $\sqrt{ } 4 \mathrm{kTR}_{\mathrm{S}}$ ).

$$
\begin{equation*}
e_{N} \text { total }=\left[e_{N}{ }^{2}+4 k T R_{S}+\left(i_{N} \times R S\right)^{2}\right]^{1 / 2} \tag{1}
\end{equation*}
$$

where $R_{s}$ is the total input source resistance.
This equation is plotted for the AD8597/AD8599 in Figure 58. Because optimum dc performance is obtained with matched source resistances, this case is considered even though it is clear from Equation 1 that eliminating the balancing source resistance lowers the total noise by reducing the total Rs by a factor of 2 .

At a very low source resistance ( $\mathrm{R}_{\mathrm{S}}<50 \Omega$ ), the voltage noise of the amplifier dominates. As source resistance increases, the Johnson noise of $R_{s}$ dominates until a higher resistance of $R_{s}>2 \mathrm{k} \Omega$ is achieved; the current noise component is larger than the resistor noise.


Figure 58. Noise vs. Source Resistance

## AD8597/AD8599

The AD8597/AD8599 are the optimum choice for low noise performance if the source resistance is kept $<1 \mathrm{k} \Omega$. At higher values of source resistance, optimum performance with respect to only noise is obtained with other amplifiers from Analog Devices. Both voltage noise and current noise must be considered. For more information on avoiding noise from grounding problems and inadequate bypassing, see the AN-345 Application Note, Grounding for Low- and High-Frequency Circuits. For
general noise theory with extensive calculations, see the AN-358 Application Note, Noise and Operational Amplifier Circuits. A good selection table for low noise op amps can be found in AN-940 Application Note, Low Noise Amplifier Selection Guide for Optimal Noise Performance. An interesting note on using one section of a monolithic dual to phase compensate the other section is in the AN-107 Application Note, Active Feedback Improves Amplifier Phase Accuracy.


## OUTLINE DIMENSIONS



ORDERING GUIDE

| Model $^{1}$ | Temperature Range | Package Description | Package Option | Branding |
| :--- | :--- | :--- | :--- | :--- |
| AD8597ACPZ-R2 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead Lead Frame Chip Scale Package [LFCSP] | CP-8-13 | A22 |
| AD8597ACPZ-REEL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead Lead Frame Chip Scale Package [LFCSP] | CP-8-13 | A22 |
| AD8597ACPZ-REEL7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead Lead Frame Chip Scale Package [LFCSP] | CP-8-13 | A22 |
| AD8597ARZ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8 -Lead Standard Small Outline Package [SOIC_N] | R-8 |  |
| AD8597ARZ-REEL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8 -Lead Standard Small Outline Package [SOIC_N] | R-8 |  |
| AD8597ARZ-REEL7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead Standard Small Outline Package [SOIC_N] | R-8 |  |
| AD8599ARZ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead Standard Small Outline Package [SOIC_N] | R-8 |  |
| AD8599ARZ-REEL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead Standard Small Outline Package [SOIC_N] | R-8 |  |
| AD8599ARZ-REEL7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead Standard Small Outline Package [SOIC_N] | R-8 |  |

[^0]NOTES
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NOTES

## NOTES


[^0]:    ${ }^{1} Z=$ RoHS Complaint Part.

