# $\mathcal{C Y}$ LIVAR LT1170/LT1171/LT1172 $100 \mathrm{kHz}, 5 \mathrm{~A}, 2.5 \mathrm{~A}$ and 1.25 A High Efficiency Switching Regulators 

## feATURES

- Wide Input Voltage Range: 3V to 60V
- Low Quiescent Current: 6mA
- Internal 5A Switch
(2.5A for LT1171, 1.25A for LT1172)
- Shutdown Mode Draws Only 50^A Supply Current
- Very Few External Parts Required
- Self-Protected Against Overloads
- Operates in Nearly All Switching Topologies
- Flyback-Regulated Mode Has Fully Floating Outputs
- Comes in Standard 5-Pin Packages
- LT1172 Available in 8-Pin MiniDIP and

Surface Mount Packages

- Can Be Externally Synchronized


## APPLICATIONS

- Logic Supply 5V at 10A
- 5V Logic to $\pm 15 \mathrm{~V}$ Op Amp Supply
- Battery Upconverter
- Power Inverter (+ to -) or (- to +)
- Fully Floating Multiple Outputs


## USER NOTE:

This data sheet is only intended to provide specifications, graphs, and a general functional description of the LT1170/LT1171/LT1172. Application circuits are included to show the capability of the LT1170/LT1171/LT1172. A complete design manual (AN19) should be obtained to assist in developing new designs. This manual contains a comprehensive discussion of both the LT1070 and the external components used with it, as well as complete formulas for calculating the values of these components. The manual can also be used for the LT1170/LT1171/LT1172 by factoring in the higher frequency. A CAD design program called SwitcherCAD is also available.

## DESCRIPTIOn

The LT ${ }^{\oplus 1170 / L T 1171 / L T 1172 ~ a r e ~ m o n o l i t h i c ~ h i g h ~ p o w e r-~}$ switching regulators. They can be operated in all standard switching configurations including buck, boost, flyback, forward, inverting and "Cuk." A high current, high efficiency switch is included on the die along with all oscillator, control and protection circuitry. Integration of all functions allows the LT1170/LT1171/LT1172 to be built in a standard 5-pin T0-3 or T0-220 power package as well as the 8-pin packages (LT1172). This makes them extremely easy to use and provides "bust proof" operation similar to that obtained with 3-pin linear regulators.
The LT1170/LT1171/LT1172 operate with supply voltages from 3 V to 60 V , and draw only 6 mA quiescent current. They can deliver load power up to 100W with no external power devices. By utilizing current-mode switching techniques, they provide excellent AC and DC load and line regulation.

The LT1170/LT1171/LT1172 have many unique features not found even on the vastly more difficult to use low power control chips presently available. They use adaptive antisat switch drive to allow very wide ranging load currents with no loss in efficiency. An externally activated shutdown mode reduces total supply current to $50 \mu \mathrm{~A}$ typically for standby operation.
$\boldsymbol{\boxed { \top }}$, LT, LTC, LTM, Linear Technology, the Linear logo are registered trademarks of Linear Technology Corporation. All other trademarks are the property of their respective owners.

## TYPICAL APPLICATION



## Maximum Output Power*



* ROUGH GUIDE ONLY. BUCK MODE $P_{\text {OUT }}=(5 A)\left(V_{\text {OUT }}\right)$ SPECIAL TOPOLOGIES DELIVER SPECIAL TOPOL
MORE POWER. ** DIVIDE VERTICAL POWER SCALE BY TWO FOR LT1171, BY FOUR FOR LT1172.


## ABSOLUTE MAXIMUM RATIOGS

(Note 1)

Operating Junction Temperature Range
LT1170M/LT1171M (OBSOLETE) ....... $-55^{\circ} \mathrm{C}$ to $150^{\circ} \mathrm{C}$
LT1172M ........................................... $-55^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$
LT1170/LT1171/LT1172HVC, LT1170/LT1171/LT1172C (Oper.)............. $0^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$ LT1170/LT1171/LT1172HVC LT1170/LT1171/LT1172C (Sh. Ckt.) ........ $0^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ LT1170/LT1171/LT1172HVI, LT1170/LT1171/LT1172I (Oper.).......... $-40^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$ LT1170/LT1171/LT1172HVI, LT1170/LT1171/LT1172I (Sh. Ckt.)...... $-40^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$
pIn CONFIGURATION

| * Do not connect Pin 4 of the LT1172 DIP or SO to external circuitry. This pin may be active in future revisions. | 4-LEAD TO-3 METAL CAN <br> LT1170MK: $\mathrm{T}_{\mathrm{JMAX}}=150^{\circ} \mathrm{C}, \theta_{\mathrm{JC}}=2^{\circ} \mathrm{C} / \mathrm{W}, \theta_{\mathrm{JA}}=35^{\circ} \mathrm{C} / \mathrm{W}$ <br> LT1170CK: TJMAX $=100^{\circ} \mathrm{C}, \theta_{\mathrm{JC}}=2^{\circ} \mathrm{C} / \mathrm{W}, \theta_{\mathrm{JA}}=35^{\circ} \mathrm{C} / \mathrm{W}$ <br> LT1171MK: $\mathrm{JJMAX}=150^{\circ} \mathrm{C}, \theta_{\mathrm{JC}}=4^{\circ} \mathrm{C} / \mathrm{W}, \theta_{\mathrm{JA}}=35^{\circ} \mathrm{C} / \mathrm{W}$ <br> LT1171CK: $T_{\text {JMAX }}=100^{\circ} \mathrm{C}, \theta_{J C}=4^{\circ} \mathrm{C} / \mathrm{W}, \theta_{\mathrm{JA}}=35^{\circ} \mathrm{C} / \mathrm{W}$ <br> LT1172MK: TJMAX $=150^{\circ} \mathrm{C}, \theta_{\mathrm{JC}}=8^{\circ} \mathrm{C} / \mathrm{W}, \theta_{\mathrm{JA}}=35^{\circ} \mathrm{C} / \mathrm{W}$ <br> LT1172CK: $T_{J M A X}=100^{\circ} \mathrm{C}, \theta_{\mathrm{JC}}=8^{\circ} \mathrm{C} / \mathrm{W}, \theta_{\mathrm{JA}}=35^{\circ} \mathrm{C} / \mathrm{W}$ Based on continuous operation. <br> $T_{\text {JMAX }}=125^{\circ} \mathrm{C}$ for intermittent fault conditions. <br> OBSOLETE | * Do not connect Pin 4 of the LT1172 DIP or SO to external circuitry. This pin may be active in future revisions. |
| :---: | :---: | :---: |
| * $\theta$ will vary from approximately $25^{\circ} \mathrm{C} / \mathrm{W}$ with 2.8 sq . in. of $10 z$. copper to $45^{\circ} \mathrm{C} / \mathrm{W}$ with 0.20 sq . in. of $10 z$. copper. Somewhat lower values can be obtained with additional copper layers in multilayer boards. |  |  |

## ORDER INFORMATION

http://www.linear.com/product/LT1170\#orderinfo

| LEAD FREE FINISH | TAPE AND REEL | PART MARKING* | PACKAGE DESCRIPTION | TEMPERATURE RANGE |
| :---: | :---: | :---: | :---: | :---: |
| LT1172MJ8 | LT1172MJ8\#TR | LT1172 | 8-Lead CERDIP | $-55^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ |
| LT1172CJ8\#PBF (OBSOLETE) | LT1172CJ8\#TRPBF |  | 8-Lead CERDIP | $0^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$ |
| LT1170MK\#PBF (OBSOLETE) | LT1170MK\#TRPBF |  | 4-Lead TO-3 Metal Can | $-55^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ |
| LT1170CK\#PBF (OBSOLETE) | LT1170CK\#TRPBF |  | 4-Lead TO-3 Metal Can | $0^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$ |
| LT1171MK\#PBF (OBSOLETE) | LT1171MK\#TRPBF |  | 4-Lead TO-3 Metal Can | $-55^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ |
| LT1171CK\#PBF (OBSOLETE) | LT1171CK\#TRPBF |  | 4-Lead TO-3 Metal Can | $0^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$ |
| LT1172MK\#PBF (OBSOLETE) | LT1172MK\#TRPBF |  | 4-Lead TO-3 Metal Can | $-55^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ |
| LT1172CK\#PBF (OBSOLETE) | LT1172CK\#TRPBF |  | 4-Lead T0-3 Metal Can | $0^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$ |
| LT1172CN8\#PBF | LT1172CN8\#TRPBF | LT1172 | 8-Lead PDIP or 8-Lead Plastic S0 | $0^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$ |
| LT1172IN8\#PBF | LT1172IN8\#TRPBF | LT1172 | 8-Lead PDIP or 8-Lead Plastic S0 | $-40^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$ |
| LT1172CS8\#PBF | LT1172CS8\#TRPBF | 1172 | 8-Lead PDIP or 8-Lead Plastic S0 | $0^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$ |
| LT1172IS8\#PBF | LT1172IS8\#TRPBF | 11721 | 8-Lead PDIP or 8-Lead Plastic S0 | $-40^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$ |
| LT1170CQ\#PBF | LT1170CQ\#TRPBF | LT1170 | 5-Lead DD | $0^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$ |
| LT1170IQ\#PBF | LT1170IQ\#TRPBF | LT1170 | 5-Lead DD | $-40^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$ |
| LT1170HVCQ\#PBF | LT1170HVCQ\#TRPBF | LT1170HV | 5-Lead DD | $0^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$ |
| LT1171CQ\#PBF | LT1171CQ\#TRPBF | LT1171 | 5-Lead DD | $0^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$ |
| LT1171IQ\#PBF | LT1171IQ\#TRPBF | LT1171 | 5-Lead DD | $-40^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$ |
| LT1171HVCQ\#PBF | LT1171HVCQ\#TRPBF | LT1171HV | 5-Lead DD | $0^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$ |
| LT1171HVIQ\#PBF | LT1171HVIQ\#TRPBF | LT1171HV | 5-Lead DD | $-40^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$ |
| LT1172CQ\#PBF | LT1172CQ\#TRPBF | LT1172 | 5-Lead DD | $0^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$ |
| LT1172HVCQ\#PBF | LT1172HVCQ\#TRPBF | LT1172HV | 5-Lead DD | $0^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$ |
| LT1172HVIQ\#PBF | LT1172HVIQ\#TRPBF | LT1172HV | 5-Lead DD | $-40^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$ |
| LT1172CSW\#PBF | LT1172CSW\#TRPBF | LT1172CSW | 16-Lead Plastic SO Wide | $0^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$ |
| LT1170CT\#PBF | LT1170CQ\#TRPBF | LT1170 | 5-Lead Plastic T0-220 | $0^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$ |
| LT1170IT\#PBF | LT1170IT\#TRPBF | LT1170 | 5-Lead Plastic T0-220 | $-40^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$ |
| LT1170HVCT\#PBF | LT1170HVCT\#TRPBF | LT1170HV | 5-Lead Plastic T0-220 | $0^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$ |
| LT1170HVIT\#PBF | LT1170HVIT\#TRPBF | LT1170 | 5-Lead Plastic T0-220 | $-40^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$ |
| LT1171CT\#PBF | LT1171CT\#TRPBF | LT1171 | 5-Lead Plastic T0-220 | $0^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$ |
| LT1171IT\#PBF | LT1171IT\#TRPBF | LT1171 | 5-Lead Plastic T0-220 | $-40^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$ |
| LT1171HVCT\#PBF | LT1171HVCT\#TRPBF | LT1171HV | 5-Lead Plastic T0-220 | $0^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$ |
| LT1171HVIT\#PBF | LT1171HVIT\#TRPBF | LT1171HV | 5-Lead Plastic T0-220 | $-40^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$ |
| LT1172CT\#PBF | LT1172CT\#TRPBF | LT1172 | 5-Lead Plastic T0-220 | $0^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$ |
| LT1172HVCT\#PBF | LT1172HVCT\#TRPBF | LT1172HV | 5-Lead Plastic T0-220 | $0^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$ |

Consult LTC Marketing for parts specified with wider operating temperature ranges. *The temperature grade is identified by a label on the shipping container.
For more information on lead free part marking, go to: http://www.linear.com/leadfree/
For more information on tape and reel specifications, go to: http://www.linear.com/tapeandreel/. Some packages are available in 500 unit reels through designated sales channels with \#TRMPBF suffix.

## LT1170/LT1171/LT1172

 temperature range, otherwise specifications are at $T_{A}=25^{\circ} \mathrm{C} . \mathrm{V}_{I N}=15 \mathrm{~V}, \mathrm{~V}_{\mathrm{C}}=0.5 \mathrm{~V}, \mathrm{~V}_{\mathrm{FB}}=\mathrm{V}_{\mathrm{REF}}$, output pin open, unless otherwise noted.

| SYMBOL | PARAMETER |  | CONDITIONS |  |  | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\text {REF }}$ | Reference Voltage |  | Measured at Feedback Pin$V_{C}=0.8 \mathrm{~V}$ |  | $\bullet$ | $\begin{aligned} & \hline 1.224 \\ & 1.214 \end{aligned}$ | $\begin{aligned} & 1.244 \\ & 1.244 \end{aligned}$ | $\begin{aligned} & \hline 1.264 \\ & 1.274 \end{aligned}$ | V |
| $\mathrm{I}_{\mathrm{B}}$ | Feedback Input Current |  | $\mathrm{V}_{\mathrm{FB}}=\mathrm{V}_{\text {REF }}$ |  | $\bullet$ |  | 350 | $\begin{gathered} \hline 750 \\ 1100 \end{gathered}$ | nA |
| $\mathrm{g}_{\mathrm{m}}$ | Error Amplifier Transconductance |  | $\Delta I_{C}= \pm 25 \mu \mathrm{~A}$ |  | $\bullet$ | $\begin{aligned} & 3000 \\ & 2400 \end{aligned}$ | 4400 | $\begin{aligned} & 6000 \\ & 7000 \end{aligned}$ | $\mu \mathrm{mho}$ <br> $\mu \mathrm{mho}$ |
|  | Error Amplifier Source or Sink Current |  | $\mathrm{V}_{C}=1.5 \mathrm{~V}$ |  | $\bullet$ | $\begin{aligned} & 150 \\ & 120 \end{aligned}$ | 200 | $\begin{aligned} & 350 \\ & 400 \end{aligned}$ | $\mu \mathrm{A}$ $\mu \mathrm{A}$ |
|  | Error Amplifier Clamp Voltage |  | $\begin{aligned} & \text { Hi Clamp, } V_{F B}=1 \mathrm{~V} \\ & \text { Lo Clamp, } V_{F B}=1.5 \mathrm{~V} \end{aligned}$ |  |  | $\begin{aligned} & 1.80 \\ & 0.25 \end{aligned}$ | 0.38 | $\begin{aligned} & 2.30 \\ & 0.52 \end{aligned}$ | V |
|  | Reference Voltage Line Regulation |  | $\begin{aligned} & 3 \mathrm{~V} \leq \mathrm{V}_{\text {IN }} \leq \mathrm{V}_{\mathrm{MAX}} \\ & \mathrm{~V}_{\mathrm{C}}=0.8 \mathrm{~V} \end{aligned}$ |  | $\bullet$ |  |  | 0.03 | \%/V |
| $A_{V}$ | Error Amplifier Voltage Gain |  | $0.9 \mathrm{~V} \leq \mathrm{V}_{\mathrm{C}} \leq 1.4 \mathrm{~V}$ |  |  | 500 | 800 |  | V/V |
|  | Minimum Input Voltage (Note 5) |  |  |  | $\bullet$ |  | 2.6 | 3.0 | V |
| IQ | Supply Current |  | $3 \mathrm{~V} \leq \mathrm{V}_{\text {IN }} \leq \mathrm{V}_{\mathrm{MAX}}, \mathrm{V}_{\mathrm{C}}=0.6 \mathrm{~V}$ |  |  |  | 6 | 9 | mA |
|  | Control Pin Threshold |  | Duty Cycle $=0$ |  | $\bullet$ | $\begin{aligned} & 0.8 \\ & 0.6 \end{aligned}$ | 0.9 | $\begin{aligned} & 1.08 \\ & 1.25 \end{aligned}$ | V |
|  | Normal/Flyback Threshold on Feedback Pin |  |  |  |  | 0.4 | 0.45 | 0.54 | V |
| $V_{\text {FB }}$ | Flyback Reference Voltage (Note 5) |  | $\mathrm{I}_{\text {FB }}=50 \mu \mathrm{~A}$ |  | $\bullet$ | $\begin{aligned} & \hline 15.0 \\ & 14.0 \end{aligned}$ | 16.3 | $\begin{aligned} & 17.6 \\ & 18.0 \end{aligned}$ | V |
|  | Change in Flyback Reference Voltage |  | $0.05 \leq \mathrm{I}_{\text {FB }} \leq 1 \mathrm{~mA}$ |  |  | 4.5 | 6.8 | 9 | V |
|  | Flyback Reference Voltage Line Regulation (Note 5) |  | $\begin{aligned} & l_{\text {FB }}=50 \mu \mathrm{~A} \\ & 7 \mathrm{~V} \leq \mathrm{V}_{\text {IN }} \leq \mathrm{V}_{\mathrm{MAX}} \end{aligned}$ |  |  |  | 0.01 | 0.03 | \%/V |
|  | Flyback Amplifier Transconductance ( $\mathrm{gm}_{\mathrm{m}}$ ) |  | $\Delta \mathrm{I}_{\mathrm{C}}= \pm 10 \mu \mathrm{~A}$ |  |  | 150 | 300 | 650 | $\mu \mathrm{mho}$ |
|  | Flyback Amplifier Source and Sink Current |  | $V_{C}=0.6 \mathrm{~V}$ Source <br> $I_{F B}=50 \mu \mathrm{~A}$ Sink |  | $\bullet$ | $\begin{aligned} & \hline 15 \\ & 25 \end{aligned}$ | $\begin{aligned} & \hline 32 \\ & 40 \end{aligned}$ | $\begin{aligned} & 70 \\ & 70 \end{aligned}$ | $\begin{aligned} & \mathrm{mA} \\ & \mathrm{~mA} \end{aligned}$ |
| BV | Output Switch Breakdown Voltage |  | $3 \mathrm{~V} \leq \mathrm{V}_{\text {IN }} \leq \mathrm{V}_{\text {MAX }}$, LT1170/LT1171/LT1172 <br> $\mathrm{I}_{\text {SW }}=1.5 \mathrm{~mA}$ LT1170HV/LT1171HV/LT1172HV <br>  LT1172S8 |  | $\stackrel{\bullet}{\bullet}$ | $\begin{aligned} & 65 \\ & 75 \\ & 60 \end{aligned}$ | $\begin{aligned} & 90 \\ & 90 \\ & 80 \end{aligned}$ |  | V V V |
| $\overline{V_{S A T}}$ | Output Switch "On" Resistance (Note 3) |  | $\begin{aligned} & \text { LT1170 } \\ & \text { LT1171 } \\ & \text { LT1172 } \end{aligned}$ |  | $\stackrel{\bullet}{\bullet}$ |  | $\begin{aligned} & 0.15 \\ & 0.30 \\ & 0.60 \end{aligned}$ | $\begin{aligned} & 0.24 \\ & 0.50 \\ & 1.00 \end{aligned}$ | $\Omega$ $\Omega$ $\Omega$ |
|  | Control Voltage to Switch Current Transconductance |  | $\begin{aligned} & \text { LT1170 } \\ & \text { LT1171 } \\ & \text { LT1172 } \end{aligned}$ |  |  |  | 8 4 2 |  | A $/ V$ A $V$ A $/ 2$ |
| $\overline{\mathrm{ILIM}}$ | Switch Current Limit | (LT1170) | $\begin{array}{\|l\|} \hline \text { Duty Cycle }=50 \% \\ \text { Duty Cycle }=50 \% \\ \text { Duty Cycle }=80 \% \text { (Note 4) } \\ \hline \end{array}$ | $\begin{aligned} & \mathrm{T}_{\mathrm{J}} \geq 25^{\circ} \mathrm{C} \\ & \mathrm{~T}_{\mathrm{J}}<25^{\circ} \mathrm{C} \end{aligned}$ | $\stackrel{\bullet}{\bullet}$ | 5 5 4 |  | $\begin{aligned} & 10 \\ & 11 \\ & 10 \end{aligned}$ | A A A |
|  |  | (LT1171) | $\begin{array}{\|l} \mid \text { Duty Cycle }=50 \% \\ \text { Duty Cycle }=50 \% \\ \text { Duty Cycle }=80 \% \text { (Note 4) } \end{array}$ | $\begin{aligned} & \mathrm{T}_{J} \geq 25^{\circ} \mathrm{C} \\ & \mathrm{~T}_{\mathrm{J}}<25^{\circ} \mathrm{C} \end{aligned}$ | $\stackrel{\bullet}{\bullet}$ | $\begin{aligned} & 2.5 \\ & 2.5 \\ & 2.0 \end{aligned}$ |  | $\begin{aligned} & 5.0 \\ & 5.5 \\ & 5.0 \end{aligned}$ | A |
|  |  | (LT1172) | $\begin{array}{\|l\|} \hline \text { Duty Cycle }=50 \% \\ \text { Duty Cycle }=50 \% \\ \text { Duty Cycle }=80 \% \text { (Note 4) } \\ \hline \end{array}$ | $\begin{aligned} & \mathrm{T}_{J} \geq 25^{\circ} \mathrm{C} \\ & \mathrm{~T}_{\mathrm{J}}<25^{\circ} \mathrm{C} \end{aligned}$ | $\stackrel{\bullet}{\bullet}$ | $\begin{aligned} & 1.25 \\ & 1.25 \\ & 1.00 \end{aligned}$ |  | $\begin{aligned} & 3.0 \\ & 3.5 \\ & 2.5 \end{aligned}$ | A |
| $\frac{\Delta l_{\mathrm{IN}}}{\Delta I_{\mathrm{SW}}}$ | Supply Current Increase During Switch On-Time |  |  |  |  |  | 25 | 35 | $\mathrm{mA} / \mathrm{A}$ |
| f | Switching Frequency |  |  |  | $\bullet$ | $\begin{aligned} & \hline 88 \\ & 85 \end{aligned}$ | 100 | $\begin{aligned} & 112 \\ & 115 \end{aligned}$ | $\begin{aligned} & \mathrm{kHz} \\ & \mathrm{kHz} \end{aligned}$ |

ELECTRICAL CHARACTERISTICS The odennes sthe seneifitaiolons which paply ver the tull operating temperature range, otherwise specifications are at $T_{A}=25^{\circ} \mathrm{C} . \mathrm{V}_{I N}=15 \mathrm{~V}, \mathrm{~V}_{\mathrm{C}}=0.5 \mathrm{~V}, \mathrm{~V}_{\mathrm{FB}}=\mathrm{V}_{\mathrm{REF}}$, output pin open, unless otherwise noted.

| SYMBOL | PARAMETER | CONDITIONS | MIN | TYP | MAX | UNITS |  |
| :--- | :--- | :--- | :---: | :---: | :---: | :---: | :---: |
| $D_{\text {MAX }}$ | Maximum Switch Duty Cycle |  | $\bullet$ | 85 | 92 | 97 | $\%$ |
|  | Shutdown Mode | $3 \mathrm{~V} \leq \mathrm{V}_{\text {IN }} \leq \mathrm{V}_{\text {MAX }}$ |  | 100 | 250 | $\mu \mathrm{~A}$ |  |
|  | Supply Current | $\mathrm{V}_{\mathrm{C}}=0.05 \mathrm{~V}$ |  |  |  |  |  |
|  | Shutdown Mode | $3 \mathrm{~V} \leq \mathrm{V}_{\text {IN }} \leq \mathrm{V}_{\text {MAX }}$ | $\bullet$ | 100 | 150 | 250 | mV |
|  | Threshold Voltage |  |  |  | 1.5 | 300 | mV |
|  | Flyback Sense Delay Time (Note 5) |  | $\mu \mathrm{S}$ |  |  |  |  |

Note 1: Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. Exposure to any Absolute Maximum Rating condition for extended periods may affect device reliability and lifetime.
Note 2: Minimum effective switch "on" time for the LT1170/LT1171/ LT1172 (in current limit only) is $\approx 0.6 \mu \mathrm{~s}$. This limits the maximum safe input voltage during an output shorted condition. Buck mode and inverting mode input voltage during an output shorted condition is limited to:
$V_{\text {IN }}(\max$, output shorted $)=15 \mathrm{~V}+\frac{(\mathrm{R})\left(\mathrm{I}_{\mathrm{L}}\right)+\mathrm{Vf}}{(\mathrm{t})(\mathrm{f})}$ buck and inverting mode
$\mathrm{R}=$ Inductor DC resistance
$I_{L}=10 A$ for LT1170, 5A for LT1171, and 2.5A for LT1172
$\mathrm{Vf}=$ Output catch diode forward voltage at $\mathrm{I}_{\mathrm{L}}$
$t=0.6 \mu \mathrm{~s}, \mathrm{f}=100 \mathrm{kHz}$ switching frequency
Maximum input voltage can be increased by increasing R or Vf.
External current limiting such as that shown in AN19, Figure 39, will provide protection up to the full supply voltage rating. C1 in Figure 39 should be reduced to 200pF.

Transformer designs will tolerate much higher input voltages because leakage inductance limits rate of rise of current in the switch. These designs must be evaluated individually to assure that current limit is well controlled up to maximum input voltage.
Boost mode designs are never protected against output shorts because the external catch diode and inductor connect input to output.
Note 3: Measured with $\mathrm{V}_{\mathrm{C}}$ in hi clamp, $\mathrm{V}_{\mathrm{FB}}=0.8 \mathrm{~V}$. $\mathrm{I}_{\mathrm{SW}}=4 \mathrm{~A}$ for LT1170, 2A for LT1171, and 1A for LT1172.
Note 4: For duty cycles (DC) between $50 \%$ and $80 \%$, minimum guaranteed switch current is given by $\mathrm{I}_{\mathrm{LIM}}=3.33(2-\mathrm{DC})$ for the $\mathrm{LT1170}, \mathrm{I}_{\text {LIM }}=1.67$ (2-DC) for the LT1171, and $\mathrm{I}_{\text {LIM }}=0.833(2-\mathrm{DC})$ for the LT1172.
Note 5: Minimum input voltage for isolated flyback mode is $7 \mathrm{~V} . \mathrm{V}_{\mathrm{MAX}}=55 \mathrm{~V}$ for HV grade in fully isolated mode to avoid switch breakdown.

## LT1170/LT1171/LT1172

## TYPICAL PERFORMANCE CHARACTERISTICS




Minimum Input Voltage


Reference Voltage vs Temperature


Switch Saturation Voltage


Feedback Bias Current vs Temperature


1170/1/2 G06

Supply Current vs Supply Voltage
(Shutdown Mode)


Driver Current* vs Switch Current


* AVERAGE LT1170 POWER SUPPLY CURRENT IS FOUND BY MULTIPLYING DRIVER CURRENT BY DUTY CYCLE, THEN ADDING QUIESCENT CURRENT.

Supply Current vs Input Voltage*


* UNDER VERY LOW OUTPUT CURRENT CONDITIONS, DUTY CYCLE FOR MOST CIRCUITS WILL APPROACH 10\% OR LESS.


## TYPICAL PERFORMANCE CHARACTERISTICS



1170/1/2 G10

Feedback Pin Clamp Voltage


Flyback Blanking Time




Error Amplifier Transconductance


Isolated Mode Flyback Reference Voltage



1170/1/2 G16

## LT1170/LT1171/LT1172

## TYPICAL PERFORMANCE CHARACTERISTICS




## BLOCK DIAGRAM


$\dagger$ ALWAYS CONNECT E1 TO THE GROUND PIN ON MINIDIP, 8- AND 16-PIN SURFACE MOUNT PACKAGES. E1 AND E2 INTERNALLY TIED TO GROUND ON TO-3 AND TO-220 PACKAGES.

## operation

The LT1170/LT1171/LT1172 are current mode switchers. This means that switch duty cycle is directly controlled by switch current rather than by output voltage. Referring to the block diagram, the switch is turned "on" at the start of each oscillator cycle. It is turned "off" when switch current reaches a predetermined level. Control of output voltage is obtained by using the output of a voltage sensing error amplifier to set current trip level. This technique has several advantages. First, it has immediate response to input voltage variations, unlike ordinary switchers which have notoriously poor line transient response. Second, it reduces the $90^{\circ}$ phase shift at midfrequencies in the energy storage inductor. This greatly simplifies closed loop frequency compensation under widely varying input voltage or output load conditions. Finally, it allows simple pulse-by-pulse current limiting to provide maximum switch protection under output overload or short conditions. A low dropout internal regulator provides a 2.3 V supply for all internal circuitry on the LT1170/LT1171/LT1172. This low dropout design allows input voltage to vary from 3 V to 60 V with virtually no change in device performance. A 100 kHz oscillator is the basic clock for all internal timing. It turns "on" the output switch via the logic and driver circuitry. Special adaptive anti-sat circuitry detects onset of saturation in the power switch and adjusts driver current instantaneously to limit switch saturation. This minimizes driver dissipation and provides very rapid turnoff of the switch.

A 1.2V bandgap reference biases the positive input of the error amplifier. The negative input is brought out for output voltage sensing. This feedback pin has a second function; when pulled low with an external resistor, it programs the LT1170/LT1171/LT1172 to disconnect the mainerroramplifier output and connects the output of the flyback amplifier to the comparator input. The LT1170/LT1171/LT1172 will then regulate the value of the flyback pulse with respect to the supply voltage.* This flyback pulse is directly proportional to output voltage in the traditional transformer coupled flyback topology regulator. By regulating the amplitude of the flyback pulse, the output voltage can be regulated with no direct connection between input and output. The output is fully floating up to the breakdown voltage of the transformer windings. Multiple floating outputs are easily obtained with additional windings.

Aspecial delay network inside the LT1170/LT1171/LT1172 ignores the leakage inductance spike at the leading edge of the flyback pulse to improve output regulation.

The error signal developed at the comparator input is brought out externally. This pin $\left(\mathrm{V}_{\mathrm{C}}\right)$ has four different functions. It is used for frequency compensation, current limit adjustment, soft-starting, and total regulator shutdown. During normal regulator operation this pin sits at a voltage between 0.9 V (low output current) and 2.0V (high output current). The error amplifiers are current output ( $\mathrm{g}_{\mathrm{m}}$ ) types, so this voltage can be externally clamped for adjusting current limit. Likewise, a capacitor coupled external clamp will provide soft-start. Switch duty cycle goes to zero if the $V_{C}$ pin is pulled to ground through a diode, placing the LT1170/LT1171/LT1172 in an idle mode. Pulling the $V_{C}$ pin below 0.15 V causes total regulator shutdown, with only $50 \mu \mathrm{~A}$ supply current for shutdown circuitry biasing. See Application Note 19 for full application details.

## Extra Pins on the MiniDIP and Surface Mount Packages

The 8- and 16-pin versions of the LT1172 have the emitters of the power transistor brought out separately from the ground pin. This eliminates errors due to ground pin voltage drops and allows the user to reduce switch current limit 2:1 by leaving the second emitter (E2) disconnected. The first emitter (E1) should always be connected to the ground pin. Note that switch "on" resistance doubles when E2 is left open, so efficiency will suffer somewhat when switch currents exceed 300mA. Also, note that chip dissipation will actually increase with E2 open during normal Ioad operation, even though dissipation in current limit mode will decrease. See "Thermal Considerations" next.

## Thermal Considerations When Using the MiniDIP and SW Packages

The low supply current and high switch efficiency of the LT1172 allow it to be used without a heat sink in most applications when the TO-220 or T0-3 package is selected. These packages are rated at $50^{\circ} \mathrm{C} / \mathrm{W}$ and $35^{\circ} \mathrm{C} / \mathrm{W}$ respectively. The miniDIPs, however, are rated at $100^{\circ} \mathrm{C} / \mathrm{W}$ in ceramic ( J ) and $130^{\circ} \mathrm{C} / \mathrm{W}$ in plastic (N).

[^0]
## operation

Care should be taken forminiDIP applications to ensure that the worst case input voltage and load current conditions do not cause excessive die temperatures. The following formulas can be used as a rough guide to calculate LT1172 power dissipation. For more details, the reader is referred to Application Note 19 (AN19), "Efficiency Calculations" section.
Average supply current (including driver current) is:

$$
\begin{aligned}
& \mathrm{I}_{\mathrm{IN}} \approx 6 \mathrm{~mA}+\mathrm{I}_{\mathrm{SW}}(0.004+\mathrm{DC} / 40) \\
& \mathrm{I}_{\mathrm{SW}}=\text { switch current } \\
& \mathrm{DC}=\text { switch duty cycle }
\end{aligned}
$$

Switch power dissipation is given by:

$$
\begin{aligned}
& \mathrm{P}_{\mathrm{SW}}=\left(\mathrm{I}_{\mathrm{SW}}\right)^{2} \bullet\left(\mathrm{R}_{\mathrm{SW}}\right)(\mathrm{DC}) \\
& \mathrm{R}_{\mathrm{SW}}=\mathrm{LT} 1172 \text { switch "on" resistance }(1 \Omega \text { maximum })
\end{aligned}
$$

Total power dissipation is the sum of supply current times input voltage plus switch power:

$$
P_{D(T O T)}=\left(I_{I N}\right)\left(V_{I N}\right)+P_{S W}
$$

In a typical example, using a boost converter to generate 12 V at 0.12 A from a 5 V input, duty cycle is approximately $60 \%$, and switch current is about 0.65 A , yielding:

$$
\begin{aligned}
& I_{I N}=6 \mathrm{~mA}+0.65(0.004+\mathrm{DC} / 40)=18 \mathrm{~mA} \\
& \mathrm{P}_{\mathrm{SW}}=(0.65)^{2} \cdot(1 \Omega)(0.6)=0.25 \mathrm{~W} \\
& \mathrm{P}_{\mathrm{D}(\text { TOT })}=(5 \mathrm{~V})(0.018 \mathrm{~A})+0.25=0.34 \mathrm{~W}
\end{aligned}
$$

Temperature rise in a plastic miniDIP would be $130^{\circ} \mathrm{C} / \mathrm{W}$ times 0.34 W , or approximately $44^{\circ} \mathrm{C}$. The maximum ambient temperature would be limited to $100^{\circ} \mathrm{C}$ (commercial temperature limit) minus $44^{\circ} \mathrm{C}$, or $56^{\circ} \mathrm{C}$.

In most applications, full load current is used to calculate die temperature. However, if overload conditions must also be accounted for, four approaches are possible. First, if loss of regulated output is acceptable under overload conditions, the internal thermal limit of the LT1172 will protect the die in most applications by shutting off switch current. Thermal limit is not a tested parameter, however, and should be considered only for noncritical applications with temporary overloads. A second approach is to use the
larger T0-220 (T) or T0-3 (K) package which, even without a heat sink, may limit die temperatures to safe levels under overload conditions. In critical situations, heat sinking of these packages is required; especially if overload conditions must be tolerated for extended periods of time.
The third approach for lower current applications is to leave the second switch emitter (miniDIP only) open. This increases switch "on" resistance by 2:1, but reduces switch current limit by $2: 1$ also, resulting in a net $2: 1$ reduction in $I^{2} R$ switch dissipation under current limit conditions.
The fourth approach is to clamp the $\mathrm{V}_{\mathrm{C}}$ pin to a voltage less than its internal clamp level of 2V. The LT1172 switch current limit is zero at approximately 1 V on the $\mathrm{V}_{\mathrm{C}}$ pin and 2 A at 2 V on the $\mathrm{V}_{\mathrm{C}}$ pin. Peak switch current can be externally clamped between these two levels with a diode. See AN19 for details.

## LT1170/LT1171/LT1172 Synchronizing

The LT1170/LT1171/LT1172 can be externally synchronized in the frequency range of 120 kHz to 160 kHz . This is accomplished as shown in the accompanying figures. Synchronizing occurs when the $V_{C}$ pin is pulled to ground with an external transistor. To avoid disturbing the DC characteristics of the internal error amplifier, the width of the synchronizing pulse should be under $0.3 \mu \mathrm{~s}$. C2 sets the pulse width at $\cong 0.2 \mu \mathrm{~s}$. The effect of a synchronizing pulse on the LT1170/LT1171/LT1172 amplifier offset can be calculated from:

$$
\Delta \mathrm{V}_{\mathrm{OS}}=\frac{\left(\frac{\mathrm{KT}}{\mathrm{q}}\right)\left(\mathrm{t}_{\mathrm{S}}\right)\left(\mathrm{f}_{\mathrm{S}}\right)\left(\mathrm{I}_{\mathrm{C}}+\frac{\mathrm{V}_{\mathrm{C}}}{\mathrm{R} 3}\right)}{\mathrm{I}_{\mathrm{C}}}
$$

$$
\begin{aligned}
\frac{\mathrm{KT}}{\mathrm{q}} & =26 \mathrm{mV} \text { at } 25^{\circ} \mathrm{C} \\
\mathrm{t}_{\mathrm{C}} & =\text { pulse width } \\
\mathrm{f}_{\mathrm{S}} & =\text { pulse frequency } \\
\mathrm{I}_{\mathrm{C}} & =\mathrm{V}_{\mathrm{C}} \text { source current }(\approx 200 \mu \mathrm{~A}) \\
\mathrm{V}_{\mathrm{C}}= & \text { operating } \mathrm{V}_{\mathrm{C}} \text { voltage }(1 \mathrm{~V} \text { to } 2 \mathrm{~V}) \\
\mathrm{R} 3= & \text { resistor used to set mid-frequency "zero" in } \\
& \text { frequency compensation network. }
\end{aligned}
$$

## OPERATION

With $\mathrm{t}_{\mathrm{S}}=0.2 \mu \mathrm{~s}, \mathrm{f}_{\mathrm{S}}=150 \mathrm{kHz}, \mathrm{V}_{\mathrm{C}}=1.5 \mathrm{~V}$, and $\mathrm{R} 3=2 \mathrm{k}$, offset voltage shift is $\approx 3.8 \mathrm{mV}$. This is not particularly bothersome, but note that high offsets could result if R3 were reduced to a much lower value. Also, the synchronizing
transistor must sink higher currents with low values of R3, so larger drives may have to be used. The transistor must be capable of pulling the $\mathrm{V}_{\mathrm{C}}$ pin to within 200 mV of ground to ensure synchronizing.

Synchronizing with Bipolar Transistor


Synchronizing with MOS Transistor


## TYPICAL APPLICATIONS

Flyback Converter


## LT1170/LT1171/LT1172

TYPICAL APPLICATIONS
(Note that maximum output currents are divided by 2 for LT1171, by 4 for LT1172.)
LCD Contrast Supply


* $V_{\text {IN }}$ AND BATTERY MAY BE TIED TOGETHER. MAXIMUM VALUE FOR V ${ }_{\text {BAT }}$ IS EQUAL TO THE |NEGATIVE OUTPUT| + 1V. WITH HIGHER BATTERY VOLTAGES, HIGHEST EFFICIENCY IS OBTAINED BY RUNNING THE LT1172 VIN PIN FROM 5V. SHUTTING OFF THE 5V SUPPLY WILL AUTOMATICALLY TURN OFF THE LT1172. EFFICIENCY IS ABOUT 80\% AT IOUT $=25 \mathrm{~mA}$.
R1, R2, R3 ARE MADE LARGE TO MINIMIZE BATTERY DRAIN IN SHUTDOWN, WHICH IS APPROXIMATELY VBAT /(R1 + R2 + R3).
** FOR HIGH EFFICIENCY, L1 SHOULD BE MADE ON A FERRITE OR MOLYPERMALLOY CORE. PEAK INDUCTOR CURRENTS ARE ABOUT 600 mA AT POUT $=0.7 \Omega$. INDUCTOR SERIES RESISTANCE SHOULD BE LESS THAN $0.4 \Omega$ FOR HIGH EFFICIENCY.
*** OUTPUT RIPPLE IS ABOUT 200mVp-p TO $400 \mathrm{mV} V_{\text {p-p }}$ WITH $C 2=2 \mu$ F TANTALUM. IF LOWER RIPPLE IS DESIRED, INCREASE C2, OR ADD A $10 \Omega, 1 \mu \mathrm{~F}$ TANTALUM OUTPUT FILTER.

Driving High Voltage FET
(for Off-Line Applications, See AN25)


External Current Limit


1170/1/2 TA06

## LT1170/LT1171/LT1172

## TYPICAL APPLICATIONS

(Note that maximum output currents are divided by 2 for LT1171, by 4 for LT1172.)

Negative-to-Positive Buck-Boost Converter ${ }^{\dagger}$


* REQUIRED IF INPUT LEADS $\geq 2$ "
** PULSE ENGINEERING 92114, COILTRONICS 50-2-52
$\dagger$ THIS CIRCUIT IS OFTEN USED TO CONVERT -48V TO 5V. TO GUARANTEE FULL SHORT-CIRCUIT PROTECTION, THE CURRENT LIMIT CIRCUIT SHOWN IN AN19, FIGURE 39, SHOULD BE ADDED WITH C1 REDUCED TO 200pF.

External Current Limit


NOTE THAT THE LT1170
1170/1/2 TA08
GND PIN IS NO LONGER COMMON TO $\mathrm{VIN}^{-}$.

Negative Buck Converter


## LT1170/LT1171/LT1172

## TYPICAL APPLICATIONS

Positive-to-Negative Buck-Boost Converter


High Efficiency Constant Current Charger


Backlight CCFL Supply (see AN45 for details)


## TYPICAL APPLICATIONS



Negative Boost Regulator


Driving High Voltage NPN


## LT1170/LT1171/LT1172

TYPICAL APPLICATIONS
Forward Converter


High Efficiency 5V Buck Converter


## PACKAGG DESCRIPTION

Please refer to http://www.linear.com/product/LT1170\#packaging for the most recent package drawings.

## J8 Package <br> 8-Lead CERDIP (Narrow . 300 Inch, Hermetic)

(Reference LTC DWG \# 05-08-1110)


## K Package

4-Lead TO-3 Metal Can
(Reference LTC DWG \# 05-08-1311)

(OBSOLETE PACKAGE)

PACKAGE DESCRIPTION
Please refer to http://www.linear.com/product/LT1170\#packaging for the most recent package drawings.

N Package
8-Lead PDIP (Narrow . 300 Inch)
(Reference LTC DWG \# 05-08-1510 Rev I)


NOTE:

1. DIMENSIONS ARE $\frac{\text { INCHES }}{\text { MILLIMETERS }}$
*THESE DIMENSIONS DO NOT INCLUDE MOLD FLASH OR PROTRUSIONS. MOLD FLASH OR PROTRUSIONS SHALL NOT EXCEED .010 INCH ( 0.254 mm )

## PACKAGE DESCRIPTION

Please refer to http://www.linear.com/product/LT1170\#packaging for the most recent package drawings.

Q Package
5-Lead Plastic DD Pak
(Reference LTC DWG \# 05-08-1461 Rev F)



RECOMMENDED SOLDER PAD LAYOUT NOTE:

1. DIMENSIONS IN INCH/(MILLIMETER)
2. DRAWING NOT TO SCALE


RECOMMENDED SOLDER PAD LAYOUT FOR THICKER SOLDER PASTE APPLICATIONS

Q(DD5) 0811 REV F

PACKAGE DESCRIPTION
Please refer to http://www.linear.com/product/LT1170\#packaging for the most recent package drawings.

## S8 Package

8-Lead Plastic Small Outline (Narrow . 150 Inch)
(Reference LTC DWG \# 05-08-1610 Rev G)


## PACKAGE DESCRIPTION

## Please refer to http://www.linear.com/product/LT1170\#packaging for the most recent package drawings.

## SW Package

16-Lead Plastic Small Outline (Wide $\mathbf{. 3 0 0}$ Inch)
(Reference LTC DWG \# 05-08-1620)


1. DIMENSIONS IN $\frac{\text { INCHES }}{\text { (MILLIMETERS) }}$

S16 (WIDE) 0502
2. DRAWING NOT TO SCALE
3. PIN 1 IDENT, NOTCH ON TOP AND CAVITIES ON THE BOTTOM OF PACKAGES ARE THE MANUFACTURING OPTIONS.

THE PART MAY BE SUPPLIED WITH OR WITHOUT ANY OF THE OPTIONS
4. THESE DIMENSIONS DO NOT INCLUDE MOLD FLASH OR PROTRUSIONS.

MOLD FLASH OR PROTRUSIONS SHALL NOT EXCEED .006" (0.15mm)

PACKAGE DESCRIPTION
Please refer to http://www.linear.com/product/LT1170\#packaging for the most recent package drawings.

T Package
5-Lead Plastic T0-220 (Standard)
(Reference LTC DWG \# 05-08-1421)


## REVISIOC HISTORY (Revision history begins at Rev $G$ )

| REV | DATE | DESCRIPTION | PAGE NUMBER |
| :---: | :---: | :--- | :---: |
| G | $3 / 10$ | Updated to Reactivate LT1172M from Obsoleted Parts List | 2 |
| H | $6 / 16$ | Removed \#PBF from MJ8 part number in first line | 3 |

## LT1170/LT1171/LT1172

## TYPICAL APPLICATION

Positive Current Boosted Buck Converter


## RELATED PARTS

| PART NUMBER | DESCRIPTION | COMMENTS |
| :---: | :---: | :---: |
| LT1070/LT1071/LT1072 | 5A/2.5A/1.25A High Efficiency Switching Regulators | 40 kHz , $\mathrm{V}_{\text {IN }}$ to 60V, $\mathrm{V}_{\text {SW }}$ to 75 V |
| LT1074/LT1076 | 5.5A/2A Step-Down Switching Regulators | 100kHz, Also for Positive-to-Negative Conversion |
| LT1082 | 1A, High Voltage, High Efficiency Switching Regulator | $\mathrm{V}_{\text {IN }}$ to 75 V , $\mathrm{V}_{\text {SW }}$ to 100 V , Telecom |
| LT1268/LT1268B | 7.5A, 150kHz Switching Regulators | $\mathrm{V}_{\text {IN }}$ to 30V, $\mathrm{V}_{\text {SW }}$ to 60 V |
| LT1269/LT1271 | 4A High Efficiency Switching Regulators | $100 \mathrm{kHz} / 60 \mathrm{kHz}$, VIN to 30 V , $\mathrm{V}_{\text {SW }}$ to 60 V |
| LT1270/LT1270A | 8A and 10A High Efficiency Switching Regulators | 60 kHz , $\mathrm{V}_{\text {IN }}$ to $30 \mathrm{~V}, \mathrm{~V}_{\text {SW }}$ to 60 V |
| LT1370 | 500kHz High Efficiency 6A Switching Regulator | High Power Boost, Flyback, SEPIC |
| LT1371 | 500kHz High Efficiency 3A Switching Regulator | Good for Boost, Flyback, Inverting, SEPIC |
| LT1372/LT1377 | 500kHz and 1MHz High Efficiency 1.5A Switching Regulators | Directly Regulates $\pm \mathrm{V}_{\text {OUT }}$ |
| $\underline{\text { LT1373 }}$ | 250kHz Low Supply Current High Efficiency 1.5A Switching Regulator | Low 1mA Quiescent Current |
| LT1374 | 4A, 500kHz Step-Down Switching Regulator | Synchronizable, $\mathrm{V}_{\text {IN }}$ to 25 V |
| LT1375/LT1376 | 1.5A, 500kHz Step-Down Switching Regulators | Up to 1.25A Out from an S0-8 |
| LT1425 | Isolated Flyback Switching Regulator | 6W Output, $\pm 5 \%$ Regulation, No Optocoupler Needed |
| LT1507 | 500 kHz Monolithic Buck Mode Switching Regulator | 1.5A Switch, Good for 5V to 3.3V |
| LT1533 | Ultralow Noise 1A Switching Regulator | Push-Pull, <100 $\mathrm{V}_{\text {P-p }}$ Output Noise |


[^0]:    *See note under Block Diagram

