# Precision, Very Low Noise, Low Input Bias Current Operational Amplifiers 

## FEATURES

Very low noise: $\mathbf{2 . 8} \mathbf{n V} / \sqrt{ } \mathrm{Hz}, 77 \mathrm{nV}$ p-p
Wide bandwidth: 10 MHz
Low input bias current: 12 nA max
Low offset voltage: $\mathbf{7 5} \mu \mathrm{V}$ max
High open-loop gain: $\mathbf{1 2 0 ~ d B}$ min
Low supply current: 3 mA per amplifier
Dual-supply operation: $\pm 5 \mathrm{~V}$ to $\pm 15 \mathrm{~V}$
Unity-gain stable
No phase reversal

## APPLICATIONS

## PLL filters

Filters for GPS
Instrumentation
Sensors and controls
Professional quality audio

## GENERAL DESCRIPTION

The AD8671/AD8672/AD8674 are very high precision amplifiers featuring very low noise, very low offset voltage and drift, low input bias current, 10 MHz bandwidth, and low power consumption. Outputs are stable with capacitive loads of over 1000 pF . Supply current is less than 3 mA per amplifier at 30 V .

The AD8671/AD8672/AD8674's combination of ultralow noise, high precision, speed, and stability is unmatched. The MSOP version of the AD8671/AD8672 requires only half the board space of comparable amplifiers.

Applications for these amplifiers include high quality PLL filters, precision filters, medical and analytical instrumentation, precision power supply controls, ATE, data acquisition, and precision controls as well as professional quality audio.

The AD8671/AD8672/AD8674 are specified over the extended industrial temperature range $\left(-40^{\circ} \mathrm{C}\right.$ to $\left.+125^{\circ} \mathrm{C}\right)$.

The AD8671/AD8672 are available in the 8-lead SOIC and 8 -lead MSOP packages. The AD8674 is available in 14-lead SOIC and 14-lead TSSOP packages.

Surface-mount devices in MSOP packages are available in tape and reel only.

## Rev. C

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## AD8671/AD8672/AD8674

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## SPECIFICATIONS

## ELECTRICAL CHARACTERISTICS, $\pm \mathbf{5 . 0} \mathbf{V}$

$\mathrm{V}_{\mathrm{S}}= \pm 5.0 \mathrm{~V}, \mathrm{~V}_{\mathrm{CM}}=0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.
Table 1.


## AD8671/AD8672/AD8674

## ELECTRICAL CHARACTERISTICS, $\pm 15 \mathrm{~V}$

$\mathrm{V}_{\mathrm{S}}= \pm 15 \mathrm{~V}, \mathrm{~V}_{\mathrm{CM}}=0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.
Table 2.

| Parameter | Symbol | Conditions | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INPUT CHARACTERISTICS |  |  |  |  |  |  |
| Offset Voltage | Vos | $-40^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<+125^{\circ} \mathrm{C}$ |  | 20 | 75 | $\mu \mathrm{V}$ |
|  |  |  |  | 30 | 125 | $\mu \mathrm{V}$ |
| Offset Voltage Drift | $\Delta \mathrm{V}_{\text {os }} / \Delta \mathrm{T}$ | $-40^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<+125^{\circ} \mathrm{C}$ |  |  |  |  |
| AD8671 |  |  |  | 0.3 | 0.5 | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| AD8672/AD8674 |  |  |  | 0.3 | 0.8 | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Input Bias Current | $\mathrm{I}_{\mathrm{B}}$ |  | -12 | +3 | +12 | nA |
|  |  | $+25^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<+125^{\circ} \mathrm{C}$ | -20 | +5 | +20 | nA |
|  |  | $-40^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<+125^{\circ} \mathrm{C}$ | -40 | +8 | +40 | nA |
| Input Offset Current | los |  | -12 | +6 | +12 | nA |
|  |  | $+25^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<+125^{\circ} \mathrm{C}$ | -20 | +6 | +20 | nA |
|  |  | $-40^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<+125^{\circ} \mathrm{C}$ | -40 | +8 | +40 | nA |
| Input Voltage Range |  |  | -12 |  | +12 | V |
| Common-Mode Rejection Ratio | CMRR | $\mathrm{V}_{\text {cm }}=-12 \mathrm{~V}$ to +12 V | 100 | 120 |  | dB |
| Large Signal Voltage Gain | Avo | $\mathrm{R}_{\mathrm{L}}=2 \mathrm{k} \Omega, \mathrm{V}_{\mathrm{o}}=-10 \mathrm{~V}$ to +10 V | 1000 | 6000 |  | V/mV |
| Input Capacitance, Common Mode | CIncm |  |  | 6.25 |  | pF |
| Input Capacitance, Differential Mode | $\mathrm{C}_{\mathrm{INDM}}$ |  |  | 7.5 |  | pF |
| Input Resistance, Common Mode | $\mathrm{R}_{\mathrm{IN}}$ |  |  | 3.5 |  | G $\Omega$ |
| Input Resistance, Differential Mode | Rindm |  |  | 15 |  | $\mathrm{M} \Omega$ |
| OUTPUT CHARACTERISTICS |  |  |  |  |  |  |
| Output Voltage High | $\mathrm{V}_{\text {OH }}$ | $\mathrm{R}_{\mathrm{L}}=2 \mathrm{k} \Omega,-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | +13.2 | +13.8 |  | V |
| Output Voltage Low | Vol | $\mathrm{R}_{\mathrm{L}}=2 \mathrm{k} \Omega,-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |  | -13.8 | -13.2 | V |
| Output Voltage High | Vor | $\mathrm{R}_{\mathrm{L}}=600 \Omega$ | +11 | +12.3 |  | V |
| Output Voltage Low | Vol | $\mathrm{RL}=600 \Omega$ |  | -12.4 | -11 | V |
| Output Current | lout |  |  | $\pm 20$ |  | mA |
| Short Circuit Current | Isc |  |  | $\pm 30$ |  | mA |
| POWER SUPPLY |  |  |  |  |  |  |
| Power Supply Rejection Ratio AD8671/AD8672 | PSRR | $\mathrm{V}_{s}= \pm 4 \mathrm{~V}$ to $\pm 18 \mathrm{~V}$ | 110 106 | 130 115 |  | dB $d B$ |
| Supply Current/Amplifier | $\mathrm{I} Y$ | $\mathrm{V}_{\mathrm{O}}=0 \mathrm{~V}$ |  | 3 | 3.5 | mA |
|  |  | $-40^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<+125^{\circ} \mathrm{C}$ |  |  |  |  |
| DYNAMIC PERFORMANCE |  |  |  |  |  |  |
| Slew Rate | SR | $\mathrm{R}_{\mathrm{L}}=2 \mathrm{k} \Omega$ |  | 4 |  | V/ $/ \mathrm{s}$ |
| Settling Time | $\mathrm{ts}^{\text {s}}$ | To 0.1\% ( 10 V step, $\mathrm{G}=1$ ) |  | 2.2 |  |  |
|  |  | To 0.01\% ( 10 V step, $\mathrm{G}=1$ ) |  | 6.3 |  |  |
| Gain Bandwidth Product | GBP |  |  | 10 |  | MHz |
| NOISE PERFORMANCE |  |  |  |  |  |  |
| Peak-to-Peak Noise | $e_{n p-p}$ | 0.1 Hz to 10 Hz |  | 77 | 100 | $\mathrm{nV} \mathrm{p}-\mathrm{p}$ |
| Voltage Noise Density | $\mathrm{e}_{\mathrm{n}}$ | $\mathrm{f}=1 \mathrm{kHz}$ |  | 2.8 | 3.8 | $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ |
| Current Noise Density | $\mathrm{in}_{n}$ | $\mathrm{f}=1 \mathrm{kHz}$ |  | 0.3 |  | $\mathrm{pA} / \sqrt{ } \mathrm{Hz}$ |
| Channel SeparationAD8672/AD8674 |  |  |  |  |  |  |
|  | $\mathrm{C}_{5}$ | $\begin{aligned} & \mathrm{f}=1 \mathrm{kHz} \\ & \mathrm{f}=10 \mathrm{kHz} \end{aligned}$ |  | -130 |  | dB |
|  |  |  |  | -105 |  | dB |

## AD8671/AD8672/AD8674

## ABSOLUTE MAXIMUM RATINGS

Table 3. ${ }^{1}$

| Parameter | Rating |
| :--- | :--- |
| Supply Voltage | 36 V |
| Input Voltage | $\mathrm{V}_{s}-$ to Vs+ |
| Differential Input Voltage | $\pm 0.7 \mathrm{~V}$ |
| Output Short-Circuit Duration | Indefinite |
| Storage Temperature Range |  |
| $\quad$ All Packages | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Operating Temperature Range |  |
| $\quad$ All Packages | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| Junction Temperature Range |  |
| $\quad$ All Packages | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Lead Temperature Range (Soldering, 60 sec$)$ | $300^{\circ} \mathrm{C}$ |

${ }^{1}$ Absolute maximum ratings apply at $25^{\circ} \mathrm{C}$, unless otherwise noted.

Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

Table 4. Package Characteristics

| Package Type | $\boldsymbol{\theta}_{\text {JA }}{ }^{1}$ | $\boldsymbol{\theta}_{\text {Jc }}$ | Unit |
| :--- | :--- | :--- | :--- |
| 8-Lead MSOP (RM) | 190 | 44 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| 8-Lead SOIC_N (R) | 158 | 43 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| 14-Lead SOIC_N (R) | 120 | 36 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| 14-Lead TSSOP (RU) | 180 | 35 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

${ }^{1} \theta_{\mathrm{JA}}$ is specified for the worst-case conditions, that is., $\theta_{\mathrm{JA}}$ is specified for the device soldered in circuit board for surface-mount packages.

## ESD CAUTION

ESD (electrostatic discharge) sensitive device. Electrostatic charges as high as 4000 V readily accumulate on the human body and test equipment and can discharge without detection. Although this product features proprietary ESD protection circuitry, permanent damage may occur on devices subjected to high energy electrostatic discharges. Therefore, proper ESD precautions are recommended to avoid performance degradation or loss of functionality.

## AD8671/AD8672/AD8674

## TYPICAL PERFORMANCE CHARACTERISTICS



Figure 7. Voltage Noise Density vs. Frequency


Figure 8. Voltage Noise Density vs. Frequency


Figure 9. Voltage Noise Density vs. Frequency


Figure 10. Input Offset Voltage Distribution


Figure 11. Input Offset Voltage Distribution


Figure 12. Input Offset Voltage vs. Temperature

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Figure 13. Input Bias Current vs. Temperature


Figure 14. Input Bias Current vs. Temperature


Figure 15. Supply Current vs. Temperature


Figure 16. Output Voltage High vs. Temperature


Figure 17. Output Voltage Low vs. Temperature


Figure 18. Open-Loop Gain and Phase Shift vs. Frequency

## AD8671/AD8672/AD8674



Figure 19. Open-Loop Gain vs. Temperature


Figure 20. Closed-Loop Gain vs. Frequency


Figure 21. Output Impedance vs. Frequency


Figure 22. Large Signal Transient Response


Figure 23. Small Signal Transient Response


Figure 24. Small Signal Overshoot vs. Load Capacitance

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Figure 25. Positive Overdrive Recovery


Figure 26. Negative Overdrive Recovery


Figure 27. CMRR vs. Frequency


Figure 28. PSRR vs. Frequency


Figure 29. PSRR vs. Temperature


Figure 30. 0.1 Hz to 10 Hz Input Voltage Noise

## AD8671/AD8672/AD8674



Figure 31. Channel Separation

## APPLICATIONS

## UNITY-GAIN FOLLOWER APPLICATIONS

When large transient pulses ( $>1 \mathrm{~V}$ ) are applied at the positive terminal of amplifiers (such as the OP27, LT1007, OPA227, and AD8671) with back-to-back diodes at the input stage, the use of a resistor in the feedback loop is recommended to avoid having the amplifier load the signal generator. The feedback resistor, $\mathrm{R}_{\mathrm{F}}$, should be at least $500 \Omega$. However, if large values must be used for $\mathrm{R}_{\mathrm{F}}$, a small capacitor, $\mathrm{C}_{\mathrm{F}}$, should be inserted in parallel with $R_{F}$ to compensate for the pole introduced by the input capacitance and $\mathrm{R}_{\mathrm{F}}$.

Figure 32 shows the uncompensated output response with a $10 \mathrm{k} \Omega$ resistor in the feedback and the compensated response with $\mathrm{C}_{\mathrm{F}}=15 \mathrm{pF}$.


Figure 32. Transient Output Response

## OUTPUT PHASE REVERSAL

Phase reversal is a change of polarity in the amplifier transfer function that occurs when the input voltage exceeds the supply voltage. The AD8671/AD8672/AD8674 do not exhibit phase reversal even when the input voltage is 1 V beyond the supplies.


## TOTAL NOISE VS. SOURCE RESISTANCE

The low input voltage noise of the AD8671/AD8672/AD8674 makes them a great choice for applications with low source resistance. However, because they have low input current noise, they can also be used in circuits with substantial source resistance.

Figure 34 shows the voltage noise, current noise, thermal noise, and total rms noise of the AD8671 as a function of the source resistance.

For $\mathrm{R}_{\mathrm{S}}<475 \Omega$, the input voltage noise, $\mathrm{e}_{\mathrm{n}}$, dominates. For $475 \Omega<\mathrm{R}_{\mathrm{s}}<412 \mathrm{k} \Omega$, thermal noise dominates. For $\mathrm{R}_{\mathrm{s}}>412 \mathrm{k} \Omega$, the input current noise dominates.


Figure 34. Noise vs. Source Resistance

## AD8671/AD8672/AD8674

## TOTAL HARMONIC DISTORTION (THD) AND NOISE

The AD8671/AD8672/AD8674 exhibit low total harmonic distortion (THD) over the entire audio frequency range. This makes them suitable for applications with high closed-loop gains, including audio applications. Figure 35 shows approximately $0.0006 \%$ of THD +N in a positive unity gain, the worst-case configuration for distortion.


Figure 35. Total Harmonic Distortion and Noise

## DRIVING CAPACITIVE LOADS

The AD8671/AD8672/AD8674 can drive large capacitive loads without causing instability. However, when configured in unity gain, driving very large loads can cause unwanted ringing or instability.

Figure 36 shows the output of the AD8671 with a capacitive load of 1 nF . If heavier loads are used in low closed-loop gain or unity-gain configurations, it is recommended to use external compensation as shown in the circuit in Figure 37. This technique reduces the overshoot and prevents the op amp from oscillation. The trade-off of this circuit is a reduction in output swing. However, a great added benefit stems from the fact that the input signal and the op amp's noise are filtered, and thus the overall output noise is kept to a minimum.

The output response of the circuit is shown in Figure 38.


Figure 36. AD8671 Capacitive Load Drive


Figure 37. Recommended Capacitive Load Circuit



Figure 39. Simplified Block Diagram of a GPS Receiver

## GPS RECEIVER

GPS receivers require low noise to minimize RF effects. The precision of the AD8671 makes it an excellent choice for such applications. Its very low noise and wide bandwidth make it suitable for band-pass and low-pass filters without the penalty of high power consumption.

Figure 39 shows a simplified block diagram of a GPS receiver. The next section details the design equations.

## BAND-PASS FILTER

Filters are useful in many applications; for example, band-pass filters are used in GPS systems, as discussed in the previous section. Figure 40 shows a second-order band-pass KRC filter.


Figure 40. Band-Pass KRC Filter
The equal component topology yields a center frequency

$$
\begin{aligned}
& f o=\frac{\sqrt{2}}{2 \pi R C} \\
& \text { and } Q=\frac{\sqrt{2}}{4-K}
\end{aligned}
$$

where:

$$
K=1+\frac{R_{B}}{R_{A}}
$$

The band-pass response is shown in Figure 41.


Figure 41. Band-Pass Response

## PLL SYNTHESIZERS AND LOOP FILTERS

Phase-lock loop filters are used in AM/FM modulation.
Loop filters in PLL design require accuracy and care in their implementation. The AD8671/AD8672/AD8674 are ideal candidates for such filter design; the low offset voltage and low input bias current minimize the output error. In addition to the excellent dc specifications, the AD8671/AD8672/AD8674 have a unique performance at high frequencies; the high open-loop gain and wide bandwidth allow the user to design a filter with a high closed-loop gain if desirable. To optimize the filter design, it is recommended to use small value resistors to minimize the thermal noise. A simple example is shown in Figure 42.


Figure 42. PLL Filter Simplified Block Diagram

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## OUTLINE DIMENSIONS



Figure 44. 8-Lead Mini Small Outline Package [MSOP] (RM-8)
Dimensions shown in millimeters


Figure 46. 14-Lead Thin Shrink Small Outline Package [TSSOP] ( $R U-14$ )
Dimensions shown in millimeters

## AD8671/AD8672/AD8674

ORDERING GUIDE

| Model | Temperature Range | Package Description | Package Option | Branding |
| :---: | :---: | :---: | :---: | :---: |
| AD8671AR | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8671AR-REEL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8671AR-REEL7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8671ARZ ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8671ARZ-REEL ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8671ARZ-REEL71 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8671ARM-R2 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead MSOP | RM-8 | BGA |
| AD8671ARM-REEL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead MSOP | RM-8 | BGA |
| AD8671ARMZ-R2 ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead MSOP | RM-8 | AOV |
| AD8671ARMZ-REEL ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead MSOP | RM-8 | AOV |
| AD8672AR | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8672AR-REEL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8672AR-REEL7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8672ARZ ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8672ARZ-REEL ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8672ARZ-REEL7 ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8672ARM-R2 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead MSOP | RM-8 | BHA |
| AD8672ARM-REEL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead MSOP | RM-8 | BHA |
| AD8672ARMZ-R2 ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead MSOP | RM-8 | AOW |
| AD8672ARMZ-REEL ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead MSOP | RM-8 | A0W |
| AD8674AR | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 14-Lead SOIC_N | R-14 |  |
| AD8674AR-REEL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 14-Lead SOIC_N | R-14 |  |
| AD8674AR-REEL7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 14-Lead SOIC_N | R-14 |  |
| AD8674ARZ ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 14-Lead SOIC_N | R-14 |  |
| AD8674ARZ-REEL ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 14-Lead SOIC_N | R-14 |  |
| AD8674ARZ-REEL71 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 14-Lead SOIC_N | R-14 |  |
| AD8674ARU | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 14-Lead TSSOP | RU-14 |  |
| AD8674ARU-REEL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 14-Lead TSSOP | RU-14 |  |
| AD8674ARUZ ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 14-Lead TSSOP | RU-14 |  |
| AD8674ARUZ-REEL ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 14-Lead TSSOP | RU-14 |  |

${ }^{1} \mathrm{Z}=\mathrm{Pb}$-free part.
$\square$

