## Data Sheet

## FEATURES

Operating frequency from $100 \mathbf{~ M H z}$ to $\mathbf{4 0 0 0} \mathbf{~ M H z}$
Digitally controlled VGA with serial and parallel interfaces
6-bit, 0.5 dB digital step attenuator
31.5 dB gain control range with $\pm 0.25 \mathrm{~dB}$ step accuracy

Gain Block Amplifier 1
Gain: $\mathbf{1 9 . 2} \mathbf{~ d B}$ at 2140 MHz
OIP3: $\mathbf{4 0 . 2 \mathrm { dBm } \text { at } 2 1 4 0 \mathrm { MHz } , ~}$
P1dB: $19.8 \mathbf{d B m}$ at 2140 MHz
Noise figure: $\mathbf{2 . 9} \mathbf{~ d B}$ at $\mathbf{2 1 4 0} \mathbf{~ M H z}$
1/4 W Driver Amplifier 2
Gain: $\mathbf{1 4 . 2} \mathbf{~ d B}$ at $2140 \mathbf{M H z}$
OIP3: $\mathbf{4 1 . 1} \mathbf{d B m}$ at 2140 MHz
P1dB: $\mathbf{2 6 . 0 ~ d B m}$ at 2140 MHz
Noise figure: $\mathbf{3 . 7} \mathbf{~ d B}$ at $\mathbf{2 1 4 0 ~ M H z}$
Gain block, DSA, or $1 / 4 \mathbf{W}$ driver amplifier can be first
Low quiescent current of 175 mA
The companion ADL5240 integrates a gain block with DSA

## APPLICATIONS

## Wireless infrastructure

Automated test equipment
RF/IF gain control

## GENERAL DESCRIPTION

The ADL5243 is a high performance, digitally controlled variable gain amplifier operating from 100 MHz to 4000 MHz .

The VGA integrates two high performance amplifiers and a digital step attenuator (DSA). Amplifier 1 (AMP1) is an internally matched gain block amplifier with 20 dB gain, and Amplifier 2 (AMP2) is a broadband $1 / 4 \mathrm{~W}$ driver amplifier that requires very few external tuning components. The DSA is 6-bit with a 31.5 dB gain control range, 0.5 dB steps, and $\pm 0.25 \mathrm{~dB}$ step accuracy. The attenuation of the DSA can be controlled using a serial or parallel interface.

The gain block and DSA are internally matched to $50 \Omega$ at their inputs and outputs, and all three internal devices are separately biased. The separate bias allows all or part of the ADL5243 to be used, which allows for easy reuse throughout a design. The pinout of the ADL5243 also enables the gain block, DSA, or $1 / 4 \mathrm{~W}$ driver amplifier to be first, giving the VGA maximum flexibility in a signal chain.
The ADL5243 consumes 175 mA and operates off a single supply ranging from 4.75 V to 5.25 V . The VGA is packaged in a thermally efficient, $5 \mathrm{~mm} \times 5 \mathrm{~mm}, 32$-lead LFCSP and is fully specified for operation from $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$. A fully populated evaluation board is available.


Figure 1.
Rev. B
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## SPECIFICATIONS

$\mathrm{VDD}=5 \mathrm{~V}, \mathrm{VCC}=5 \mathrm{~V}, \mathrm{VCC} 2=5 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$.
Table 1.

\begin{tabular}{|c|c|c|c|c|c|}
\hline Parameter \& Conditions \& Min \& Typ \& Max \& Unit \\
\hline OVERALL FUNCTION Frequency Range \& \& 100 \& \& 4000 \& MHz \\
\hline \begin{tabular}{l}
AMPLIFIER 1 FREQUENCY \(=150 \mathrm{MHz}\) \\
Gain \\
vs. Frequency \\
vs. Temperature \\
vs. Supply \\
Input Return Loss \\
Output Return Loss \\
Output 1 dB Compression Point Output Third-Order Intercept Noise Figure
\end{tabular} \& Using the AMP1IN and AMP1OUT pins
\[
\begin{aligned}
\& \pm 50 \mathrm{MHz} \\
\& -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C} \\
\& 4.75 \mathrm{~V} \text { to } 5.25 \mathrm{~V} \\
\& \mathrm{~S} 11 \\
\& \mathrm{~S} 22
\end{aligned}
\]
\[
\Delta \mathrm{f}=1 \mathrm{MHz} \text {, Pout }=3 \mathrm{dBm} / \text { tone }
\] \& \& \[
\begin{aligned}
\& 18.2 \\
\& \pm 0.97 \\
\& \pm 0.07 \\
\& \pm 0.03 \\
\& -10.4 \\
\& -8.2 \\
\& 18.4 \\
\& 29.5 \\
\& 2.8
\end{aligned}
\] \& \& \begin{tabular}{l}
dB \\
dB \\
dB \\
dB \\
dB \\
dB \\
dBm \\
dBm \\
dB
\end{tabular} \\
\hline \begin{tabular}{l}
AMPLIFIER 1 FREQUENCY \(=450 \mathrm{MHz}\) \\
Gain \\
vs. Frequency \\
vs. Temperature \\
vs. Supply \\
Input Return Loss \\
Output Return Loss \\
Output 1 dB Compression Point \\
Output Third-Order Intercept \\
Noise Figure
\end{tabular} \& \begin{tabular}{l}
Using the AMP1IN and AMP1OUT pins
\[
\begin{aligned}
\& \pm 50 \mathrm{MHz} \\
\& -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C} \\
\& 4.75 \mathrm{~V} \text { to } 5.25 \mathrm{~V} \\
\& \text { S11 } \\
\& \text { S22 }
\end{aligned}
\] \\
\(\Delta \mathrm{f}=1 \mathrm{MHz}\), Pout \(=3 \mathrm{dBm} /\) tone
\end{tabular} \& \& \[
\begin{aligned}
\& 20.6 \\
\& \pm 0.10 \\
\& \pm 0.36 \\
\& \pm 0.01 \\
\& -17.8 \\
\& -16.5 \\
\& 19.5 \\
\& 38.4 \\
\& 2.8
\end{aligned}
\] \& \& \begin{tabular}{l}
dB \\
dB \\
dB \\
dB \\
dB \\
dB \\
dBm \\
dBm \\
dB
\end{tabular} \\
\hline \begin{tabular}{l}
AMPLIFIER 1 FREQUENCY \(=748 \mathrm{MHz}\) \\
Gain \\
vs. Frequency \\
vs. Temperature \\
vs. Supply \\
Input Return Loss \\
Output Return Loss \\
Output 1 dB Compression Point Output Third-Order Intercept Noise Figure
\end{tabular} \& \begin{tabular}{l}
Using the AMP1IN and AMP1OUT pins
\[
\begin{aligned}
\& \pm 50 \mathrm{MHz} \\
\& -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C} \\
\& 4.75 \mathrm{~V} \text { to } 5.25 \mathrm{~V} \\
\& \mathrm{~S} 11 \\
\& \mathrm{~S} 22
\end{aligned}
\] \\
\(\Delta \mathrm{f}=1 \mathrm{MHz}\), Pout \(=3 \mathrm{dBm} /\) tone
\end{tabular} \& \& \[
\begin{aligned}
\& 20.8 \\
\& \pm 0.02 \\
\& \pm 0.32 \\
\& \pm 0.01 \\
\& -22.0 \\
\& -21.6 \\
\& 19.6 \\
\& 39.6 \\
\& 2.7
\end{aligned}
\] \& \& \begin{tabular}{l}
dB \\
dB \\
dB \\
dB \\
dB \\
dB \\
dBm \\
dBm \\
dB
\end{tabular} \\
\hline \begin{tabular}{l}
AMPLIFIER 1 FREQUENCY \(=943 \mathrm{MHz}\) \\
Gain \\
vs. Frequency \\
vs. Temperature \\
vs. Supply \\
Input Return Loss \\
Output Return Loss \\
Output 1 dB Compression Point \\
Output Third-Order Intercept \\
Noise Figure
\end{tabular} \& \begin{tabular}{l}
Using the AMP1IN and AMP1OUT pins
\[
\begin{aligned}
\& \pm 18 \mathrm{MHz} \\
\& -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C} \\
\& 4.75 \mathrm{~V} \text { to } 5.25 \mathrm{~V} \\
\& \text { S11 } \\
\& \mathrm{S} 22
\end{aligned}
\] \\
\(\Delta f=1 \mathrm{MHz}\), Pout \(=3 \mathrm{dBm} /\) tone
\end{tabular} \& 19.0

18.5 \& \[
$$
\begin{aligned}
& 20.3 \\
& \pm 0.01 \\
& \pm 0.28 \\
& \pm 0.02 \\
& -24.0 \\
& -21.5 \\
& 19.9 \\
& 40.4 \\
& 2.7
\end{aligned}
$$

\] \& 22.0 \& | dB |
| :--- |
| dB |
| dB |
| dB |
| dB |
| dB |
| dBm |
| dBm |
| dB | <br>

\hline
\end{tabular}

## ADL5243

\begin{tabular}{|c|c|c|c|c|c|}
\hline Parameter \& Conditions \& Min \& Typ \& Max \& Unit \\
\hline \begin{tabular}{l}
AMPLIFIER 1 FREQUENCY \(=1960 \mathrm{MHz}\) \\
Gain \\
vs. Frequency \\
vs. Temperature \\
vs. Supply \\
Input Return Loss \\
Output Return Loss \\
Output 1 dB Compression Point Output Third-Order Intercept Noise Figure
\end{tabular} \& \begin{tabular}{l}
Using the AMP1IN and AMP1OUT pins
\[
\begin{aligned}
\& \pm 30 \mathrm{MHz} \\
\& -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C} \\
\& 4.75 \mathrm{~V} \text { to } 5.25 \mathrm{~V} \\
\& \mathrm{~S} 11 \\
\& \mathrm{~S} 22
\end{aligned}
\] \\
\(\Delta f=1 \mathrm{MHz}\), Pout \(=3 \mathrm{dBm} /\) tone
\end{tabular} \& \& \[
\begin{aligned}
\& 19.5 \\
\& \pm 0.02 \\
\& \pm 0.26 \\
\& \pm 0.04 \\
\& -13.5 \\
\& -12.4 \\
\& 19.6 \\
\& 40.4 \\
\& 2.9
\end{aligned}
\] \& \& \begin{tabular}{l}
dB \\
dB \\
dB \\
dB \\
dB \\
dB \\
dBm \\
dBm \\
dB
\end{tabular} \\
\hline ```
AMPLIFIER 1 FREQUENCY = 2140 MHz
Gain
vs. Frequency
vs. Temperature
vs.Supply
Input Return Loss
Output Return Loss
Output 1 dB Compression Point
Output Third-Order Intercept
Noise Figure
``` \& \begin{tabular}{l}
Using the AMP1IN and AMP1OUT pins
\[
\begin{aligned}
\& \pm 30 \mathrm{MHz} \\
\& -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C}
\end{aligned}
\] \\
4.75 V to 5.25 V \\
S11 \\
S22 \\
\(\Delta \mathrm{f}=1 \mathrm{MHz}\), Pout \(=3 \mathrm{dBm} /\) tone
\end{tabular} \& \[
17.5
\]
\[
17.5
\] \& \[
\begin{aligned}
\& 19.2 \\
\& \pm 0.02 \\
\& \pm 0.26 \\
\& \pm 0.05 \\
\& -13.3 \\
\& -12.2 \\
\& 19.8 \\
\& 40.2 \\
\& 2.9
\end{aligned}
\] \& 21.5 \& \begin{tabular}{l}
dB \\
dB \\
dB \\
dB \\
dB \\
dB \\
dBm \\
dBm \\
dB
\end{tabular} \\
\hline ```
AMPLIFIER 1 FREQUENCY = 2630 MHz
Gain
vs. Frequency
vs. Temperature
vs. Supply
Input Return Loss
Output Return Loss
Output 1 dB Compression Point
Output Third-Order Intercept
Noise Figure
``` \& \begin{tabular}{l}
Using the AMP1IN and AMP1OUT pins
\[
\begin{aligned}
\& \pm 60 \mathrm{MHz} \\
\& -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C}
\end{aligned}
\] \\
4.75 V to 5.25 V \\
S11 \\
S22
\[
\Delta \mathrm{f}=1 \mathrm{MHz}, \text { Pout }=3 \mathrm{dBm} / \text { tone }
\]
\end{tabular} \& 17.5

17.5 \& \[
$$
\begin{aligned}
& 19.0 \\
& \pm 0.03 \\
& \pm 0.22 \\
& \pm 0.05 \\
& -17.3 \\
& -12.3 \\
& 19.5 \\
& 39.5 \\
& 2.9
\end{aligned}
$$

\] \& 21.5 \& | dB |
| :--- |
| dB |
| dB |
| dB |
| dB |
| dB |
| dBm |
| dBm |
| dB | <br>


\hline | AMPLIFIER 1 FREQUENCY $=3600 \mathrm{MHz}$ |
| :--- |
| Gain |
| vs. Frequency |
| vs. Temperature |
| vs. Supply |
| Input Return Loss |
| Output Return Loss |
| Output 1 dB Compression Point |
| Output Third-Order Intercept |
| Noise Figure | \& | Using the AMP1IN and AMP1OUT pins $\begin{aligned} & \pm 100 \mathrm{MHz} \\ & -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C} \\ & 4.75 \mathrm{~V} \text { to } 5.25 \mathrm{~V} \\ & \text { S11 } \\ & \text { S22 } \end{aligned}$ |
| :--- |
| $\Delta f=1 \mathrm{MHz}$, Pout $=3 \mathrm{dBm} /$ tone | \& \& \[

$$
\begin{aligned}
& 18.0 \\
& \pm 0.10 \\
& \pm 0.05 \\
& \pm 0.12 \\
& -30.7 \\
& -9.0 \\
& 18.0 \\
& 34.6 \\
& 3.3
\end{aligned}
$$

\] \& \& | dB |
| :--- |
| dB |
| dB |
| dB |
| dB |
| dB |
| dBm |
| dBm |
| dB | <br>


\hline | AMPLIFIER 2 FREQUENCY $=150 \mathrm{MHz}$ |
| :--- |
| Gain |
| vs. Frequency |
| vs. Temperature |
| vs. Supply |
| Input Return Loss |
| Output Return Loss |
| Output 1 dB Compression Point Output Third-Order Intercept Noise Figure | \& Using the AMP2IN and AMP2OUT pins

$$
\begin{aligned}
& \pm 50 \mathrm{MHz} \\
& -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C} \\
& 4.75 \mathrm{~V} \text { to } 5.25 \mathrm{~V} \\
& \mathrm{~S} 11 \\
& \mathrm{~S} 22
\end{aligned}
$$

$$
\Delta \mathrm{f}=1 \mathrm{MHz} \text {, Pout }=5 \mathrm{dBm} / \text { tone }
$$ \& \& \[

$$
\begin{aligned}
& 20.8 \\
& \pm 1.1 \\
& \pm 0.3 \\
& \pm 0.03 \\
& -11.0 \\
& -6.5 \\
& 22.8 \\
& 40.6 \\
& 6.3
\end{aligned}
$$

\] \& \& | dB |
| :--- |
| dB |
| dB |
| dB |
| dB |
| dB |
| dBm |
| dBm |
| dB | <br>

\hline
\end{tabular}

| Parameter | Conditions | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: |
| AMPLIFIER 2 FREQUENCY $=450 \mathrm{MHz}$ <br> Gain <br> vs. Frequency <br> vs. Temperature <br> vs. Supply <br> Input Return Loss <br> Output Return Loss <br> Output 1 dB Compression Point <br> Output Third-Order Intercept <br> Noise Figure | Using the AMP2IN and AMP2OUT pins $\begin{aligned} & \pm 50 \mathrm{MHz} \\ & -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C} \\ & 4.75 \mathrm{~V} \text { to } 5.25 \mathrm{~V} \\ & \mathrm{~S} 11 \\ & \mathrm{~S} 22 \end{aligned}$ <br> $\Delta \mathrm{f}=1 \mathrm{MHz}$, Pout $=5 \mathrm{dBm} /$ tone |  | $\begin{aligned} & 16.4 \\ & \pm 0.5 \\ & \pm 0.35 \\ & \pm 0.07 \\ & -9.0 \\ & -8.0 \\ & 23.2 \\ & 38.1 \\ & 6.2 \end{aligned}$ |  | dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dBm <br> dBm <br> dB |
| ```AMPLIFIER 2 FREQUENCY \(=748 \mathrm{MHz}\) Gain vs. Frequency Input Return Loss Output Return Loss Output 1 dB Compression Point Output Third-Order Intercept Noise Figure``` | Using the AMP2IN and AMP2OUT pins $\begin{aligned} & \pm 50 \mathrm{MHz} \\ & \mathrm{~S} 11 \\ & \mathrm{~S} 22 \end{aligned}$ $\Delta \mathrm{f}=1 \mathrm{MHz} \text {, Pout }=5 \mathrm{dBm} / \text { tone }$ |  | $\begin{aligned} & 17.5 \\ & \pm 0.14 \\ & -14 \\ & -8.6 \\ & 24.7 \\ & 41.5 \\ & 5.6 \\ & \hline \end{aligned}$ |  | dB <br> dB <br> dB <br> dB <br> dBm <br> dBm <br> dB |
| ```AMPLIFIER 2 FREQUENCY \(=943 \mathrm{MHz}\) Gain vs. Frequency vs. Temperature vs. Supply Input Return Loss Output Return Loss Output 1 dB Compression Point Output Third-Order Intercept Noise Figure``` | Using the AMP2IN and AMP2OUT pins $\begin{aligned} & \pm 18 \mathrm{MHz} \\ & -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C} \end{aligned}$ <br> 4.75 V to 5.25 V <br> S11 <br> S22 <br> $\Delta \mathrm{f}=1 \mathrm{MHz}$, Pout $=5 \mathrm{dBm} /$ tone |  | $\begin{aligned} & 16.5 \\ & \pm 0.05 \\ & \pm 0.39 \\ & \pm 0.10 \\ & -11.2 \\ & -8.1 \\ & 25.0 \\ & 43.3 \\ & 5.3 \\ & \hline \end{aligned}$ |  | dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dBm <br> dBm dB |
| ```AMPLIFIER 2 FREQUENCY = 1960 MHz Gain vs. Frequency Input Return Loss Output Return Loss Output 1 dB Compression Point Output Third-Order Intercept Noise Figure``` | Using the AMP2IN and AMP2OUT pins $\begin{aligned} & \pm 30 \mathrm{MHz} \\ & \mathrm{~S} 11 \\ & \mathrm{~S} 22 \end{aligned}$ $\Delta \mathrm{f}=1 \mathrm{MHz} \text {, Pout }=5 \mathrm{dBm} / \text { tone }$ |  | $\begin{aligned} & 14.9 \\ & \pm 0.15 \\ & -14 \\ & -7.0 \\ & 26.0 \\ & 39.9 \\ & 3.73 \end{aligned}$ |  | dB <br> dB <br> dB <br> dB <br> dBm <br> dBm <br> dB |
| ```AMPLIFIER 2 FREQUENCY \(=2140 \mathrm{MHz}\) Gain vs. Frequency vs. Temperature vs. Supply Input Return Loss Output Return Loss Output 1 dB Compression Point Output Third-Order Intercept Noise Figure``` | Using the AMP2IN and AMP2OUT pins $\begin{aligned} & \pm 30 \mathrm{MHz} \\ & -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C} \\ & 4.75 \mathrm{~V} \text { to } 5.25 \mathrm{~V} \\ & \text { S11 } \\ & \text { S22 } \end{aligned}$ $\Delta \mathrm{f}=1 \mathrm{MHz} \text {, Pout }=5 \mathrm{dBm} / \text { tone }$ | 13.0 | $\begin{aligned} & 14.2 \\ & \pm 0.03 \\ & \pm 0.50 \\ & \pm 0.09 \\ & -10.7 \\ & -8.1 \\ & 26.0 \\ & 41.1 \\ & 3.7 \end{aligned}$ | 15.5 | dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dBm <br> dBm <br> dB |

## ADL5243

| Parameter | Conditions | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: |
| AMPLIFIER 2 FREQUENCY $=2630 \mathrm{MHz}$ <br> Gain <br> vs. Frequency <br> vs. Temperature <br> vs. Supply <br> Input Return Loss <br> Output Return Loss <br> Output 1 dB Compression Point <br> Output Third-Order Intercept <br> Noise Figure | Using the AMP2IN and AMP2OUT pins $\begin{aligned} & \pm 60 \mathrm{MHz} \\ & -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C} \\ & 4.75 \mathrm{~V} \text { to } 5.25 \mathrm{~V} \\ & \mathrm{~S} 11 \\ & \mathrm{~S} 22 \end{aligned}$ $\Delta \mathrm{f}=1 \mathrm{MHz} \text {, Pout }=5 \mathrm{dBm} / \text { tone }$ |  | $\begin{aligned} & 13.0 \\ & \pm 0.13 \\ & \pm 0.56 \\ & \pm 0.09 \\ & -9.4 \\ & -8.3 \\ & 24.5 \\ & 40.4 \\ & 4.1 \\ & \hline \end{aligned}$ |  | dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dBm <br> dBm <br> dB |
| AMPLIFIER 2 FREQUENCY $=3600 \mathrm{MHz}$ <br> Gain <br> vs. Frequency <br> vs. Temperature <br> vs. Supply <br> Input Return Loss <br> Output Return Loss <br> Output 1 dB Compression Point Output Third-Order Intercept Noise Figure | Using the AMP2IN and AMP2OUT pins $\begin{aligned} & \pm 200 \mathrm{MHz} \\ & -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C} \\ & 4.75 \mathrm{~V} \text { to } 5.25 \mathrm{~V} \\ & \mathrm{~S} 11 \\ & \mathrm{~S} 22 \end{aligned}$ $\Delta \mathrm{f}=1 \mathrm{MHz} \text {, Pout }=5 \mathrm{dBm} / \text { tone }$ |  | $\begin{aligned} & 12.3 \\ & \pm 1.23 \\ & \pm 1.05 \\ & \pm 0.07 \\ & -15.0 \\ & -11.0 \\ & 26.2 \\ & 36.2 \\ & 5.5 \\ & \hline \end{aligned}$ |  | dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dBm <br> dBm <br> dB |
| $\begin{aligned} & \hline \text { DSA FREQUENCY = } 150 \mathrm{MHz} \\ & \text { Insertion Loss } \\ & \text { vs. Frequency } \\ & \text { vs. Temperature } \\ & \text { Attenuation Range } \\ & \text { Attenuation Step Error } \\ & \text { Attenuation Absolute Error } \\ & \text { Input Return Loss } \\ & \text { Output Return Loss } \\ & \text { Input Third-Order Intercept } \end{aligned}$ | Using the DSAIN and DSAOUT pins, minimum attenuation $\begin{aligned} & \pm 50 \mathrm{MHz} \\ & -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C} \end{aligned}$ <br> Between maximum and minimum attenuation states <br> All attenuation states <br> All attenuation states $\Delta \mathrm{f}=1 \mathrm{MHz} \text {, Pout }=5 \mathrm{dBm} / \text { tone }$ |  | $\begin{aligned} & -1.5 \\ & \pm 0.12 \\ & \pm 0.10 \\ & 28.8 \\ & \pm 0.18 \\ & \pm 1.35 \\ & -13.5 \\ & -13.3 \\ & 48.2 \end{aligned}$ |  | dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dBm |
| DSA FREQUENCY $=450 \mathrm{MHz}$ <br> Insertion Loss <br> vs. Frequency <br> vs. Temperature <br> Attenuation Range <br> Attenuation Step Error <br> Attenuation Absolute Error <br> Input Return Loss <br> Output Return Loss Input Third-Order Intercept | Using the DSAIN and DSAOUT pins, minimum attenuation $\begin{aligned} & \pm 50 \mathrm{MHz} \\ & -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C} \end{aligned}$ <br> Between maximum and minimum attenuation states <br> All attenuation states <br> All attenuation states $\Delta f=1 \mathrm{MHz} \text {, Pout }=5 \mathrm{dBm} / \text { tone }$ |  | $\begin{aligned} & -1.4 \\ & \pm 0.02 \\ & \pm 0.12 \\ & 30.7 \\ & \pm 0.14 \\ & \pm 0.39 \\ & -17.7 \\ & -17.4 \\ & 44.0 \\ & \hline \end{aligned}$ |  | dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dBm |
| $\begin{aligned} & \hline \text { DSA FREQUENCY = } 748 \mathrm{MHz} \\ & \text { Insertion Loss } \\ & \text { vs. Frequency } \\ & \text { vs. Temperature } \\ & \text { Attenuation Range } \\ & \text { Attenuation Step Error } \\ & \text { Attenuation Absolute Error } \\ & \text { Input Return Loss } \\ & \text { Output Return Loss } \\ & \text { Input Third-Order Intercept } \end{aligned}$ | Using the DSAIN and DSAOUT pins, minimum attenuation $\begin{aligned} & \pm 50 \mathrm{MHz} \\ & -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C} \end{aligned}$ <br> Between maximum and minimum attenuation states <br> All attenuation states <br> All attenuation states $\Delta \mathrm{f}=1 \mathrm{MHz} \text {, Pout }=5 \mathrm{dBm} / \text { tone }$ |  | $\begin{aligned} & -1.5 \\ & \pm 0.02 \\ & \pm 0.12 \\ & 30.9 \\ & \pm 0.15 \\ & \pm 0.30 \\ & -17.1 \\ & -17.1 \\ & 44.0 \end{aligned}$ |  | dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dBm |


| Parameter | Conditions | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: |
| DSA FREQUENCY $=943 \mathrm{MHz}$ <br> Insertion Loss <br> vs. Frequency <br> vs. Temperature <br> Attenuation Range <br> Attenuation Step Error <br> Attenuation Absolute Error <br> Input Return Loss <br> Output Return Loss <br> Input 1 dB Compression Point Input Third-Order Intercept | Using the DSAIN and DSAOUT pins, minimum attenuation $\begin{aligned} & \pm 18 \mathrm{MHz} \\ & -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C} \end{aligned}$ <br> Between maximum and minimum attenuation states <br> All attenuation states <br> All attenuation states $\Delta \mathrm{f}=1 \mathrm{MHz} \text {, Pout }=5 \mathrm{dBm} / \text { tone }$ |  | $\begin{aligned} & -1.6 \\ & \pm 0.01 \\ & \pm 0.13 \\ & 30.9 \\ & \pm 0.15 \\ & \pm 0.28 \\ & -16.0 \\ & -15.9 \\ & 30.5 \\ & 50.7 \end{aligned}$ |  | dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dBm <br> dBm |
| DSA FREQUENCY $=1960 \mathrm{MHz}$ <br> Insertion Loss <br> vs. Frequency <br> vs. Temperature <br> Attenuation Range <br> Attenuation Step Error Attenuation Absolute Error Input Return Loss Output Return Loss Input 1 dB Compression Point Input Third-Order Intercept | Using the DSAIN and DSAOUT pins, minimum attenuation $\begin{aligned} & \pm 30 \mathrm{MHz} \\ & -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C} \end{aligned}$ <br> Between maximum and minimum attenuation states <br> All attenuation states <br> All attenuation states $\Delta \mathrm{f}=1 \mathrm{MHz} \text {, Pout }=5 \mathrm{dBm} / \text { tone }$ |  | $\begin{aligned} & -2.5 \\ & \pm 0.04 \\ & \pm 0.18 \\ & 30.8 \\ & \pm 0.15 \\ & \pm 0.35 \\ & -10.3 \\ & -9.6 \\ & 31.5 \\ & 49.6 \\ & \hline \end{aligned}$ |  | dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dBm <br> dBm |
| DSA FREQUENCY $=2140 \mathrm{MHz}$ <br> Insertion Loss <br> vs. Frequency <br> vs. Temperature <br> Attenuation Range <br> Attenuation Step Error <br> Attenuation Absolute Error <br> Input Return Loss <br> Output Return Loss <br> Input 1 dB Compression Point Input Third-Order Intercept | Using the DSAIN and DSAOUT pins, minimum attenuation $\begin{aligned} & \pm 30 \mathrm{MHz} \\ & -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C} \end{aligned}$ <br> Between maximum and minimum attenuation states <br> All attenuation states <br> All attenuation states $\Delta \mathrm{f}=1 \mathrm{MHz} \text {, Pout }=5 \mathrm{dBm} / \text { tone }$ |  | $\begin{aligned} & -2.6 \\ & \pm 0.02 \\ & \pm 0.19 \\ & 30.9 \\ & \pm 0.13 \\ & \pm 0.32 \\ & -9.8 \\ & -9.3 \\ & 31.5 \\ & 49.6 \end{aligned}$ |  | dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dBm <br> dBm |
| DSA FREQUENCY $=2630 \mathrm{MHz}$ Insertion Loss <br> vs. Frequency <br> vs. Temperature <br> Attenuation Range <br> Attenuation Step Error Attenuation Absolute Error Input Return Loss Output Return Loss Input 1 dB Compression Point Input Third-Order Intercept | Using the DSAIN and DSAOUT pins, minimum attenuation $\begin{aligned} & \pm 60 \mathrm{MHz} \\ & -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C} \end{aligned}$ <br> Between maximum and minimum attenuation states <br> All attenuation states <br> All attenuation states $\Delta \mathrm{f}=1 \mathrm{MHz} \text {, Pout }=5 \mathrm{dBm} / \text { tone }$ |  | $\begin{aligned} & -2.8 \\ & \pm 0.02 \\ & \pm 0.21 \\ & 31.2 \\ & \pm 0.18 \\ & \pm 0.24 \\ & -10.0 \\ & -9.6 \\ & 31.5 \\ & 48.3 \end{aligned}$ |  | dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dBm <br> dBm |

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| Parameter | Conditions | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: |
| DSA FREQUENCY $=3600 \mathrm{MHz}$ <br> Insertion Loss <br> vs. Frequency <br> vs. Temperature <br> Attenuation Range <br> Attenuation Step Error Attenuation Absolute Error Input Return Loss Output Return Loss Input 1 dB Compression Point Input Third-Order Intercept | Using the DSAIN and DSAOUT pins, minimum attenuation $\begin{aligned} & \pm 100 \mathrm{MHz} \\ & -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C} \end{aligned}$ <br> Between maximum and minimum attenuation states <br> All attenuation states <br> All attenuation states $\Delta \mathrm{f}=1 \mathrm{MHz} \text {, Pout }=5 \mathrm{dBm} / \text { tone }$ |  | -3.0 $\pm 0.02$ $\pm 0.23$ 31.7 $\pm 0.38$ $\pm 0.35$ -12.3 -11.7 31.0 46.2 |  | dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> dBm <br> dBm |
| DSA Gain Settling <br> Minimum Attenuation to Maximum Attenuation <br> Maximum Attenuation to Minimum Attenuation | Using the DSAIN and DSAOUT pins |  | 36 $36$ |  | ns ns |
| LOOP FREQUENCY $=150 \mathrm{MHz}$ <br> Gain <br> vs. Frequency <br> Gain Range <br> Input Return Loss <br> Output Return Loss <br> Output 1 dB Compression Point <br> Output Third-Order Intercept <br> Noise Figure | AMP1 - DSA - AMP2, DSA at minimum attenuation $\pm 50 \mathrm{MHz}$ <br> Between maximum and minimum attenuation states <br> S11 <br> S22 $\Delta \mathrm{f}=1 \mathrm{MHz} \text {, Pout }=5 \mathrm{dBm} / \text { tone }$ |  | $\begin{aligned} & 37.4 \\ & \pm 0.1 \\ & 28.0 \\ & -10.0 \\ & -7.0 \\ & 22.5 \\ & 38.5 \\ & 3.0 \end{aligned}$ |  | dB <br> dB <br> dB <br> dB <br> dB <br> dBm <br> dBm <br> dB |
| LOOP FREQUENCY $=450 \mathrm{MHz}$ <br> Gain <br> vs. Frequency <br> Gain Range Input Return Loss <br> Output Return Loss <br> Output 1 dB Compression Point <br> Output Third-Order Intercept Noise Figure | AMP1 - DSA - AMP2, DSA at minimum attenuation $\pm 50 \mathrm{MHz}$ <br> Between maximum and minimum attenuation states <br> S11 <br> S22 $\Delta \mathrm{f}=1 \mathrm{MHz} \text {, Pout }=5 \mathrm{dBm} / \text { tone }$ |  | $\begin{aligned} & 35.8 \\ & \pm 0.43 \\ & 31.0 \\ & -12.5 \\ & -6.4 \\ & 23.1 \\ & 37.6 \\ & 3.1 \end{aligned}$ |  | dB <br> dB <br> dB <br> dB <br> dB <br> dBm <br> dBm <br> dB |
| LOOP FREQUENCY $=943 \mathrm{MHz}$ <br> Gain <br> vs. Frequency <br> Gain Range <br> Input Return Loss <br> Output Return Loss <br> Output 1 dB Compression Point <br> Output Third-Order Intercept <br> Noise Figure | AMP1-DSA-AMP2, DSA at minimum attenuation $\pm 18 \mathrm{MHz}$ <br> Between maximum and minimum attenuation states <br> S11 <br> S22 $\Delta \mathrm{f}=1 \mathrm{MHz} \text {, Pout }=5 \mathrm{dBm} / \text { tone }$ |  | $\begin{aligned} & 34.0 \\ & \pm 0.10 \\ & 29.3 \\ & -14.2 \\ & -10.1 \\ & 25.1 \\ & 42.8 \\ & 2.9 \\ & \hline \end{aligned}$ |  | dB <br> dB <br> dB <br> dB <br> dB <br> dBm <br> dBm <br> dB |
| LOOP FREQUENCY $=2140 \mathrm{MHz}$ <br> Gain <br> vs. Frequency <br> Gain Range <br> Input Return Loss <br> Output Return Loss <br> Output 1 dB Compression Point <br> Output Third-Order Intercept <br> Noise Figure | AMP1 - DSA - AMP2, DSA at minimum attenuation $\pm 30 \mathrm{MHz}$ <br> Between maximum and minimum attenuation states <br> S11 <br> S22 $\Delta \mathrm{f}=1 \mathrm{MHz} \text {, Pout }=5 \mathrm{dBm} / \text { tone }$ |  | $\begin{aligned} & 31.3 \\ & \pm 0.03 \\ & 32.5 \\ & -9.3 \\ & -5.4 \\ & 25.3 \\ & 40.0 \\ & 3.1 \end{aligned}$ |  | dB <br> dB <br> dB <br> dB <br> dB <br> dBm <br> dBm <br> dB |

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| Parameter | Conditions | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: |
| ```LOOP FREQUENCY = 2630 MHz Gain vs. Frequency Gain Range Input Return Loss Output Return Loss Output 1 dB Compression Point Output Third-Order Intercept Noise Figure``` | AMP1 - DSA - AMP2, DSA at minimum attenuation $\pm 60 \mathrm{MHz}$ <br> Between maximum and minimum attenuation states <br> S11 <br> S22 $\Delta \mathrm{f}=1 \mathrm{MHz} \text {, Pout }=5 \mathrm{dBm} / \text { tone }$ |  | $\begin{aligned} & 29.5 \\ & \pm 0.56 \\ & 30.0 \\ & -12.6 \\ & -5.8 \\ & 24.6 \\ & 39.3 \\ & 3.1 \end{aligned}$ |  | dB <br> dB <br> dB <br> dB <br> dB <br> dBm <br> dBm <br> dB |
| ```LOOP FREQUENCY \(=3600 \mathrm{MHz}\) Gain vs. Frequency Gain Range Input Return Loss Output Return Loss Output 1 dB Compression Point Output Third-Order Intercept Noise Figure``` | AMP1 - DSA - AMP2, DSA at minimum attenuation $\pm 200 \mathrm{MHz}$ <br> Between maximum and minimum attenuation states <br> S11 <br> S22 $\Delta \mathrm{f}=1 \mathrm{MHz} \text {, Pout }=5 \mathrm{dBm} / \text { tone }$ |  | $\begin{aligned} & 26.5 \\ & \pm 1.3 \\ & 33.0 \\ & -8.0 \\ & -8.0 \\ & 24.7 \\ & 36.0 \\ & 3.7 \end{aligned}$ |  | dB <br> dB <br> dB <br> dB <br> dB <br> dBm <br> dBm <br> dB |
| LOGIC INPUTS Input High Voltage, $\mathrm{V}_{\mathrm{INH}}$ Input Low Voltage, VinL Input Current, $I_{\mathrm{NH}} / \mathrm{I}_{\mathrm{INL}}$ Input Capacitance, $\mathrm{C}_{\mathrm{IN}}$ | CLK, DATA, LE, SEL, D0~D6 | 2.5 | $\begin{aligned} & 0.1 \\ & 1.5 \end{aligned}$ | 0.8 | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~V} \\ & \mu \mathrm{~A} \\ & \mathrm{pF} \end{aligned}$ |
| POWER SUPPLIES <br> Voltage <br> Supply Current | $\begin{aligned} & \text { AMP1 } \\ & \text { AMP2 } \\ & \text { DSA } \end{aligned}$ | 4.75 | $\begin{aligned} & 5.0 \\ & 89 \\ & 86 \\ & 0.5 \end{aligned}$ | $\begin{aligned} & 5.25 \\ & 120 \\ & 120 \end{aligned}$ | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~mA} \\ & \mathrm{~mA} \\ & \mathrm{~mA} \end{aligned}$ |

## ABSOLUTE MAXIMUM RATINGS

Table 2.

| Parameter | Rating |
| :--- | :--- |
| Supply Voltage (VDD, VCC, VCC2) | 6.5 V |
| Input Power |  |
| $\quad$ AMP1IN | 16 dBm |
| $\quad$ AMP2IN ( $50 \Omega$ Impedance) | 20 dBm |
| $\quad$ DSAIN | 30 dBm |
| Internal Power Dissipation | 1.0 W |
| $\theta_{\mathrm{JA}}$ (Exposed Paddle Soldered Down) | $34.8^{\circ} \mathrm{C} / \mathrm{W}$ |
| $\theta_{\mathrm{JC}}$ (Exposed Paddle) | $6.2^{\circ} \mathrm{C} / \mathrm{W}$ |
| Maximum Junction Temperature | $150^{\circ} \mathrm{C}$ |
| Lead Temperature (Soldering, 60 sec ) | $240^{\circ} \mathrm{C}$ |
| Operating Temperature Range | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| Storage Temperature Range | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |

Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## ESD CAUTION

|  | ESD (electrostatic discharge) sensitive device. <br> Charged devices and circuit boards can discharge <br> without detection. Although this product features <br> patented or proprietary protection circuitry, damage <br> may occur on devices subjected to high energy ESD. <br> Therefore, proper ESD precautions should be taken to <br> avoid performance degradation or loss of functionality. |
| :--- | :--- |

## PIN CONFIGURATION AND FUNCTION DESCRIPTIONS



## NOTES

1. NC = NO CONNECT. DO NOT CONNECT TO THIS PIN. 2. THE EXPOSED PAD MUST BE CONNECTED TO GROUND.

Figure 2. Pin Configuration
Table 3. Pin Function Descriptions

| Pin No. | Mnemonic | Description |
| :--- | :--- | :--- |
| 1,24 | VDD | Supply Voltage for DSA. Connect this pin to a 5 V supply. |
| $2,3,5,7,8,9,11,12,13,14$, | NC | No Connect. Do not connect to this pin. |
| $17,18,20,22,23$ |  |  |
| 4 | DSAIN | RF Input to DSA. |
| 6 | AMP1OUT/VCC | RF Output from Amplifier 1/Supply Voltage for Amplifier 1. Bias to Gain Block Amplifier 1 is |
|  |  | provided through a choke to this pin when connected to VCC. |
| 10 | AMP1N | RF Input to Gain Block Amplifier 1. |
| 15 | AMP2OUT/VCC2 | RF Output from Amplifier 2/Supply Voltage for Amplifier 2. Bias to Driver Amplifier 2 is |
|  |  | provided through a choke to this pin when connected to VCC2. |
| 16 | VBIAS | Bias for Driver Amplifier 2. |
| 19 | AMP2IN | RF Input to Amplifier 2. |
| 21 | DSAOUT | RF Output from DSA. |
| 25 | D6 | Data Bit in Parallel Mode (LSB). Connect to supply in serial mode. |
| 26 | D5 | Data Bit in Parallel Mode. Connect to ground in serial mode. |
| 27 | D4 | Data Bit in Parallel Mode. Connect to ground in serial mode. |
| 28 | D3 | Data Bit in Parallel Mode. Connect to ground in serial mode. |
| 29 | D2/LE | Data Bit in Parallel Mode/Latch Enable in Serial Mode. |
| 30 | D1/DATA | Data Bit in Parallel Mode (MSB)/Data in Serial Mode. |
| 31 | D0/CLK | Connect this pin to ground in parallel mode. This pin functions as a clock in serial mode. |
| 32 | SEL | Select Pin. For parallel mode operation, connect this pin to the supply. For serial mode |
|  |  | operation, connect this pin to ground. |

## TYPICAL PERFORMANCE CHARACTERISTICS



Figure 3. AMP1: Gain, P1dB, OIP3 at Pout $=3 \mathrm{dBm} /$ Tone and Noise Figure vs. Frequency


Figure 4. AMP1: Gain vs. Frequency and Temperature


Figure 5. AMP1: Input Return Loss (S11), Output Return Loss (S22), and Reverse Isolation (S12) vs. Frequency


Figure 6. AMP1: OIP3 at Pout $=3 \mathrm{dBm} /$ Tone and P1dB vs. Frequency and Temperature


Figure 7. AMP1: OIP3 vs. Pout and Frequency


Figure 8. AMP1: Noise Figure vs. Frequency and Temperature


Figure 9. AMP2-943 MHz: Gain, P1dB, OIP3 at Pout $=5 \mathrm{dBm} /$ Tone and Noise Figure vs. Frequency


Figure 10. AMP2-943 MHz: Gain vs. Frequency and Temperature


Figure 11. AMP2-943 MHz: Input Return Loss (S11), Output Return Loss (S22), and Reverse Isolation (S12) vs. Frequency


Figure 12. AMP2-943 MHz: OIP3 at Pout $=5 \mathrm{dBm} /$ Tone and $P 1 \mathrm{~dB}$ vs. Frequency and Temperature


Figure 13. AMP2-943 MHz: OIP3 vs. Pout and Frequency


Figure 14. AMP2-943 MHz: Noise Figure vs. Frequency and Temperature


Figure 15. AMP2-2140 MHz: Gain, P1dB, OIP3 at Pout $=5 \mathrm{dBm} /$ Tone and Noise Figure vs. Frequency


Figure 16. AMP2-2140 MHz: Gain vs. Frequency and Temperature


Figure 17. AMP2-2140 MHz: Input Return Loss (S11), Output Return Loss (S22), and Reverse Isolation (S12) vs. Frequency


Figure 18. AMP2-2140 MHz: OIP3 at Pout $=5 \mathrm{dBm} /$ Tone and $P 1 \mathrm{~dB}$ vs. Frequency and Temperature


Figure 19. AMP2-2140 MHz: OIP3 vs. Pout and Frequency


Figure 20. AMP2-2140 MHz: Noise Figure vs. Frequency and Temperature


Figure 21. AMP2-2630 MHz: Gain, P1dB, OIP3 at Pout $=5 \mathrm{dBm} /$ Tone and Noise Figure vs. Frequency


Figure 22. AMP2-2630 MHz: Gain vs. Frequency and Temperature


Figure 23. AMP2-2630 MHz: Input Return Loss (S11), Output Return Loss (S22), and Reverse Isolation (S12) vs. Frequency


Figure 24. AMP2-2630 MHz: OIP3 at Pout $=5 \mathrm{dBm} /$ Tone and $P 1 \mathrm{~dB}$ vs. Frequency and Temperature


Figure 25. AMP2-2630 MHz: OIP3 vs. Pout and Frequency


Figure 26. AMP2-2630 MHz: Noise Figure vs. Frequency and Temperature


Figure 27. DSA: Attenuation vs. Frequency


Figure 28. DSA: Attenuation vs. Frequency and Temperature


Figure 29. DSA: Step Error vs. Attenuation


Figure 30. DSA: Absolute Error vs. Attenuation


Figure 31. DSA: Input Return Loss vs. Frequency, All States


Figure 32. DSA: Output Return Loss vs. Frequency, All States


Figure 33. DSA: Input P1dB and Input IP3 vs. Frequency, Minimum Attenuation State


Figure 34. DSA: Gain Settling Time, $0 d B$ to $31.5 d B$


Figure 35. DSA: Gain Settling Time, $31.5 d B$ to $0 d B$


Figure 36. DSA: Phase vs. Attenuation


Figure 37. Loop-943 MHz: Gain, P1dB, OIP3 at Pout $=5 \mathrm{dBm} /$ Tone and Noise Figure vs. Frequency, Minimum Attenuation State


Figure 38. Loop-943 MHz: Input Return Loss (S11), Output Return Loss (S22), and Reverse Isolation (S12) vs. Frequency, Minimum Attenuation State


Figure 39. Loop-943 MHz: OIP3 vs. Pout and Frequency, Minimum Attenuation State


Figure 40. Loop-2140 MHz: Gain, P1dB, OIP3 at Pout $=5 \mathrm{dBm} /$ Tone and Noise Figure vs. Frequency, Minimum Attenuation State


Figure 41. Loop-2140 MHz: Input Return Loss (S11), Output Return Loss (S22), and Reverse Isolation (S12) vs. Frequency, Minimum Attenuation State


Figure 42. Loop-2140 MHz: OIP3 vs. Pout and Frequency, Minimum Attenuation State


Figure 43. Loop-2630 MHz: Gain, P1dB, OIP3 at Pout $=5 \mathrm{dBm} /$ Tone and Noise Figure vs. Frequency, Minimum Attenuation State


Figure 44. Loop-2630 MHz: Input Return Loss (S11), Output Return Loss (S22), and Reverse Isolation (S12) vs. Frequency, Minimum Attenuation State


Figure 45. Loop-2630 MHz: OIP3 vs. Pout and Frequency, Minimum Attenuation State


Figure 46. AMP1: Supply Current vs. Voltage and Temperature


Figure 47. AMP1: Supply Current vs. Pout and Temperature


Figure 48. AMP2: Supply Current vs. Voltage and Temperature


Figure 49. AMP2: Supply Current vs. Pout and Temperature


Figure 50. AMP1: Gain Distribution at 2140 MHz


Figure 51. AMP1: P1dB Distribution at 2140 MHz


Figure 52. AMP1: OIP3 Distribution at 2140 MHz


Figure 53. AMP1: Noise Figure Distribution at 2140 MHz


Figure 54. AMP2: Gain Distribution at 2140 MHz


Figure 55. AMP2: P1dB Distribution at 2140 MHz


Figure 56. AMP2: OIP3 Distribution at 2140 MHz


Figure 57. AMP2: Noise Figure Distribution at 2140 MHz

## APPLICATIONS INFORMATION

## BASIC LAYOUT CONNECTIONS

The basic connections for operating the ADL5243 are shown in Figure 58. The schematic of AMP2 is configured for 2140 MHz operation.


Figure 58. Basic Connections

## Amplifier 1 Power Supply

AMP1 in the ADL5243 is a broadband gain block. The dc bias is supplied through Inductor L1 and is connected to the AMP1OUT pin. Three decoupling capacitors (C13, C14, and C 25 ) are used to prevent RF signals from propagating on the dc lines. The dc supply ranges from 4.75 V to 5.25 V and should be connected to the VCC test pin.

## Amplifier 1 RF Input Interface

Pin 10 is the RF input for AMP1 of the ADL5243. The amplifier is internally matched to $50 \Omega$ at the input; therefore, no external components are required. Only a dc blocking capacitor (C21) is required.

## Amplifier 1 RF Output Interface

Pin 6 is the RF output for AMP1 of the ADL5243. The amplifier is internally matched to $50 \Omega$ at the output as well; therefore, no external components are required. Only a dc blocking capacitor (C4) is required. The bias is provided through this pin via a choke inductor, L1.

## Amplifier 2 Power Supply

The collector bias for AMP2 is supplied through Inductor L2 and is connected to the AMP2OUT pin, whereas the base bias is provided through Pin 16. The base bias is connected to the same supply pin as the collector bias. Three decoupling capacitors (C3, C20, and C25) are used to prevent RF signals from propagating on the dc lines. The dc supply ranges from 4.75 V to 5.25 V and should be connected to the VCC2 test pin.

## Amplifier 2 RF Input Interface

Pin 19 is the RF input for AMP2 of the ADL5243. The input of the amplifier is easily matched to $50 \Omega$ with a combination of series and shunt capacitors and a microstrip line serving as an inductor. Figure 58 shows the input matching components and is configured for 2140 MHz .

## Amplifier 2 RF Output Interface

Pin 15 is the RF input for AMP2 of the ADL5243. The output of the amplifier is easily matched to $50 \Omega$ with a combination of series and shunt capacitors and a microstrip line serving as an inductor.

Additionally, bias is provided through this pin. Figure 58 shows the output matching components and is configured for 2140 MHz .

## DSA RF Input Interface

Pin 4 is the RF input for the DSA of the ADL5243. The input impedance of the DSA is close to $50 \Omega$ over the entire frequency range; therefore, no external components are required. Only a dc blocking capacitor (C1) is required.

## DSA RF Output Interface

Pin 21 is the RF output for the DSA of the ADL5243. The output impedance of the DSA is close to $50 \Omega$ over the entire frequency range; therefore, no external components are required. Only a dc blocking capacitor (C5) is required.

## DSA SPI Interface

The DSA of the ADL5243 can operate in either serial or parallel mode. Pin 32 (SEL) controls the mode of operation. For serial mode operation, connect SEL to ground, and for parallel mode operation, connect SEL to VDD. In parallel mode, Pin 25 to Pin 30 (D6 to D1) are the data bits, with D6 being the LSB. Connect Pin 31 (D0) to ground during parallel mode of operation. In serial mode, Pin 29 is the latch enable (LE), Pin 30 is the data (DATA), and Pin 31 is the clock (CLK). Pin 26, Pin 27, and Pin 28 are not used in the serial mode and should be connected to ground. Pin 25 (D6) should be connected to VDD during the serial mode of operation. To prevent noise from coupling onto the digital signals, an RC filter can be used on each data line.

## SPI TIMING

## SPI Timing Sequence

Figure 60 shows the timing sequence for the SPI function using a 6-bit operation. The clock can be as fast as 20 MHz . In serial mode operation, Register B5 (MSB) is first, and Register B0 (LSB) is last.

Table 4. Mode Selection Table

| Pin 32 (SEL) | Functionality |
| :--- | :--- |
| Connect to Ground | Serial mode |
| Connect to Supply | Parallel mode |

Table 5. SPI Timing Specifications

| Parameter | Limit | Unit | Test Conditions/Comments |
| :--- | :--- | :--- | :--- |
| $\mathrm{F}_{\mathrm{CLK}}$ | 10 | MHz | Data clock frequency |
| $\mathrm{t}_{1}$ | 30 | ns min | Clock high time |
| $\mathrm{t}_{2}$ | 30 | ns min | Clock low time |
| $\mathrm{t}_{3}$ | 10 | ns min | Data to clock setup time |
| $\mathrm{t}_{4}$ | 10 | ns min | Clock to data hold time |
| $t_{5}$ | 10 | ns min | Clock low to LE setup time |
| $\mathrm{t}_{6}$ | 30 | ns min | LE pulse width |



Figure 60. SPI Timing Sequence
Table 6. DSA Attenuation Truth Table-Serial Mode

| Attenuation State | B5 (MSB) | B4 | B3 | B2 | B1 | B0 (LSB) |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 0 dB (Reference) | 1 | 1 | 1 | 1 | 1 | 1 |
| 0.5 dB | 1 | 1 | 1 | 1 | 0 |  |
| 1.0 dB | 1 | 1 | 1 | 0 | 1 |  |
| 2.0 dB | 1 | 1 | 0 | 1 | 1 |  |
| 4.0 dB | 1 | 0 | 1 | 1 | 1 |  |
| 8.0 dB | 1 | 1 | 1 | 1 | 1 |  |
| 16.0 dB | 0 | 0 | 0 | 1 | 1 |  |
| 31.5 dB | 0 | 1 | 0 | 0 |  |  |

Table 7. DSA Attenuation Truth Table-Parallel Mode

| Attenuation State | D1 (MSB) | D2 | D3 | D4 | D5 | D6 (LSB) |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 0 dB (Reference) | 1 | 1 | 1 | 1 | 1 | 1 |
| 0.5 dB | 1 | 1 | 1 | 1 | 0 |  |
| 1.0 dB | 1 | 1 | 1 | 0 | 1 |  |
| 2.0 dB | 1 | 1 | 0 | 1 | 1 |  |
| 4.0 dB | 1 | 0 | 1 | 1 | 1 |  |
| 8.0 dB | 1 | 1 | 1 | 1 | 1 |  |
| 16.0 dB | 0 | 1 | 0 | 1 | 0 |  |
| 31.5 dB | 0 | 0 | 0 |  |  |  |

## ADL5243 AMPLIFIER 2 MATCHING

The AMP2 input and output of the ADL5243 can be matched to $50 \Omega$ with two or three external components and the microstrip line used as an inductor. Table 8 lists the required matching components values. All capacitors are Murata GRM155 series (0402 size), and Inductor L2 is a Coilcraft ${ }^{\circ} 0603 C S$ series (0603 size). For all frequency bands, the placement of Capacitors C22, C26, and C28 is critical.

Table 9 lists the recommended component spacing of C22, C26, and C28 for the various frequencies. The placement of R12 and C 27 is fixed for the matching network on evaluation board and
the spacing is 153 mils and 25 mils respectively. The component spacing is referenced from the center of the component to the edge of the package. Figure 61 to Figure 69 show the graphical representation of the matching network. It is recommended to configure a RC feedback network and bias the AMP2 input through external R for optimal performance at-frequency bands less than 500 MHz as shown at Figure 61 and Figure 62. In this case, VBIAS pin must be left open.

Table 8. Component Values on Evaluation Board

| Frequency | C27 | C26 | C28 | C8 | C22 | C23 | L2 | R10 | R20 ${ }^{1}$ | R12 | R16 | R15 | C10 | R31 | R30 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 150 MHz | 2.7n H | 1.5 pF | N/A | 1500 pF | 0.5 pF | 4700 pF | 390 nH | $21 \Omega$ | N/A | 22 nH | $3.16 \mathrm{k} \Omega$ | $750 \Omega$ | 1 nF | $0 \Omega$ | N/A |
| 450 MHz | $0 \Omega$ | N/A | 5.1 pF | 1000 pF | 0.5 pF | 1000 pF | 110 nH | $21 \Omega$ | $5.6 \Omega$ | 3.9 nH | $3.16 \mathrm{k} \Omega$ | $750 \Omega$ | 1 nF | $0 \Omega$ | N/A |
| 748 MHz | $0 \Omega$ | N/A | 5.1 pF | 12 pF | 1.3 pF | 18 pF | 56 nH | $18 \Omega$ | $5.6 \Omega$ | 3.9 nH | N/A | N/A | N/A | N/A | $0 \Omega$ |
| 943 MHz | $0 \Omega$ | 3.9 pF | N/A | 6 pF | 1.3 pF | 100 pF | 56 nH | $18 \Omega$ | N/A | 3.3 nH | N/A | N/A | N/A | N/A | $0 \Omega$ |
| 1960 MHz | 2.7 pF | N/A | 1.0 pF | 10 pF | 1.0 pF | 20 pF | 9.5 nH | $0 \Omega$ | N/A | $0 \Omega$ | N/A | N/A | N/A | N/A | $0 \Omega$ |
| 2140 MHz | 2.2 pF | N/A | 1.8 pF | 10 pF | 1.0 pF | 10 pF | 9.5 nH | $0 \Omega$ | N/A | $0 \Omega$ | N/A | N/A | N/A | N/A | $0 \Omega$ |
| 2350 MHz | 3.3 pF | 1.6 pF | $1.5 \mathrm{~K} \Omega$ | 10 pF | 1.0 pF | 20 pF | 9.5 nH | $0 \Omega$ | N/A | $0 \Omega$ | N/A | N/A | N/A | N/A | $0 \Omega$ |
| 2630 MHz | 2.7 pF | 1.1 pF | $1.5 \mathrm{~K} \Omega$ | 10 pF | 1.3 pF | 20 pF | 9.5 nH | $0 \Omega$ | N/A | $0 \Omega$ | N/A | N/A | N/A | N/A | $0 \Omega$ |
| 3600 MHz | 1.0 pF | $1.5 \mathrm{~K} \Omega$ | 1.2 pF | 10 pF | 1.2 pF | 20 pF | 9.5 nH | $0 \Omega$ | N/A | 1.0 nH | N/A | N/A | N/A | N/A | $0 \Omega$ |

${ }^{1}$ R20 is not reserved on the evaluation board.
Table 9. Component Spacing on Evaluation Board

| Frequency | C26: $\boldsymbol{\lambda 1}(\mathbf{m i l s})$ | C28: $\boldsymbol{\lambda 2}(\mathbf{m i l s})$ | C22: $\boldsymbol{\lambda 3}(\mathbf{m i l s})$ |
| :--- | :--- | :--- | :--- |
| 150 MHz | 213 | $\mathrm{~N} / \mathrm{A}$ | 408 |
| 450 MHz | $\mathrm{N} / \mathrm{A}$ | 230 | 485 |
| 748 MHz | $\mathrm{N} / \mathrm{A}$ | 315 | 201 |
| 943 MHz | 236 | $\mathrm{~N} / \mathrm{A}$ | 394 |
| 1960 MHz | $\mathrm{N} / \mathrm{A}$ | 366 | 244 |
| 2140 MHz | $\mathrm{N} / \mathrm{A}$ | 366 | 244 |
| 2350 MHz | 153 | 195 | 244 |
| 2630 MHz | 126 | 161 | 240 |
| 3600 MHz | 342 | 366 | 106 |



Figure 61. AMP2: Matching Circuit at 150 MHz



Figure 63. AMP2: Matching Circuit at 748 MHz



Figure 65. AMP2: Matching Circuit at 1960 MHz



Figure 67. AMP2: Matching Circuit at 2350 MHz


Figure 68. AMP2: Matching Circuit at 2630 MHz


## ADL5243 LOOP PERFORMANCE

The typical configuration of the ADL5243 is to connect in AMP1-DSA-AMP2 mode, as shown in Figure 70. Because AMP1 and DSA are broadband in nature and internally matched, only an ac coupling capacitor is required between them. The AMP2 is externally matched for each frequency band of operation, and these matching elements should be placed between the DSA and AMP2 and at the output of AMP2. Matching circuits for AMP2 are shown in Figure 61 through Figure 69. This works well in a loop in each case but matching circuits between the DSA and AMP2 requires slight retuning, such as adding a shunt capacitor at the DSA output or changing the location of a shunt capacitor for optimum performance in a loop at certain frequency bands. Figure 71 and Figure 72 show the retuned matching circuits from Figure 66 and Figure 69 at 2140 MHz and 3600 MHz , respectively. Figure 37 to Figure 45 show the performance of the ADL5243 when connected in a loop for the three primary frequency bands of operation, namely $943 \mathrm{MHz}, 2140 \mathrm{MHz}$, and 2630 MHz .

Table 10. Component Spacing in a Loop on Evaluation Board

| Frequency | C26: $\mathbf{\lambda 1}$ <br> (mils) | C28: $\mathbf{1 2}$ <br> (mils) | C22: $\mathbf{\lambda 3}$ <br> (mils) | C11: $\mathbf{1 4}$ <br> (mils) |
| :--- | :--- | :--- | :--- | :--- |
| 2140 MHz | $\mathrm{N} / \mathrm{A}$ | 366 | 244 | 122 |
| 3600 MHz | 126 | 342 | 106 | $\mathrm{~N} / \mathrm{A}$ |



Figure 70. ADL5243 Loop Block Diagram


Figure 71. ADL5243 Matching Circuit at 2140 MHz in a Loop


Figure 72. ADL5243 Matching Circuit at 3600 MHz in a Loop

## PROPER DRIVING LEVEL FOR THE OPTIMUM ACLR

It is usually required to drive the amplifier as high as possible in order to maximize output power. However, properly driving AMP1 and AMP2 at the ADL5243 is required to achieve optimum ACLR performance. Once output power approaches P1dB and OIP3, there is ACLR degradation. The driving level of amplifier with a modulated signal should be backed off properly from P1dB by at least the amount of a signal crest factor for optimum ACLR. So assuming a gain and P1dB of AMP1 at 2140 MHz are 19 dB and 19 dBm respectively, the output power, which is backed off by 11 dB crest factor at the modulated signal case, is 8 dBm . Therefore, the proper input driving level should be under -11 dBm .


Figure 73. Single Carrier WCDMA Adjacent Chanel Power Ratio vs. Input Power at AMP1 and AMP2, 2140 MHz

## THERMAL CONSIDERATIONS

The ADL5243 is packaged in a thermally efficient, $5 \mathrm{~mm} \times 5 \mathrm{~mm}$, 32-lead LFCSP. The thermal resistance from junction to air $\left(\theta_{J A}\right)$ is $34.8^{\circ} \mathrm{C} / \mathrm{W}$. The thermal resistance for the product was extracted assuming a standard 4 -layer JEDEC board with 25 copper platter thermal vias. The thermal vias are filled with conductive copper paste, AE3030, with a thermal conductivity of $7.8 \mathrm{~W} / \mathrm{mk}$ and thermal expansion as follows: $\alpha 1$ of $4 \times 10^{-5} /{ }^{\circ} \mathrm{C}$ and $\alpha 2$ of $8.6 \times$ $10^{-5} /{ }^{\circ} \mathrm{C}$. The thermal resistance from junction to case $\left(\theta_{\mathrm{JC}}\right)$ is $6.2^{\circ} \mathrm{C} / \mathrm{W}$, where case is the exposed pad of the lead frame package.

For the best thermal performance, it is recommended to add as many thermal vias as possible under the exposed pad of the LFCSP. The above thermal resistance numbers assume a minimum of 25 thermal vias arranged in a $5 \times 5$ array with a via diameter of 13 mils, via pad of 25 mils, and pitch of 25 mils. The vias are plated with copper, and the drill hole is filled with a conductive copper paste. For optimal performance, it is recommended to fill the thermal vias with a conductive paste of equivalent thermal conductivity, as mentioned above, or use an external heat sink to dissipate the heat quickly without affecting the die junction temperature. It is also recommended to extend the ground pattern as shown in Figure 74 to improve thermal efficiency.

## SOLDERING INFORMATION AND RECOMMENDED PCB LAND PATTERN

Figure 74 shows the recommended land pattern for the ADL5243. To minimize thermal impedance, the exposed paddle on the $5 \mathrm{~mm} \times 5 \mathrm{~mm}$ LFCSP package is soldered down to a ground plane. To improve thermal dissipation, 25 thermal vias are arranged in a $5 \times 5$ array under the exposed paddle. If multiple ground layers exist, they should be tied together using vias. For more information on land pattern design and layout, see the AN-772 Application Note, A Design and Manufacturing Guide for the Lead Frame Chip Scale Package (LFCSP).


Figure 74. Recommended Land Pattern

## EVALUATION BOARD

The schematic of the ADL5243 evaluation board is shown in Figure 75. All RF traces on the evaluation board have a characteristic impedance of $50 \Omega$ and are fabricated from Rogers3003 material. The traces are CPWG with a width of 25 mils, spacing of 20 mils, and dielectric thickness of 10 mils. The input and output to the DSA and amplifier should be ac-coupled with capacitors of an appropriate value to ensure broadband performance. The bias to AMP1 is provided through a choke connected to the AMP1OUT pin and, similarly, bias to AMP2 is provided through a choke connected to the AMP2OUT pin. Bypassing capacitors are recommended on all supply lines to minimize RF coupling. The DSA and the amplifiers can be individually biased or connected to the VDD plane through Resistors R1, R2, and R11. The schematic of AMP2 on evaluation board is configured for 2140 MHz operation.

When configuring the ADL5243 evaluation board in the AMP1-DSA-AMP2 loop, remove Capacitors C1, C4, C5, and C 8 and remove Resistor R10. Place 10 pF in place of C 24 and C6, and $0 \Omega$ in place of R32 and R33. If needed, placing a shunt capacitor $(1.3 \mathrm{pF})$ at the output of the DSA improves the output return loss of this loop as described at the ADL5243 Loop Performance section.

On the digital signal traces, provisions for an RC filter are made to clean any potential coupled noise. In normal operation, series resistors are $0 \Omega$ and shunt resistors and capacitors are open.

The evaluation board is designed to control DSA in either parallel or serial mode by connecting the SEL pin to the supply or ground by a switch.

For adjusting attenuation at DSA, the ADL5243 can be programmed in two ways: through the on-board USB interface from a PC USB port, or through an SDP board, which will become the Analog Devices common control board in the future. The on-board USB interface circuitry of the evaluation board is powered directly by the PC. USB based programming software is available to download from the ADL5243 product page at $w w w$.analog.com. Figure 71 shows the window of the programming software where the user selects serial or parallel mode for the attenuation adjustment at DSA. The selection of the mode in the window should match the mode of the evaluation board switch.

It is highly recommended to refer the evaluation board layout for the optimal and stable performance of each block as well as for the improvement of thermal efficiency.

Table 11. Evaluation Board Configurations Options

| Component | Function | Default Value |
| :---: | :---: | :---: |
| C1, C5 | AC coupling caps for DSA. | $\mathrm{C} 1, \mathrm{C} 5=10 \mathrm{pF}$ |
| C4, C21 | AC coupling capacitors for AMP1. | C4, C21 = 10 pF |
| C13, C14, C15 | Power supply bypassing capacitors for AMP1. Capacitor C15 should be closest to the device. | $\begin{aligned} & \mathrm{C} 13=10 \mu \mathrm{~F} \\ & \mathrm{C} 14=10 \mathrm{nF} \\ & \mathrm{C} 15=10 \mathrm{pF} \end{aligned}$ |
| L1 | The bias for AMP1 comes through L1 when connected to a 5 V supply. L1 should be high impedance for the frequency of operation, while providing low resistance for the dc current. | $\mathrm{L} 1=33 \mathrm{nH}$ |
| C8 | AMP2 input ac coupling capacitor. | $\mathrm{C} 8=10 \mathrm{pF}$ |
| C23 | AMP2 output ac coupling capacitor. | $\mathrm{C} 23=10 \mathrm{pF}$ |
| C22 | AMP2 shunt output tuning capacitor. | $\mathrm{C} 22=1.0 \mathrm{pF}$ at 244 mils from edge of package |
| C26 | ANP2 shunt input tuning capacitor. | DNP |
| C27 | AMP2 series input tuning capacitor. | $\mathrm{C} 27=2.2 \mathrm{pF}$ |
| C28 | AMP2 shunt input tuning capacitor. | $\mathrm{C} 28=1.8 \mathrm{pF}$ at 366 mils from edge of package |
| C3, C25, C20 | Power supply bypassing capacitors for AMP2. Capacitor C3 should be closest to the device. | $\begin{aligned} & \mathrm{C} 3=10 \mathrm{pF} \\ & \mathrm{C} 25=10 \mathrm{nF} \\ & \mathrm{C} 20=10 \mu \mathrm{~F} \\ & \hline \end{aligned}$ |
| L2 | The bias for AMP2 comes through L2 when connected to a 5 V supply. L2 should be high impedance for the frequency of operation, while providing low resistance for the dc current. | $\mathrm{L} 2=9.5 \mathrm{nH}$ |
| C17 | Power supply bypassing capacitor for DSA. | $\mathrm{C} 17=0.1 \mu \mathrm{~F}$ |
| R10, R12 | Placeholder for the series component for the other frequency band. | R10, R12 $=0 \Omega$ |
| C6, C24, R32, R33 | Replace with capacitors and resistors to connect the device in a loop. | C6, C24, R32, R33 = open |
| R1, R2, R11 | Resistors to connect the supply for the amplifier and the DSA to the same VDD plane. | R1, R2 = open |
| S1 | Switch to change between serial and parallel mode operation; connect to a supply for parallel mode and to ground for serial mode operation. | 3-pin rocker |





Figure 77. Evaluation Board Layout—Top


Figure 78. Evaluation Board Layout—Bottom


Figure 79. Evaluation Board Control Software

## ADL5243

## OUTLINE DIMENSIONS



ORDERING GUIDE

| Model $^{1}$ | Temperature Range | Package Description | Package Option |
| :--- | :--- | :--- | :--- |
| ADL5243ACPZ-R7 | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 32-Lead Lead Frame Chip Scale Package LFCSP_VQ <br> ADL5243-EVALZ | Evaluation Board |

[^0]$\square$
Data Sheet
ADL5243
NOTES

## NOTES


[^0]:    ${ }^{1} \mathrm{Z}=$ RoHS Compliant Part.

