

# 20 GHz to 54 GHz, GaAs, pHEMT, MMIC, 29 dBm (0.5 W) Power Amplifier

Data Sheet ADPA7009CHIP

#### **FEATURES**

Output P1dB: 28.5 dBm typical at 24 GHz to 36 GHz

P<sub>SAT</sub>: 29 dBm typical at 24 GHz to 36 GHz Gain: 19.5 dB typical at 24 GHz to 36 GHz

Input return loss: 17.5 dB typical at 24 GHz to 36 GHz
Output return loss: 22.0 dB typical at 24 GHz to 36 GHz
Output IP3: 35 dBm typical at 24 GHz to 36 GHz

Supply voltage: 5 V typical at 750 mA  $50 \Omega$  matched input and output

Die size: 2.750 mm × 1.845 mm× 0.102 mm

#### **APPLICATIONS**

Military and space
Test instrumentation
Satellite communications

#### **GENERAL DESCRIPTION**

The ADPA7009CHIP is a gallium arsenide (GaAs), pseudomorphic high electron mobility transistor (pHEMT), monolithic microwave integrated circuit (MMIC), 29 dBm saturated output power (0.5 W) distributed power amplifier that operates from 20 GHz to 54 GHz. The amplifier provides a gain of 19.5 dB, an output power for 1 dB compression (P1dB) of 28.5 dBm, and a typical output third-order intercept (IP3) of

#### **FUNCTIONAL BLOCK DIAGRAM**

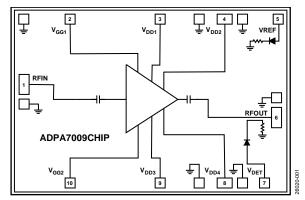


Figure 1.

35 dBm at 24 GHz to 36 GHz. The ADPA7009CHIP requires 750 mA from a 5 V supply voltage ( $V_{\rm DD}$ ) and features inputs and outputs that are internally matched to 50  $\Omega$ , facilitating integration into multichip modules (MCMs). All data is taken with the RFIN and RFOUT pads connected via one 0.076 mm (3 mil) ribbon bond of 0.076 mm (3 mil) minimal length.

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#### **REVISION HISTORY**

3/2021—Revision 0: Initial Version

## **SPECIFICATIONS**

#### **20 GHz TO 24 GHz FREQUENCY RANGE**

 $T_A = 25$ °C, supply voltage ( $V_{DD}$ ) = 5 V,  $I_{DQ}$  = 750 mA, and 50  $\Omega$  matched input and output, unless otherwise noted. Adjust the gate voltage ( $V_{GGx}$ ) from -1.5 V to 0 V to achieve  $I_{DQ}$  = 750 mA typical.

Table 1.

Parameter	Symbol	Min	Тур	Max	Unit	Test Conditions/Comments
FREQUENCY RANGE		20		24	GHz	
GAIN		14.5	17		dB	
Gain Flatness			±1.2		dB	
Gain Variation Over Temperature			0.033		dB/°C	
NOISE FIGURE			6.5		dB	
RETURN LOSS						
Input			15.0		dB	
Output			20.0		dB	
OUTPUT						
Output Power for 1 dB Compression	P1dB	25	27.5		dBm	
Saturated Output Power	P <sub>SAT</sub>		28.5		dBm	
Output Third-Order Intercept	IP3		32		dBm	Output power ( $P_{OUT}$ ) per tone = 14 dBm with 1 MHz tone spacing
SUPPLY						
Quiescent Current	$I_{DQ}$		750		mA	Adjust V <sub>GGx</sub> to achieve I <sub>DQ</sub> = 750 mA typical
Voltage	$V_{DD}$	3	5		V	

#### 24 GHz TO 36 GHz FREQUENCY RANGE

 $T_A$  = 25°C,  $V_{DD}$  = 5 V,  $I_{DQ}$  = 750 mA, and 50  $\Omega$  matched input and output, unless otherwise noted. Adjust  $V_{GGx}$  from -1.5 V to 0 V to achieve  $I_{DQ}$  = 750 mA typical.

Table 2.

Parameter	Symbol	Min	Тур	Max	Unit	Test Conditions/Comments
FREQUENCY RANGE		24		36	GHz	
GAIN		17.0	19.5		dB	
Gain Flatness			±1.1		dB	
Gain Variation Over Temperature			0.023		dB/°C	
NOISE FIGURE			5.5		dB	
RETURN LOSS						
Input			17.5		dB	
Output			22.0		dB	
OUTPUT						
Output Power for 1 dB Compression	P1dB	26	28.5		dBm	
Saturated Output Power	P <sub>SAT</sub>		29		dBm	
Output Third-Order Intercept	IP3		35		dBm	P <sub>OUT</sub> per tone = 14 dBm with 1 MHz tone spacing
SUPPLY			•	•		
Quiescent Current	$I_{DQ}$		750		mA	Adjust $V_{GGx}$ to achieve $I_{DQ} = 750$ mA typical
Voltage	$V_{DD}$	3	5		V	

#### **36 GHz TO 50 GHz FREQUENCY RANGE**

 $T_A$  = 25°C,  $V_{DD}$  = 5 V,  $I_{DQ}$  = 750 mA, and 50  $\Omega$  matched input and output, unless otherwise noted. Adjust  $V_{GGx}$  from -1.5 V to 0 V to achieve  $I_{DQ}$  = 750 mA typical.

Table 3.

Parameter	Symbol	Min	Тур	Max	Unit	Test Conditions/Comments
FREQUENCY RANGE		36		50	GHz	
GAIN		17.5	20.0		dB	
Gain Flatness			±1.1		dB	
Gain Variation Over Temperature			0.026		dB/°C	
NOISE FIGURE			6.0		dB	
RETURN LOSS						
Input			20		dB	
Output			20		dB	
OUTPUT						
Output Power for 1 dB Compression	P1dB	22	25		dBm	
Saturated Output Power	P <sub>SAT</sub>		27.0		dBm	
Output Third-Order Intercept	IP3		34.5		dBm	Pout per tone = 14 dBm with 1 MHz tone spacing
SUPPLY						
Quiescent Current	$I_{DQ}$		750		mA	Adjust $V_{GGx}$ to achieve $I_{DQ} = 750$ mA typical
Voltage	$V_{\text{DD}}$	3	5		V	

#### **50 GHz TO 54 GHz FREQUENCY RANGE**

 $T_A$  = 25°C,  $V_{DD}$  = 5 V,  $I_{DQ}$  = 750 mA, and 50  $\Omega$  matched input and output, unless otherwise noted. Adjust  $V_{GGx}$  from -1.5 V to 0 V to achieve  $I_{DQ}$  = 750 mA typical.

Table 4.

Parameter	Symbol	Min	Тур	Max	Unit	Test Conditions/Comments
FREQUENCY RANGE		50		54	GHz	
GAIN			20.5		dB	
Gain Flatness			±0.85		dB	
Gain Variation Over Temperature			0.027		dB/°C	
NOISE FIGURE			6.0		dB	
RETURN LOSS						
Input			16.5		dB	
Output			20.0		dB	
OUTPUT						
Output Power for 1 dB Compression	P1dB		24.0		dBm	
Saturated Output Power	P <sub>SAT</sub>		26.0		dBm	
Output Third-Order Intercept	IP3		33		dBm	P <sub>OUT</sub> per tone = 14 dBm with 1 MHz tone spacing
SUPPLY						
Quiescent Current	$I_{DQ}$		750		mA	Adjust $V_{GGx}$ to achieve $I_{DQ} = 750$ mA typical
Voltage	$V_{DD}$	3	5		V	

## **ABSOLUTE MAXIMUM RATINGS**

#### Table 5.

Parameter	Rating
Drain Bias Voltage (V <sub>DDx</sub> )	6.0 V
$V_{GGx}$	-1.6 V to 0 V
RF Input Power (RFIN)	20 dBm
Continuous Power Dissipation ( $P_{DISS}$ ), T <sub>A</sub> = 85°C (Derate 85 mW/°C Above 85°C)	7.7 W
Junction Temperature to Maintain 1,000,000 Hour Mean Time to Failure (MTTF)	175°C
Nominal Junction Temperature ( $T_J = 85$ °C, $V_{DD} = 5 \text{ V}$ , $I_{DQ} = 750 \text{ mA}$ )	129°C
Temperature Range	
Storage	−65°C to +150°C
Operating	−55°C to +85°C

Stresses at or above those listed under Absolute Maximum Ratings may cause permanent damage to the product. This is a stress rating only; functional operation of the product at these or any other conditions above those indicated in the operational section of this specification is not implied. Operation beyond the maximum operating conditions for extended periods may affect product reliability.

#### THERMAL RESISTANCE

Thermal performance is directly linked to the carrier or substrate on which the die is mounted. Careful attention is needed with each material used in the thermal path below the IC.

 $\theta_{\text{JC}}$  is the channel to case thermal resistance, channel to bottom of die using die attach epoxy.

**Table 6. Thermal Resistance** 

Package Type	<b>Ө</b> лс	Unit
C-10-13	11.7	°C/W

#### **ELECTROSTATIC DISCHARGE (ESD) RATINGS**

The following ESD information is provided for handling of ESD sensitive devices in an ESD protected area only.

Human body model (HBM) per ANSI/ESDA/JEDEC JS-001.

#### **ESD Ratings for ADPA7009CHIP**

Table 7. ADPA7009CHIP, 10-Pad Die

ESD Model	Withstand Threshold (V)	Class
HBM	±500	1B

#### **ESD CAUTION**



**ESD** (electrostatic discharge) sensitive device. Charged devices and circuit boards can discharge without detection. Although this product features patented or proprietary protection circuitry, damage may occur on devices subjected to high energy ESD. Therefore, proper ESD precautions should be taken to avoid performance degradation or loss of functionality.

# PIN CONFIGURATION AND FUNCTION DESCRIPTIONS

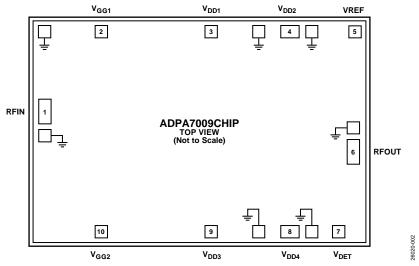


Figure 2. Pin Configuration

**Table 8. Pin Function Descriptions** 

Pin No.	Mnemonic	Description
1	RFIN	RF Signal Input. This pad is ac-coupled and matched to 50 $\Omega$ . See Figure 6 for the interface schematic.
2, 10	V <sub>GG1</sub> , V <sub>GG2</sub>	Amplifier Gate Controls. External bypass capacitors of 4.7 $\mu$ F, 0.01 $\mu$ F, and 100 pF are required for these pads. Adjust V <sub>GGx</sub> from $-1.5$ V to 0 V to achieve the desired quiescent current. See Figure 7 for the interface schematic.
3, 4, 8, 9	V <sub>DD1</sub> , V <sub>DD2</sub> , V <sub>DD4</sub> , V <sub>DD3</sub>	Drain Biases for the Amplifier. External bypass capacitors of 4.7 $\mu$ F, 0.01 $\mu$ F, and 100 pF are required for these pads. See Figure 9 for the interface schematic.
5	VREF	Reference Diode Voltage. Use this pad for temperature compensation of the VDET RF output power measurements. Used in combination with VDET, this voltage provides temperature compensation to the VDET RF output power measurements. See Figure 4 for the interface schematic.
6	RFOUT	RF Signal Output. This pad is ac-coupled and matched to 50 $\Omega$ . See Figure 8 for the interface schematic.
7	VDET	Detector Diode Used for Measuring the RF Output Power. Detection via this pad requires the application of a dc bias voltage through an external series resistor. Used in combination with VREF, the difference detector voltage, VREF – VDET, is a temperature compensated dc voltage proportional to the RF output power. See Figure 5 for the interface schematic.
Die Bottom	GND	Ground. The die bottom must be connected to RF and dc ground. See Figure 3 for the interface schematic.

#### **INTERFACE SCHEMATICS**



Figure 3. GND Interface Schematic

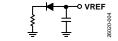


Figure 4. VREF Interface Schematic



Figure 5. VDET Interface Schematic



Figure 6. RFIN Interface Schematic

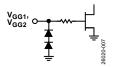


Figure 7.  $V_{GG1}$ ,  $V_{GG2}$  Interface Schematic



Figure 8. RFOUT Interface Schematic



Figure 9. V<sub>DD1</sub> to V<sub>DD4</sub> Interface Schematic

## TYPICAL PERFORMANCE CHARACTERISTICS

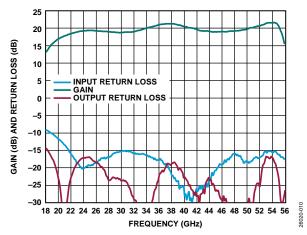


Figure 10. Gain and Return Loss vs. Frequency,  $V_{DD} = 5 V$ ,  $I_{DQ} = 750 \text{ mA}$ 

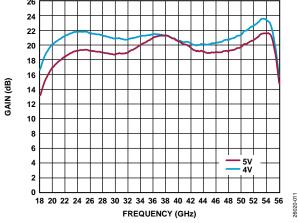


Figure 11. Gain vs. Frequency for Various Supply Voltages,  $I_{DQ} = 750 \text{ mA}$ 

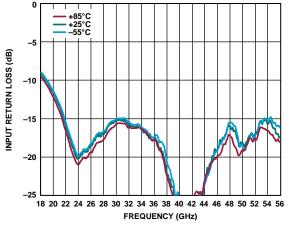


Figure 12. Input Return Loss vs. Frequency for Various Temperatures,  $V_{DD} = 5 V$ ,  $I_{DQ} = 750 \text{ mA}$ 

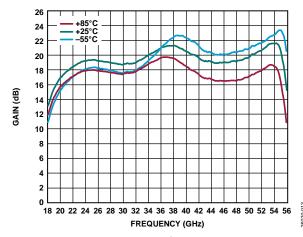


Figure 13. Gain vs. Frequency for Various Temperatures,  $V_{DD} = 5 V$ ,  $I_{DQ} = 750 \text{ mA}$ 

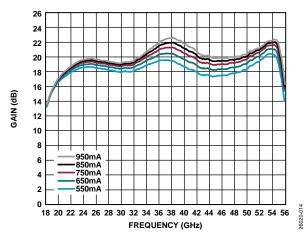


Figure 14. Gain vs. Frequency for Various  $I_{DQ}$  Currents,  $V_{DD} = 5 V$ 

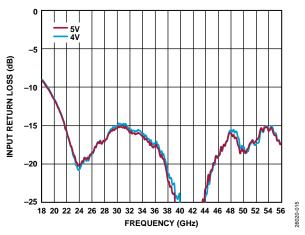


Figure 15. Input Return Loss vs. Frequency for Various Supply Voltages,  $I_{DQ} = 750 \text{ mA}$ 

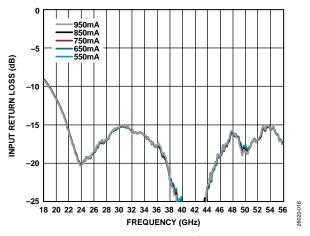


Figure 16. Input Return Loss vs. Frequency for Various  $I_{DQ}$  Currents,  $V_{DD} = 5 \text{ V}$ 

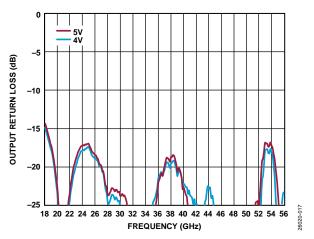


Figure 17. Output Return Loss vs. Frequency for Various Supply Voltages,  $I_{DQ} = 750 \text{ mA}$ 

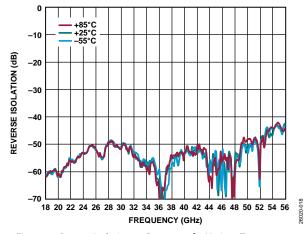


Figure 18. Reverse Isolation vs. Frequency for Various Temperatures,  $V_{DD} = 5 V$ ,  $I_{DQ} = 750 \text{ mA}$ 

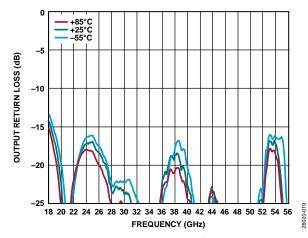


Figure 19. Output Return Loss vs. Frequency for Various Temperatures,  $V_{DD} = 5 \text{ V}$ ,  $I_{DQ} = 750 \text{ mA}$ 

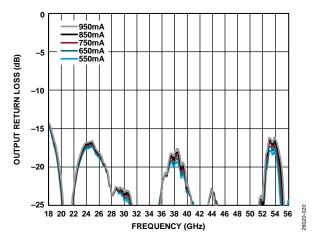


Figure 20. Output Return Loss vs. Frequency for Various  $I_{DQ}$  Currents,  $V_{DD}$  = 5 V

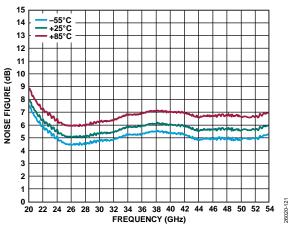


Figure 21. Noise Figure vs. Frequency for Various Temperatures,  $V_{DD} = 5 V$ ,

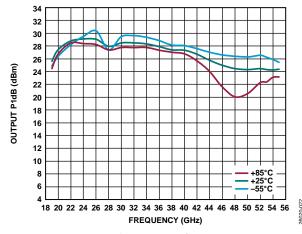


Figure 22. Output P1dB vs. Frequency for Various Temperatures,  $V_{DD} = 5 V$ ,  $I_{DQ} = 750 \text{ mA}$ 

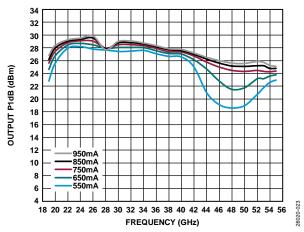


Figure 23. Output P1dB vs. Frequency for Various  $I_{DQ}$  Currents,  $V_{DD} = 5 V$ 

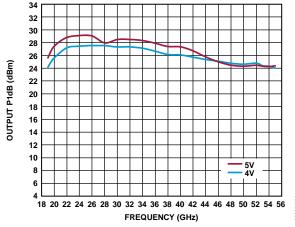


Figure 24. Output P1dB vs. Frequency for Various Supply Voltages,  $I_{DQ} = 750 \, \text{mA}$ 

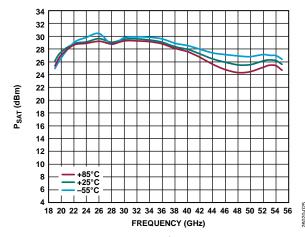


Figure 25.  $P_{SAT}$  vs. Frequency for Various Temperatures,  $V_{DD} = 5 \text{ V}$ ,  $I_{DQ} = 750 \text{ mA}$ 

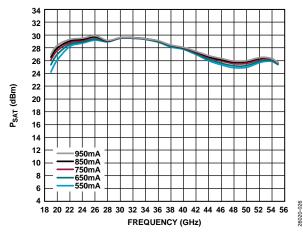


Figure 26.  $P_{SAT}$  vs. Frequency for Various  $I_{DQ}$  Currents,  $V_{DD} = 5 V$ 

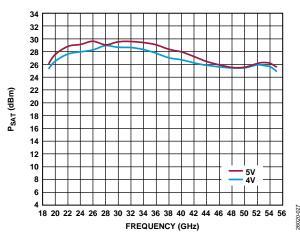


Figure 27.  $P_{SAT}$  vs. Frequency for Various Voltages,  $I_{DQ} = 750 \text{ mA}$ 

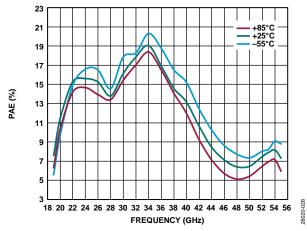


Figure 28. Power Added Efficiency (PAE) vs. Frequency for Various Temperatures,  $V_{DD}$  = 5 V,  $I_{DQ}$  = 750 mA, PAE at  $P_{SAT}$  (dBm)

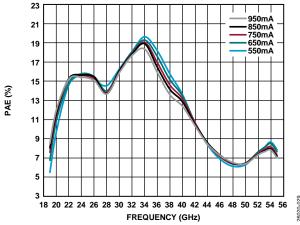


Figure 29. PAE vs. Frequency for Various  $I_{DQ}$  Currents,  $V_{DD} = 5 V$ , PAE at  $P_{SAT}$  (dBm)

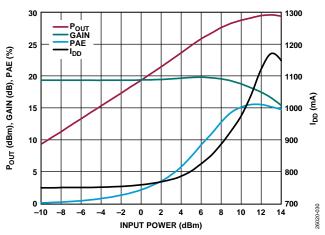


Figure 30.  $P_{OUT}$ , Gain, PAE, and Drain Current with RF Applied ( $I_{DD}$ ) vs. Input Power, 26 GHz,  $V_{DD}=5$  V,  $I_{DQ}=750$  mA

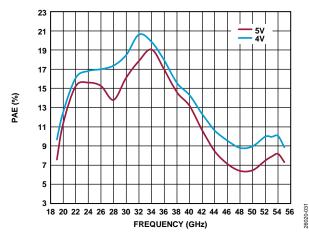


Figure 31. PAE vs. Frequency for Various Supply Voltages,  $I_{DQ} = 750$  mA, PAE at  $P_{SAT}(dBm)$ 

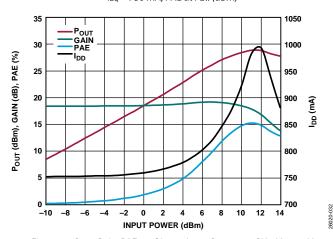


Figure 32. Pout, Gain, PAE, and  $I_{DD}$  vs. Input Power, 22 GHz,  $V_{DD}$  = 5 V,  $I_{DQ}$  = 750 mA

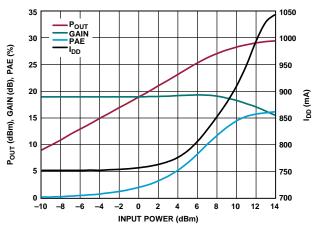


Figure 33.  $P_{OUT}$ , Gain, PAE, and  $I_{DD}$  vs. Input Power, 30 GHz,  $V_{DD} = 5 V$ ,  $I_{DQ} = 750 \text{ mA}$ 

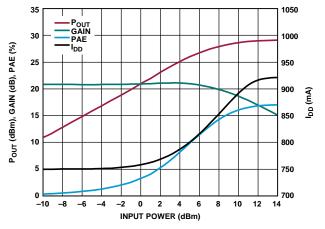


Figure 34.  $P_{OUT}$ , Gain, PAE, and  $I_{DD}$  vs. Input Power, 36 GHz,  $V_{DD}$  = 5 V,  $I_{DO}$  = 750 mA

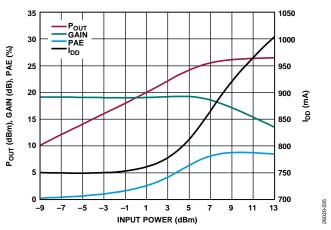


Figure 35. Pout, Gain, PAE, and  $I_{DD}$  vs. Input Power, 44 GHz,  $V_{DD}$  = 5 V,  $I_{DQ}$  = 750 mA

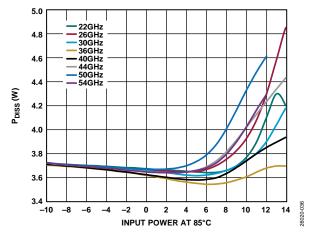


Figure 36.  $P_{DISS}$  vs. Input Power for Various Frequencies at  $T_A = 85$ °C,  $V_{DD} = 5$  V,  $I_{DQ} = 750$  mA

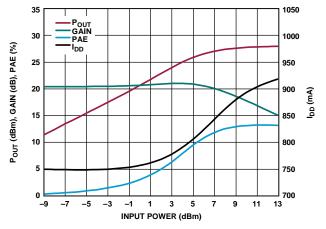


Figure 37.  $P_{OUT}$ , Gain, PAE, and  $I_{DD}$  vs. Input Power, 40 GHz,  $V_{DD}$  = 5 V,  $I_{DQ}$  = 750 mA

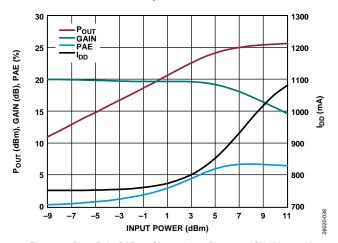


Figure 38. Pout, Gain, PAE, and  $I_{DD}$  vs. Input Power, 50 GHz,  $V_{DD}$  = 5 V,  $I_{DQ}$  = 750 mA

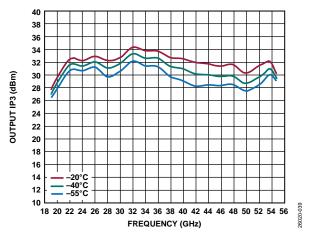


Figure 39. Output IP3 vs. Frequency at  $-20^{\circ}$ C,  $-40^{\circ}$ C, and  $-55^{\circ}$ C,  $P_{OUT}$  per Tone = 14 dBm,  $V_{DD}$  = 5 V,  $I_{DQ}$  = 750 mA

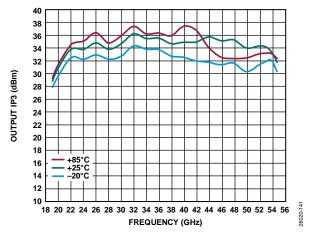


Figure 40. Output IP3 vs. Frequency at  $+25^{\circ}$ C,  $+85^{\circ}$ C and  $-20^{\circ}$ C,  $P_{OUT}$  per Tone = 14 dBm,  $V_{DD}$  = 5 V,  $I_{DQ}$  = 750 mA

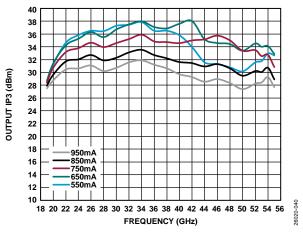


Figure 41. Output IP3 vs. Frequency for Various  $I_{DQ}$  Currents,  $P_{OUT}$  per Tone = 14 dBm,  $V_{DD}$  = 5 V

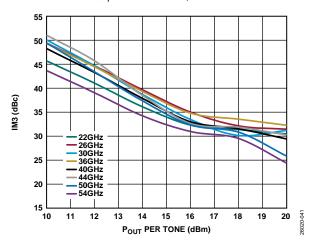


Figure 42. Third-Order Intermodulation Distortion (IM3) vs.  $P_{OUT}$  per Tone,  $V_{DD}=4\,V$ ,  $I_{DQ}=750\,mA$ 

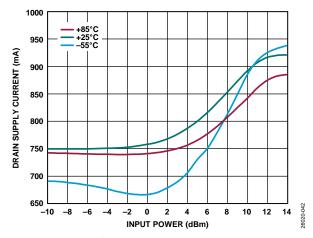


Figure 43. Drain Supply Current vs. Input Power at Various Frequencies,  $V_{DD} = 5 \text{ V}$ ,  $I_{DQ} = 750 \text{ mA}$ 

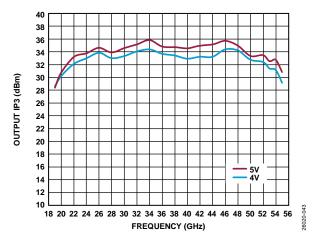


Figure 44. Output IP3 vs. Frequency for Various Supply Voltages,  $P_{OUT}$  per Tone = 14 dBm,  $I_{DQ}$  = 750 mA

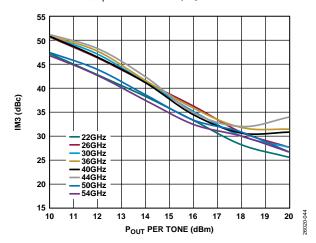


Figure 45. IM3 vs.  $P_{OUT}$  per Tone,  $V_{DD} = 5 V$ ,  $I_{DQ} = 750 \text{ mA}$ 

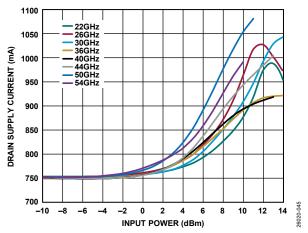


Figure 46. Drain Supply Current vs. Input Power at Various Temperature, 36 GHz,  $V_{DD}$  = 5 V,  $I_{DQ}$  = 750 mA

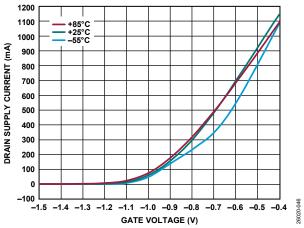


Figure 47. Drain Supply Current vs. Gate Voltage at Various Temperature

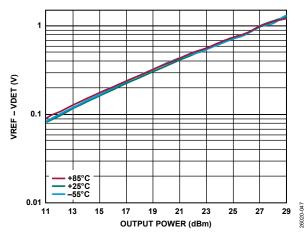


Figure 48. Detector Voltage (VREF – VDET) vs. Output Power for Various Temperatures at 36 GHz

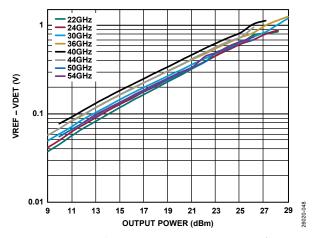


Figure 49. Detector Voltage (VREF – VDET) vs. Output Power for Various Frequencies

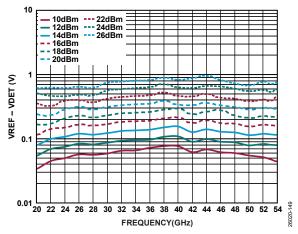


Figure 50. Detector Voltage (VREF – VDET) vs. Frequency for Various Output Powers

#### **LOWER BIAS OPERATION**

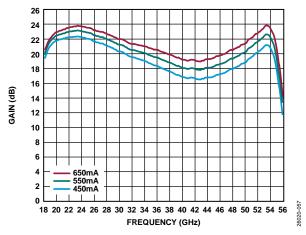


Figure 51. Gain vs. Frequency for Various  $I_{DQ}$  Currents,  $V_{DD} = 3 V$ 

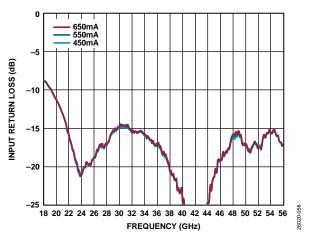


Figure 52. Input Return Loss vs. Frequency for Various  $I_{DQ}$  Currents,  $V_{DD} = 3 \text{ V}$ 

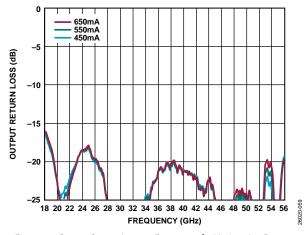


Figure 53. Output Return Loss vs. Frequency for Various  $I_{DQ}$  Currents,  $V_{DD}$  = 3 V

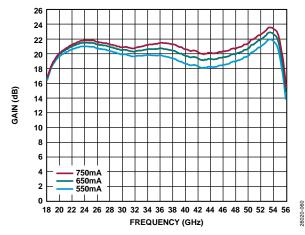


Figure 54. Gain vs. Frequency for Various  $I_{DQ}$  Currents,  $V_{DD} = 4 V$ 

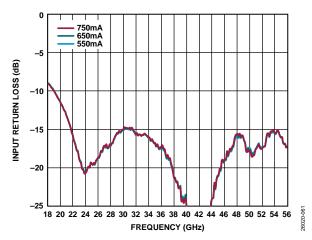


Figure 55. Input Return Loss vs. Frequency for Various  $I_{DQ}$  Currents,  $V_{DD} = 4 V$ 

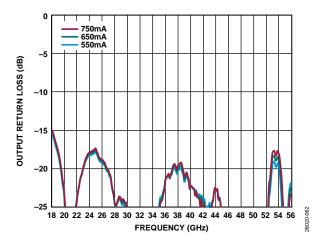


Figure 56. Output Return Loss vs. Frequency for Various  $I_{DQ}$  Currents,  $V_{DD} = 4 V$ 

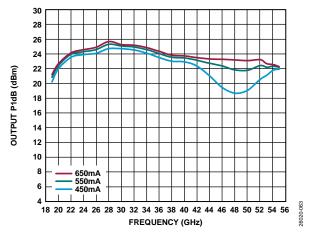


Figure 57. Output P1dB vs. Frequency for Various  $I_{DQ}$  Currents,  $V_{DD} = 3 V$ 

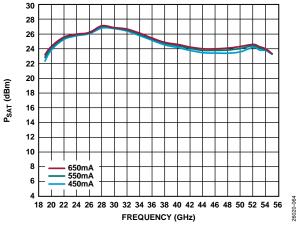


Figure 58.  $P_{SAT}$  vs. Frequency for Various  $I_{DQ}$  Currents,  $V_{DD} = 3 V$ 

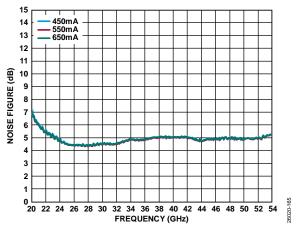


Figure 59. Noise Figure vs. Frequency for Various  $I_{DQ}$  Currents,

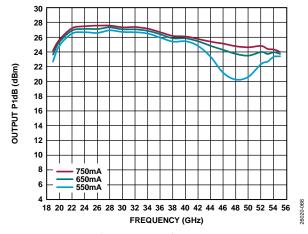


Figure 60. Output P1dB vs. Frequency for Various  $I_{DQ}$  Currents,  $V_{DD} = 4 V$ 

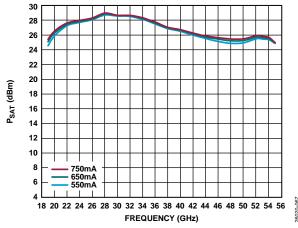


Figure 61.  $P_{SAT}$  vs. Frequency for Various  $I_{DQ}$  Currents,  $V_{DD} = 4 V$ 

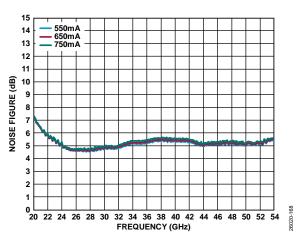


Figure 62. Noise Figure vs. Frequency for Various  $I_{DQ}$  Currents,

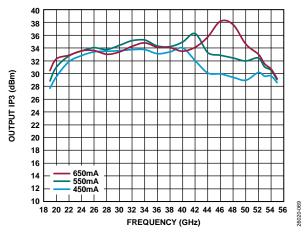


Figure 63. Output IP3 vs. Frequency for Various  $I_{DQ}$  Currents,  $P_{OUT}$  per Tone = 14 dBm,  $V_{DD}$  = 3 V

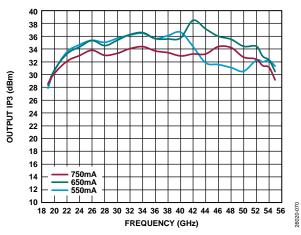


Figure 64. Output IP3 vs. Frequency for Various  $I_{DQ}$  Currents,  $P_{OUT}$  per Tone = 14 dBm,  $V_{DD}$  = 4 V

## THEORY OF OPERATION

The architecture of the ADPA7009CHIP, a medium power amplifier, is shown in Figure 65. The ADPA7009CHIP uses a cascaded, four-stage amplifier operating in quadrature between two 90° hybrids.

The input signal is divided evenly in two. Each path is amplified through four independent gain stages. The amplified signals are then combined at the output. This balanced amplifier approach forms an amplifier with a combined gain of 19.5 dB and a  $P_{SAT}$  value of 29 dBm. The gate pins are internally connected and can be biased from either north or south of the circuit.

A portion of the RF output signal is directionally coupled to a diode for detection of the RF output power. When the diode is dc biased, the diode rectifies the RF power and makes the RF power available for measurement as a dc voltage at VDET. To allow temperature compensation of VDET, an identical and symmetrically located circuit, minus the coupled RF power, is available via VREF. Taking the difference of VREF – VDET provides a temperature compensated signal that is proportional to the RF output (see Figure 65).

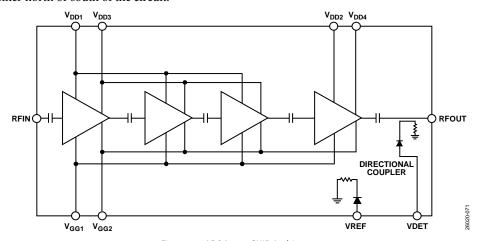


Figure 65. ADPA7009CHIP Architecture

### APPLICATIONS INFORMATION

The ADPA7009CHIP is a GaAs, pHEMT, MMIC power amplifier. Capacitive bypassing is required for all primary and alternate  $V_{\rm GGx}$  and  $V_{\rm DDx}$  pads.  $V_{\rm GG1}$  and  $V_{\rm GG2}$  are the gate bias pads for the amplifier.  $V_{\rm DD1}$ ,  $V_{\rm DD2}$ ,  $V_{\rm DD3}$ , and  $V_{\rm DD4}$  are the drain bias pads for the amplifier.

All measurements for this device were taken using the primary application circuit (see Figure 66) and were configured as shown in the assembly diagram (see Figure 79).

The recommended bias sequence during power-up is as follows:

- 1. Connect GND to RF and dc ground.
- 2. Set the gate bias voltages,  $V_{GG1}$  and  $V_{GG2}$ , to -1.5 V.
- 3. Set all the drain bias voltages,  $V_{\rm DDx}$ , to 5 V.
- 4. Increase the gate bias voltages,  $V_{\rm GG1}$  and  $V_{\rm GG2}$ , to achieve an  $I_{\rm DQ}$  of 750 mA.
- 5. Apply the RF signal.

The recommended bias sequence during power-down is as follows:

- 1. Turn off the RF signal.
- 2. Decrease the primary gate bias voltages,  $V_{\rm GG1}$  and  $V_{\rm GG2}$ , to  $-1.5~\rm V$  to achieve  $I_{\rm DQ}=0~\rm mA$  (approximately).
- 3. Decrease all the drain bias voltages to 0 V.
- 4. Increase the gate bias voltage to 0 V.

The  $V_{\rm DD}=5~{\rm V}$  and  $I_{\rm DQ}=750~{\rm mA}$  bias conditions are recommended to optimize overall performance. Unless otherwise noted, the data shown was taken using the recommended bias conditions. Operation of the ADPA7009CHIP at different bias conditions may provide performance that differs from what is shown in Table 1 to Table 4. Biasing the ADPA7009CHIP for higher drain current typically results in higher P1dB and gain at the expense of increased power consumption (see Table 9).

#### **TYPICAL APPLICATION CIRCUIT**

Figure 66 shows the primary application circuit. Figure 67 shows the alternate typical application circuit.

Table 9. Power Selection Table 1, 2

I <sub>DQ</sub> (mA)	Gain (dB)	P1dB (dBm)	Output IP3 (dBm)	P <sub>DISS</sub> (W) at P <sub>SAT</sub>	V <sub>GGx</sub> (V)
650	20.33	27.57	37.07	3.25	-0.68
750	21.02	27.93	34.83	3.75	-0.63
850	21.52	28.17	32.69	4.25	-0.59
950	22.02	28.34	31.19	4.75	-0.54

 $<sup>^{1}</sup>$  Data taken at the following nominal bias conditions:  $V_{DD} = 5$  V,  $T_{A} = 25$ °C, and frequency = 36 GHz.

<sup>&</sup>lt;sup>2</sup> Adjust V<sub>GGx</sub> from –1.5 V to 0 V to achieve the desired drain current.

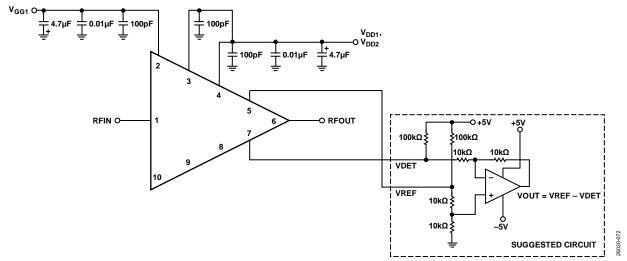


Figure 66. Primary Application Circuit

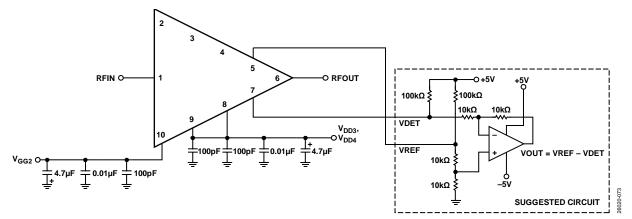


Figure 67. Alternate Application Circuit

## BIASING THE ADPA7009CHIP WITH THE HMC980LP4E

The HMC980LP4E is an active bias controller that is designed to meet the bias requirements for enhancement mode and depletion mode amplifiers such as the ADPA7009CHIP. The controller provides constant drain current biasing over temperature and device to device variation, and properly sequences gate and drain voltages to ensure the safe operation of the amplifier. The HMC980LP4E also offers self-protection in the event of a short circuit, an internal charge pump that generates the negative voltage needed on the gate of the ADPA7008CHIP, and the option to use an external negative voltage source. The HMC980LP4E is also available in die form as the HMC980-Die.

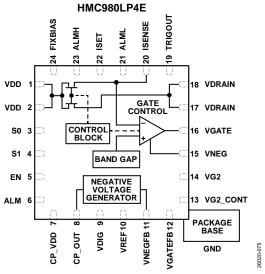


Figure 68. HMC980LP4E Active Bias Control

#### **APPLICATION CIRCUIT SETUP**

Figure 69 shows an application circuit using the HMC980LP4E to control the ADPA7009CHIP. When using an external negative supply for VNEG, refer to the application circuit shown in Figure 70.

In the application circuit shown in Figure 69, the ADPA7009CHIP drain voltage,  $V_{DRAIN}$ , and drain current,  $I_{DRAIN}$ , are set by the following equations:

$$V_{DD} = V_{DRAIN} + (I_{DRAIN} \times 0.85 \Omega)$$
 (1)  
 $V_{DD} = 5 \text{ V} + (0.85 \text{ A} \times 0.85 \Omega) = 5.72 \text{ V}$ 

where:

 $V_{DD}$  and  $V_{DRAIN}$  are in volts.

 $I_{DRAIN}$  is in amperes.

$$R10 = (150 \ \Omega \times A) \div (I_{DRAIN})$$
 (2)  
 $R10 = (150 \ \Omega \times A) \div (0.85 \ A) = 176 \ \Omega$ 

where:

R10 is in ohms.

 $I_{DRAIN}$  is in amperes.

# LIMITING VGATE FOR THE ADPA7009CHIP $V_{\text{GGx}}$ ABSOLUTE MAXIMUM RATING REQUIREMENT

When using the HMC980LP4E to control the ADPA7009CHIP, the minimum voltages for VNEG and VGATE must be  $-1.5~\rm V$  to keep the voltages within the absolute maximum rating limit for the  $V_{\rm GGx}$  pad of the ADPA7009CHIP. To set the minimum voltages, set R15 and R16 to the values shown in Figure 69 and Figure 70. Refer to the AN-1363 Application Note for more information and calculations for R15 and R16.

The HMC980LP4E application circuits for biasing figures in the AN-1363 are two examples of how the HMC980LP4E is used as an active bias controller. Both application circuits within the AN-1363 show the R5 and R7 resistors, which are analogous to the R15 and R16 resistor shown in Figure 69 and Figure 70.

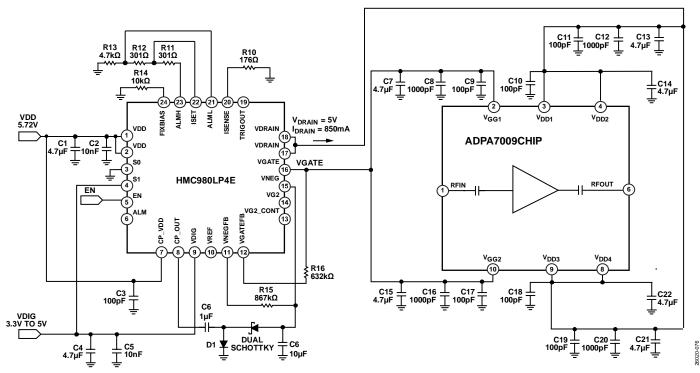


Figure 69. Application Circuit Using the HMC980LP4E with the ADPA7009CHIP (Internal Negative Voltage Source)

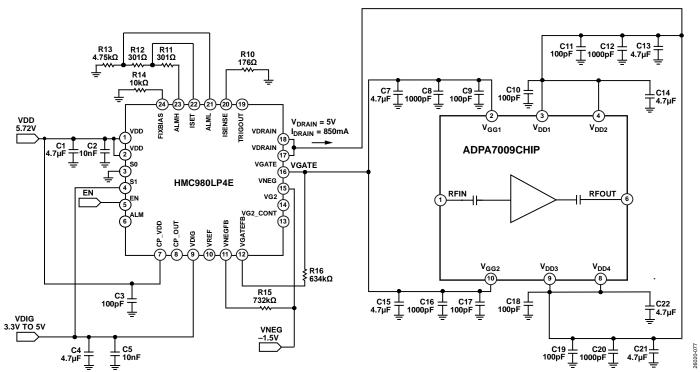


Figure 70. Application Circuit Using the HMC980LP4E with the ADPA7009CHIP (External Negative Voltage Source)

#### **HMC980LP4E BIAS SEQUENCE**

The dc supply sequence described in this section is required to prevent damage to the HMC980LP4E when using the device to control the ADPA7009CHIP.

#### Power-Up Sequence

The power-up sequence for the HMC980LP4E is as follows:

- Set VDIG = 3.3 V.
- 2. Set S0 = 3.3 V.
- 3. Set VDD = 5.72 V.
- 4. Set VNEG = -1.5 V (this step is unnecessary if using an internally generated voltage).
- 5. Set EN = 3.3 V (the transition from 0 V to 3.3 V turns on VGATE and VDRAIN).

#### **Power-Down Sequence**

The power-down sequence for the HMC980LP4E is as follows:

- 1. Set EN = 0 V (the transition from 3.3 V to 0 V turns off  $V_{DRAIN}$  and  $V_{GATE}$ ).
- 2. Set VNEG = 0 V (this step is unnecessary if using and internally generated voltage).
- 3. Set VDD = 0 V.
- 4. Set S0 = 0 V.
- 5. Set VDIG = 0 V.

After the HMC980LP4E bias control circuit is set up, toggle the bias to the ADPA7009CHIP on or off by applying 3.3 V or 0 V, respectively, to the EN pad. At EN = +3.3 V,  $V_{\rm GATE}$  drops to -1.5 V, and  $V_{\rm DRAIN}$  turns on at +5 V. VGATE then rises until  $I_{\rm DRAIN}$  = 850 mA, and the closed control loop regulates  $I_{\rm DRAIN}$  at 850 mA. When EN = 0 V, VDRAIN is set to -1.5 V, and VDRAIN is set to 0 V.

# CONSTANT DRAIN CURRENT BIASING vs. CONSTANT GATE VOLTAGE BIASING

The HMC980LP4E uses closed-loop feedback to continuously adjust VGATE to maintain a constant drain current bias over dc supply variation, temperature, and device to device variation. In addition, constant drain current bias is the optimum method for reducing time in calibration procedures and for maintaining consistent performance over time. By comparing the constant drain current bias with a constant gate voltage bias where the current is driven to increase when RF power is applied, a slightly lower output P1dB is seen with a constant drain current bias. This output P1dB is shown in Figure 78, where the RF performance is slightly lower than the constant gate voltage bias operation due to a lower drain current at the high input powers as the device reaches 1 dB compression.

To increase the output P1dB performance for the constant drain current bias toward the constant gate voltage bias performance, increase the set current toward the  $I_{\rm DD}$  value this performance reaches under the RF drive in the constant gate voltage bias condition, as shown in Figure 78. The limit of increasing  $I_{\rm DQ}$  under the constant drain current operation is set by the thermal limitations found in Table 5 with the maximum power dissipation specification. As the  $I_{\rm DD}$  increase continues, the actual output P1dB does not continue to increase indefinitely and the power dissipation increases. Therefore, when using constant drain current biasing, take the trade-off between the power dissipation and the output P1dB performance into consideration.

#### **CONSTANT IDD OPERATION**

 $T_A = 25$ °C,  $V_{DD} = 5$  V,  $I_{DD} = 850$  mA for nominal operation, unless otherwise noted. Figure 71 to Figure 78 are biased with the HMC980LP4E active bias controller. See the Biasing the ADPA7009CHIP with the HMC980LP4E section for biasing details.

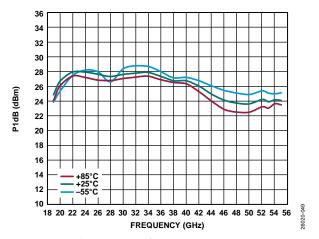


Figure 71. P1dB vs. Frequency for Various Temperatures,  $V_{DD} = 5 V$ ,

Data Measured with Constant  $I_{DD}$ 

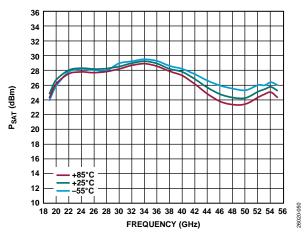


Figure 72.  $P_{SAT}$  vs. Frequency for Various Temperatures,  $V_{DD} = 5 V$ ,

Data Measured with Constant  $I_{DD}$ 

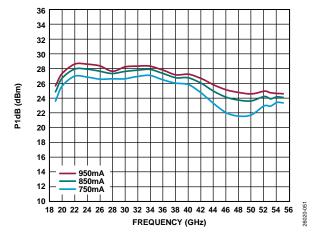


Figure 73. P1dB vs. Frequency for Various Drain Currents,  $V_{DD} = 5 V$ ,

Data Measured with Constant  $I_{DD}$ 

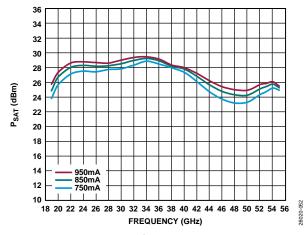


Figure 74.  $P_{SAT}$  vs. Frequency for Various Drain Currents,  $V_{DD} = 5 V$ ,

Data Measured with Constant  $I_{DD}$ 

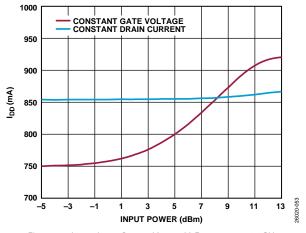


Figure 75.  $I_{DD}$  vs. Input Power,  $V_{DD} = 5$  V, Frequency = 36 GHz, Constant Drain Current Bias ( $I_{DRAIN}$  Setpoint = 850 mA) and Constant Gate Voltage Bias ( $V_{GGx} \approx -0.63$  V)

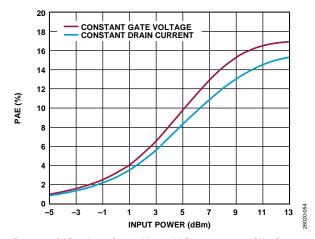


Figure 76. PAE vs. Input Power,  $V_{DD} = 5$  V, Frequency = 36 GHz, Constant Drain Current Bias ( $I_{DRAIN}$  Setpoint = 850 mA) and Constant Gate Voltage Bias ( $V_{GGx} \approx -0.63$  V)

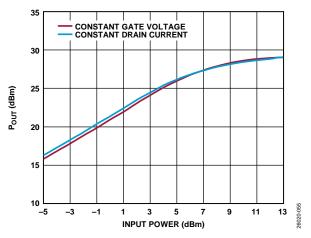


Figure 77.  $P_{OUT}$  vs. Input Power,  $V_{DD} = 5$  V, Frequency = 36 GHz, Constant Drain Current Bias ( $I_{DRAIN}$  Setpoint = 850 mA) and Constant Gate Voltage Bias ( $V_{GGx} \approx -0.63$  V)

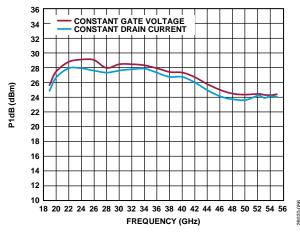


Figure 78. P1dB vs. Frequency,  $V_{DD} = 5 V$ , Constant Drain Current Bias ( $I_{DRAIN}$  Setpoint = 850 mA) and Constant Gate Voltage Bias ( $V_{GGx} \approx -0.63 V$ )

## **ASSEMBLY DIAGRAM**

Figure 79 shows the assembly diagram for the ADPA7009CHIP.

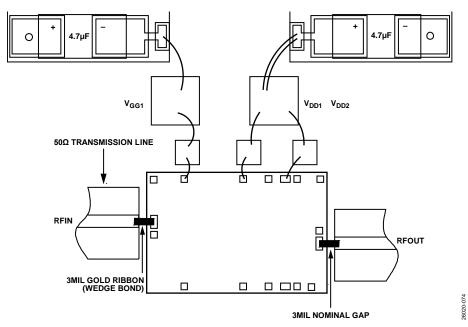


Figure 79. Assembly Diagram with Bias Control on North Side of Die

# MOUNTING AND BONDING TECHNIQUES FOR MILLIMETERWAVE GAAS MMICS

Attach the die directly to the ground plane with conductive epoxy (see the Handling Precautions section, the Mounting section, and the Wire Bonding section).

Place the microstrip substrates as close to the die as possible to minimize ribbon bond length. Typical die to substrate spacing is 0.076 mm to 0.152 mm (3 mil to 6 mil).

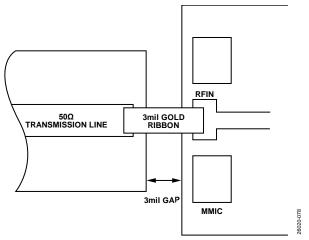


Figure 80. High Frequency Input Wideband Matching

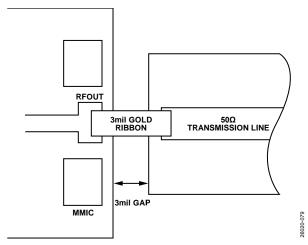


Figure 81. High Frequency Output Wideband Matching

# HANDLING PRECAUTIONS

To avoid permanent damage, follow these storage, cleanliness, static sensitivity, transient, and general handling precautions:

- Place all bare die in either waffle- or gel-based ESD protective containers and then seal the die in an ESD protective bag for shipment. After the sealed ESD protective bag is opened, store all die in a dry nitrogen environment.
- Handle the chips in a clean environment. Do not attempt to clean the chips using liquid cleaning systems.
- Follow ESD precautions to protect against ESD strikes.
- While bias is applied, suppress instrument and bias supply transients. Use shielded signal and bias cables to minimize inductive pickup.
- Handle the chip along the edges with a vacuum collet or with a sharp pair of tweezers. The surface of the chip has fragile air bridges and must not be touched with a vacuum collet, tweezers, or fingers.

#### **MOUNTING**

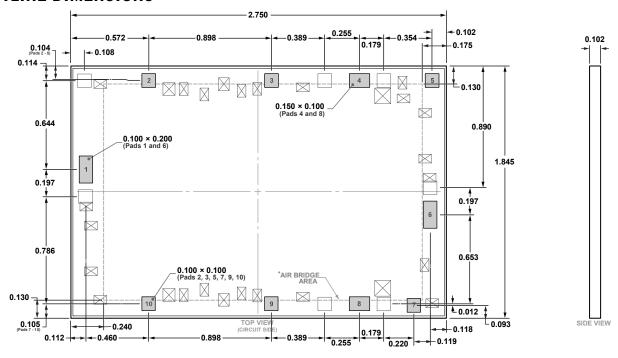
Before the epoxy die is attached, apply a minimum amount of epoxy to the mounting surface so that a thin epoxy fillet is observed around the perimeter of the chip after it is placed into position. Cure the epoxy per the schedule of the manufacturer.

#### **WIRE BONDING**

RF bonds made with 0.076 mm  $\times$  0.0127 mm (3 mil  $\times$  0.5 mil) gold ribbon are recommended for the RF ports. These bonds must be thermosonically bonded with a force of 40 g to 60 g. Thermosonically bonded dc bonds of 0.025 mm (1mil) diameter are recommended. Create ball bonds with a force of 40 g to 50 g, and wedge bonds with a force of 18 g to 22 g. Create all bonds with a nominal stage temperature of 150°C. Apply the minimum amount of ultrasonic energy (depending on the process and package being used) to achieve reliable bonds. Keep all bonds as short as possible, less than 0.31 mm (12.2 mil).

Alternatively, use short RF bonds that are ≤3 mm and made with two 1 mm wires.

## **OUTLINE DIMENSIONS**



\*This die utilizes fragile air bridges. Any pickup tools used must not contact this area.

Figure 82. 10-Pad Bare Die [CHIP] (C-10-13) Dimensions shown in millimeter

#### **ORDERING GUIDE**

Model <sup>1, 2</sup>	<b>Temperature Range</b>	Package Description	Package Option	
ADPA7009CHIP	−55°C to +85°C	10-Pad Bare Die [CHIP]	C-10-13	
ADPA7009C-KIT	-55°C to +85°C	10-Pad Bare Die [CHIP]	C-10-13	

<sup>&</sup>lt;sup>1</sup> The ADPA7009CHIP and ADPA7009C-KIT are RoHS compliant parts.

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<sup>&</sup>lt;sup>2</sup> Die inspected to meet MIL-STD-883 Method 2010, Condition B.