

DEMO MANUAL DC368A

LT1763 500mA Low Noise Micropower LDO Regulator

DESCRIPTION

Demonstration circuit DC368A is a low noise micropower voltage regulator using the LT®1763 in the 8-lead SO package. These circuits are used primarily in voltage controlled oscillators, RF power supplies and, in larger systems, as local regulators. The ability to tolerate a wide variety of

output capacitors makes them ideal in space- and costsensitive systems.

Design files for this circuit board are available at http://www.linear.com/demo/DC368A

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PERFORMANCE SUMMARY

 $T_A = 25^{\circ}C$, $V_{IN} = 2.3V$, $V_{SHDN} = 5V$, $I_{LOAD} = 1mA$, $V_{OUT} = 1.22V$ (JP2 set on Pins 1-2), unless otherwise specified.

PARAMETER	CONDITIONS	MIN	ТҮР	MAX	UNITS
Input Voltage Range		2.3		20	V
Output Voltage (Note 1)		1.208	1.220	1.232	V
Output Voltage (Note 1)	V _{IN} = 1.5V, JP2 on Pins 5-6	1.478	1.497	1.519	V
Output Voltage (Note 1)	V _{IN} = 1.8V, JP2 on Pins 7-8	1.775	1.802	1.834	V
Output Voltage (Note 1)	V _{IN} = 2.5V, JP2 on Pins 9-10	2.462	2.506	2.563	V
Output Voltage (Note 1)	V _{IN} = 3V, JP2 on Pins 11-12	2.961	3.019	3.093	V
Output Voltage (Note 1)	V _{IN} = 3.3V, JP2 on Pins 13-14	3.235	3.300	3.384	V
Output Voltage (Note 1)	V _{IN} = 5V, JP2 on Pins 15-16	4.897	5.006	5.148	V
Line Regulation	$\Delta V_{IN} = 2.3 V$ to 20V		1	5	mV
Quiescent Current	$\Delta I_{LOAD} = 0 mA$		30	50	μA
Load Regulation	$\Delta I_{LOAD} = 1 \text{ mA to } 500 \text{ mA}$		0.2	1	%
SHDN Pin Threshold	On-to-Off	0.45	0.65		V
	Off-to-On, I _{LOAD} = 1mA		0.8	1.8	V
Output Voltage Noise	I _{LOAD} = 500mA, BW = 10Hz to 100kHz		20		μV _{RMS}

Note 1: Output voltage variations include ±1% tolerance of feedback divider network. For tighter voltage range, use lower tolerance resistors or use fixed voltage output devices.

TYPICAL PERFORMANCE CHARACTERISTICS









PACKAGE AND SCHEMATIC DIAGRAMS



Figure 1. LT1763 500mA Low Noise Micropower LDO Regulator





PARTS LIST

ITEM	QUANTITY	REFERENCE	PART DESCRIPTION	MANUFACTURE/PART #	
1	0	ADJ1	OPT, 0402		
2	1	C1	CAP, X5R 1µF 25V 10%, 0603	AVX 06033D105KAT2A	
3	1	C2	CAP, X7R 0.01µF 16V 5%, 0402	AVX 0402YC103JAT1A	
4	1	C3	CAP CER X7R 10µF 10V, 1210	TAIYO YUDEN LMK325BJ106MN	
5	4	E1 to E4	TP, TERMINAL TURRET, 1 PIN, 0.064 HOLE	Mill-Max 2308-2	
6	1	JP1	JMP, 2 PINS 1 ROW .079CC	COMM-CON 2802S-02-G1	
7	1	JP2	CONN, SMT2X8, 0.39" GAP	COMM-CON 6351-16P1	
8	1	SHUNTS FOR JP1	SHUNTS, .079" CENTER	COMM-CON CCIJ2MM-138G	
9	1	SHUNTS FOR JP2	SHUNTS 0.39CC	COMM-CON CTAIJ1MM-G	
10	1	R1	RES., CHIP 56.2k 1/16W 1% 0402	AAC CR05-5622FM	
11	1	R2	RES., CHIP 118k 1/16W 1% 0402	AAC CR05-1183FM	
12	1	R3	RES., CHIP 261k 1/16W 1% 0402	AAC CR05-2613FM	
13	1	R4	RES., CHIP 365k 1/16W 1% 0402	AAC CR05-3653FM	
14	1	R5	RES., CHIP 422k 1/16W 1% 0402	AAC CR05-4223FM	
15	1	R6	RES., CHIP 768k 1/16W 1% 0402	AAC CR05-7683FM	
16	1	R7	RES., CHIP 249k 1/16W 1% 0402	AAC CR05-2493FM	
17	1	U1	IC, LT1763CS8, SO8	LINEAR TECH. LT1763CS8	



HOOK-UP

Solid turret terminals are provided for easy connection to supplies and test equipment. Connect a OV to 20V, 0.6A power supply across the IN and GND terminals and the load across the OUT and GND terminals. The SHDN pin can be disconnected from IN via JP1 to allow for separate shutdown control via a secondary control line. JP2 can be used to select any of a number of common fixed output voltages, or used in conjunction with ADJ1 to create a custom output voltage using the formula:

 $ADJ1 = (V_{OUT} - 1.22V)/4.93\mu A$

Thermal Characteristics

Demonstration Circuit DC368A has been laid out to illustrate and achieve maximum power handling capabilities. Although a simple two-layer board might have been sufficient for electrical operation of the LT1763, the four-layer board with vias to internal ground planes offers excellent thermal characteristics. A two-layer board of the same size with no thermal vias will exhibit a thermal resistance of 60°C/W, whereas DC368A exhibits a thermal resistance of 50°C/W.

OUTPUT CAPACITOR SELECTION

The output capacitor C3 is a 10µF X7R ceramic chip capacitor. Should a different output capacitor be desired, care must be exercised with the selection. Many ceramic capacitor dielectrics exhibit strong temperature and voltage characteristics that reduce their effective capacitance to as low as 10% to 20% of nominal over the full temperature range. For further information, see Linear Technology Application Note 83, "Performance Verification of Low Noise, Low Dropout Regulators," Appendix B, "Capacitor Selection Considerations," reprinted below.

CAPACITOR SELECTION CONSIDERATIONS

Bypass Capacitance and Low Noise Performance

Adding a capacitor between the regulator's V_{OUT} and BYP pins lowers output noise. A good quality, low leakage capacitor is recommended. This capacitor bypasses the regulator's reference, providing a low frequency noise

pole. A 0.01μ F capacitor lowers the output voltage noise to 20μ V_{RMS}. Using a bypass capacitor also improves transient response. With no bypassing and a 10μ F output capacitor, a 10mA to 500mA load step settles to within 1% of final value in under 100µs. With a 0.01μ F bypass capacitor, the output settles to within 1% for the same load step in under 10µs; total output deviation is inside 2.5%. Regulator start-up time is inversely proportional to bypass capacitor size, slowing to 15ms with a 0.01μ F bypass capacitor and 10μ F at the output.

Output Capacitance and Transient Response

The regulators are designed to be stable with a wide range of output capacitors. Output capacitor ESR affects stability, most notably with small capacitors. A 3.3μ F minimum output value with ESR of 3Ω or less is recommended to prevent oscillation. Transient response is a function of output capacitance. Larger values of output capacitance decrease peak deviations, providing improved transient response for large load current changes. Bypass capacitors, used to decouple individual components powered by the regulator, increase the effective output capacitor value. Larger values of reference bypass capacitance dictate larger output capacitors. For 100pF of bypass capacitance, 4.7μ F of output capacitor is recommended. With 1000pF or more of bypass capacitance, a 6.8μ F output capacitor is required.

The shaded region of Figure B1 defines the regulator's stability range. The minimum ESR needed is set by the amount of bypass capacitance used, while maximum ESR is 3Ω .

Ceramic Capacitors

Ceramic capacitors require extra consideration. They are manufactured with a variety of dielectrics, each with different behavior across temperature and applied voltage. The most common dielectrics are Z5U, Y5V, X5R and X7R. The Z5U and Y5V dielectrics provide high capacitance in a small package, but exhibit strong voltage and temperature coefficients, as shown in Figures B2 and B3. Used with a 5V regulator, a 10 μ F Y5V capacitor shows values as low as 1 μ F to 2 μ F over the operating temperature range. The X5R and X7R dielectrics have





more stable characteristics and are more suitable for output capacitor use. The X7R type has better stability over temperature, while the X5R is less expensive and available in higher values.

Voltage and temperature coefficients are not the only problem sources. Some ceramic capacitors have a piezoelectric response. A piezoelectric device generates voltage across its terminals due to mechanical stress, similar to the way a piezoelectric accelerometer or microphone works. For a ceramic capacitor, the stress can be induced by vibrations in the system or thermal transients. The resulting voltages can cause appreciable amounts of noise, especially when a ceramic capacitor is used for noise bypassing. A ceramic capacitor produced Figure B4's trace in response to light tapping from a pencil. Similar vibration-induced behavior can masquerade as increased output voltage noise.



Figure B1. LT1763 Regulator Stability for Various Output and Bypass (C_{BYP}) Capacitor Characteristics



Figure B3. Ceramic Capacitor Temperture Characteristics Show Large Capacitance Shift. Effect Should Be Considered When Determining Circuit Error Budget



Figure B2. Ceramic Capacitor DC Bias Characteristics Indicate Pronounced Voltage Dependence. Device Must Provide Desired Capacitance Value at Operating Voltage



Figure B4. A Ceramic Capacitor Responds to Light Pencil Tapping. Piezoelectric Based Response Approaches 80µV_{P-P}

OUTPUT VOLTAGE NOISE

Measuring output voltage noise can be a tricky process, further complicated by the low levels of noise inherent in a circuit such as this. Consideration must be given to regulator operating conditions, as well as the noise bandwidth of interest. Linear Technology has invested an enormous amount of time to provide accurate, relevant data to customers regarding noise performance. For further information on measuring output voltage noise, see Linear Technology Application Note 83, "Performance Verification of Low Noise, Low Dropout Regulators."

Noise Testing Considerations

What noise bandwidth is of interest and why is it interesting? In most systems, the range of 10Hz to 100kHz is the information signal processing area of concern. Additionally, linear regulators produce little noise energy outside this region.¹ These considerations suggest a measurement bandpass of 10Hz to 100kHz, with steep slopes at the band limits. Figure 2 shows a conceptual filter for LDO noise testing. The Butterworth sections are the key to steep slopes and flatness in the passband. The small input level requires 60dB of low noise gain to provide adequate signal for the Butterworth filters. Figure 3 details the filter scheme. The regulator under test is at the diagram's center.² A1–A3 make up a 60dB gain highpass section. A1 and A2, extremely low noise devices (<1nV \sqrt{Hz}), comprise a 60dB gain stage with a 5Hz highpass input. A3 provides a 10Hz, 2nd order Butterworth highpass characteristic. The LTC[®]1562 filter block is arranged as a 4th order Butterworth lowpass. Its output is delivered via the 330µF-100Ω highpass network. The circuit's output drives a thermally responding RMS voltmeter.³ Note that all circuit power is furnished by batteries, precluding ground loops from corrupting the measurement.

Note 1: Switching regulators are an entirely different proposition, requiring very broadband noise measurement.

Note 2: Component choice for the regulator, more critical than might be supposed, is discussed in "Capacitor Selection Considerations." **Note 3:** The choice of the RMS voltmeter is absolutely crucial to obtaining meaningful measurements. See Appendix C, Application Note 83 "Understanding and Selecting RMS Voltmeters."



Figure 2. Filter Structure for Noise Testing LDOs. Butterworth Sections Provide Appropriate Response in Desired Frequency Range





Figure 3. Implementation of Figure 2. Low Noise Amplifiers Provide Gain and Initial Highpass Shaping. LTC1562 Filter Supplies 4th Order Butterworth Lowpass Characteristic



PCB LAYOUT AND FILM





Layer 4, Solder Side*



* These layers are shorted to L1 with Vias and function as heat dispersants.



PC FAB DRAWING



NOTES: UNLESS OTHERWISE SPECIFIED

- 1. MATERIAL: FR4 OR EQUIVALENT EPOXY, 2 0Z. COPPER CLAD THICKNESS 0.062 0.006 TOTAL OF 4 LAYERS.
- FINISH: ALL PLATED HOLES 0.001 MIN./0.005 MAX. COPPER PLATE ELECTRODEPOSITED TIN-LEAD COMPOSITION BEFORE REFLOW. SOLDER MASK OVER BARE COPPER (SMOBC).
- 3. SOLDER MASK: BOTH SIDES USING LPI OR EQUIVALENT.
- 4. SILKSCREEN: USING WHITE EPOXY NON-CONDUCTIVE INK.
- 5. UNUSED SMD COMPONENTS SHOULD BE FREE OF SOLDER.
- 6. FILL UP ALL VIAS WITH SOLDER.

7. SCORING:



0.017

SYMBOL	DIAMETER	NUMBER OF HOLES	PLATED		
Α	0.02	25	YES		
В	0.035	2	YES		
С	0.064	4	YES		
D	0.07	2	NO		
TOTAL HOLES 33					



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