LT1303/LT1303-5

## Micropower High Efficiency DC/DC Converters with Low-Battery Detector Adjustable and Fixed 5V

## feATURES

- 5 V at 200 mA from a 2 V Input
- Supply Voltage As Low As 1.8 V
- Up to 88\% Efficiency
- 120 1 A Quiescent Current
- Low-Battery Detector
- Low V ${ }_{\text {CESAT }}$ Switch: 170 mV at 1A Typ
- Uses Inexpensive Surface Mount Inductors
- 8-Lead PDIP or SO Package


## APPLICATIONS

- EL Panel Drivers
- 2-Cell and 3-Cell to 5 V Conversion
- Palmtop Computers
- Portable Instruments
- Bar-Code Scanners
- PDAs
- Wireless Systems


## DESCRIPTION

The LT ${ }^{\otimes} 1303 / L T 1303-5$ are micropower step-up high efficiency $D C / D C$ converters using Burst Mode ${ }^{\text {TM }}$ operation. They are ideal for use in small, low-voltage batteryoperated systems. The LT1303-5 accepts an input voltage between 1.8 V and 5 V and converts itto a regulated 5 V . The LT1303 is an adjustable version that can supply an output voltage up to 25 V . Quiescent current is only $120 \mu \mathrm{~A}$ from the battery and the shutdown pin further reduces current to $10 \mu \mathrm{~A}$. The low-battery detector provides an opencollector output that goes low when the input voltage drops below a preset level. The on-chip NPN power switch has a low 170 mV saturation voltage at a switch current of 1 A. The LT1303/LT1303-5 are available in 8 -lead PDIP or SO packages, easing board space requirements.
For higher output current, please see the LT1305 or LT1302.
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## TYPICAL APPLICATION



Figure 1. 2-Cell to 5V DC/DC Converter with Low-Battery Detect


## ABSOLUTE MAXIMUM RATINGS


SW1 Voltage ..................................................... 25V
Sense Voltage (LT1303-5) ..................................... 20V
FB Voltage (LT1303) ............................................ 10V
Shutdown Voltage ............................................ 10V
LBO Voltage ..................................................... 10V
LBI Voltage ...................................................... 10V
Maximum Power Dissipation 500 mW
Operating Temperature Range .................... $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$
Storage Temperature Range ................ $-65^{\circ} \mathrm{C}$ to $150^{\circ} \mathrm{C}$ Lead Temperature (Soldering, 10 sec )................. $300^{\circ} \mathrm{C}$

PACKAGE/ORDER INFORMATION

|  | ORDER PART NUMBER |
| :---: | :---: |
| LBO 2 - 7 SW | LT1303CN8 |
| SHDN 3 3 $6 \mathrm{~V}_{\mathrm{IN}}$ | LT1303CS8 |
| FB (SENSE)* 4 5 LBI | LT1303CN8-5 |
|  | LT1303CS8-5 |
| 8-LEAD PDIP |  |
| S8 PACKAGE | S8 PART MARKING |
| *FIXED VERSION | 1303 |
| $\begin{aligned} & \mathrm{T}_{\text {JMAX }}=100^{\circ} \mathrm{C}, \theta_{\mathrm{JA}}=130^{\circ} \mathrm{C} / \mathrm{W}(\mathrm{~N} 8) \\ & \mathrm{T}_{\mathrm{JMAX}}=100^{\circ} \mathrm{C}, \theta_{\mathrm{JA}}=150^{\circ} \mathrm{C} / \mathrm{W}(\mathrm{~S} 8) \end{aligned}$ | 13035 |

Consult factory for Industrial and Military grade parts.

## ELECTRICAL CHARACTERIST|CS $T_{A}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{IN}}=2.0 \mathrm{~V}$, unless otherwise noted.

| SYMBOL | PARAMETER | CONDITIONS |  | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }_{1}$ | Quiescent Current | $\begin{aligned} & V_{\text {SHDN }}=0.5 \mathrm{~V}, \mathrm{~V}_{\text {SEL }}=5 \mathrm{~V}, \mathrm{~V}_{\text {SENSE }}=5.5 \mathrm{~V} \\ & \mathrm{~V}_{\text {SHDN }}=1.8 \mathrm{~V} \end{aligned}$ | $\bullet$ |  | $\begin{gathered} 120 \\ 7 \end{gathered}$ | $\begin{gathered} 200 \\ 15 \end{gathered}$ | $\mu \mathrm{A}$ $\mu \mathrm{A}$ |
| $\overline{\mathrm{V}} \mathrm{IN}$ | Input Voltage Range |  | $\bullet$ | $\begin{aligned} & 1.8 \\ & 2.0 \end{aligned}$ | 1.55 |  | V |
|  | Feedback Voltage | LT1303 | $\bullet$ | 1.22 | 1.24 | 1.26 | V |
|  | Output Sense Voltage | LT1303-5 | $\bullet$ | 4.8 | 5.0 | 5.2 | V |
|  | Comparator Hysteresis | LT1303 (Note 1) | $\bullet$ |  | 6 | 12.5 | mV |
|  | Output Hysteresis | LT1303-5 (Note 1) | $\bullet$ |  | 22 | 50 | mV |
|  | Feedback Pin Bias Current | LT1303, $\mathrm{V}_{\text {FB }}=1 \mathrm{~V}$ | $\bullet$ |  | 7 | 20 | nA |
|  | Oscillator Frequency | Current Limit Not Asserted |  | 120 | 155 | 185 | kHz |
|  | Oscillator TC |  |  |  | 0.2 |  | \%/ ${ }^{\circ} \mathrm{C}$ |
| DC | Maximum Duty Cycle |  | $\bullet$ | 75 | 86 | 95 | \% |
| $\mathrm{t}_{\mathrm{ON}}$ | Switch On Time | Current Limit Not Asserted |  |  | 5.6 |  | $\mu \mathrm{s}$ |
|  | Output Line Regulation | $1.8 \mathrm{~V}<\mathrm{V}_{\text {IN }}<6 \mathrm{~V}$ | $\bullet$ |  | 0.06 | 0.15 | \%/V |
| $\mathrm{V}_{\text {CESAT }}$ | Switch Saturation Voltage | $\mathrm{I}_{\text {SW }}=700 \mathrm{~mA}$ | $\bullet$ |  | 130 | 200 | mV |
|  | Switch Leakage Current | $\mathrm{V}_{\text {SW }}=5 \mathrm{~V}$, Switch Off | $\bullet$ |  | 0.1 | 10 | $\mu \mathrm{A}$ |
|  | Peak Switch Current | $\begin{aligned} & V_{\text {IN }}=2 V \\ & V_{\text {IN }}=5 \mathrm{~V} \end{aligned}$ | $\bullet$ | $\begin{aligned} & 0.75 \\ & 0.65 \end{aligned}$ | $\begin{aligned} & 1.0 \\ & 0.9 \end{aligned}$ | $\begin{aligned} & 1.25 \\ & 1.15 \end{aligned}$ | A |
|  | LBI Trip Voltage |  | $\bullet$ | 1.21 | 1.24 | 1.27 | V |
|  | LBI Input Bias Current | $\mathrm{V}_{\mathrm{LBI}}=1 \mathrm{~V}$ | $\bullet$ |  | 7 | 20 | nA |
|  | LBO Output Low | $\mathrm{I}_{\text {LOAD }}=100 \mu \mathrm{~A}$ | $\bullet$ |  | 0.11 | 0.4 | V |
|  | LBO Leakage Current | $\mathrm{V}_{\mathrm{LBI}}=1.3 \mathrm{~V}, \mathrm{~V}_{\mathrm{LB} 0}=5 \mathrm{~V}$ | $\bullet$ |  | 0.1 | 5 | $\mu \mathrm{A}$ |
| $\mathrm{V}_{\text {SHDNH }}$ | Shutdown Pin High |  | $\bullet$ | 1.8 |  |  | V |
| $V_{\text {SHDNL }}$ | Shutdown Pin Low |  |  |  |  | 0.5 | V |
| ISHDN | Shutdown Pin Bias Current | $\begin{aligned} & V_{\text {SHDN }}=5 \mathrm{~V} \\ & V_{\text {SHDN }}=2 \mathrm{~V} \\ & V_{\text {SHDN }}=0 \mathrm{~V} \\ & \hline \end{aligned}$ | $\stackrel{\bullet}{\bullet}$ |  | $\begin{aligned} & \hline 8.0 \\ & 3.0 \\ & 0.1 \\ & \hline \end{aligned}$ | $20$ <br> 1 | $\mu \mathrm{A}$ $\mu \mathrm{A}$ $\mu \mathrm{A}$ |

The denotes specifications which apply over the $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ operating temperature range.

Note 1: Hysteresis specified is DC. Output ripple may be higher if output capacitance is insufficient or capacitor ESR is excessive.

TYPICAL PERFORMAOCE CHARACTERISTICS


LT1303 601
LT1303 FB Voltage


LT1330 G04


LT1303 G02
LT1303-5 Sense Voltage


LT1303 G05
FB Pin Bias Current


LT1303-5 Sense Pin Resistance to Ground


LT1303 GO3
Low Battery Detect Trip Point


LT1303 G06


## LT1303/LT1303-5

## TYPICAL PERFORMANCE CHARACTERISTICS

Switch On-Time


LT1303 G10
Quiescent Current


Transient Response
Figure 1 Circuit


$$
\begin{aligned}
& V_{I N}=2 \mathrm{~V} \\
& V_{\text {OUT }}=5 \mathrm{~V}
\end{aligned}
$$

Oscillator Frequency


Quiescent Current


LT1303 G14

Shutdown Pin Response

$R_{\text {LOAD }}=100 \Omega$
$V_{\text {IN }}=2 \mathrm{~V}$
$V_{\text {OUT }}=5 \mathrm{~V}$
$C_{\text {OUT }}=100 \mu \mathrm{~F}$

Maximum Duty Cycle


LT1303 G12
Switch Current Limit


Low Battery Detector Transient Response


RPULL-UP $=47 \mathrm{k}$

## PIn functions

GND (Pin 1): Signal Ground. Tie to PGND under the package.
LBO (Pin 2): Open-Collector Output of Low-Battery Comparator. Can sink $100 \mu \mathrm{~A}$. Disabled when device is in shutdown.
SHDN (Pin 3): Shutdown. Pull high to shut down the device. Ground for normal operation.
FB/Sense (Pin 4): On 1303 (adjustable) this pin connects to the main comparator C1 input. On LT1303-5 this pin connects to the resistor string that sets output voltage at 5 V .

LBI (Pin 5): Low-Battery Comparator Input. When voltage on this pin below 1.24 V , LBO is low.
$\mathrm{V}_{\mathrm{IN}}$ (Pin 6): Supply Pin. Must be bypassed with a large value electrolytic to ground. Keep bypass within $0.2^{2}$ of the device.
SW (Pin 7): Switch Pin. Connect inductor and diode here. Keep layout short and direct to minimize radio frequency interference.
PGND (Pin 8): Power ground. Tie to signal ground (pin1) under the package. Bypass capacitor from $\mathrm{V}_{\text {IN }}$ should be tied directly to PGND within 0.2 " of the device.

## BLOCK DIAGRAMS



Figure 2. LT1303 Block Digram

5

## BLOCK DIAGRAMS



Figure 3. LT1303-5 Block Diagram

## OPERATION

Operation of the LT1303 is best understood by referring to the Block Diagram in Figure 2. When C1's negative input, related to the output voltage by the appropriate resistordivider ratio, is higher than the 1.24 V reference voltage, C1's output is low. C2, A3 and the oscillator are turned off, drawing no current. Only the reference and C1 consume current, typically $140 \mu \mathrm{~A}$. When C1's negative input drops below 1.24 V and overcomes C1's 6 mV hysteresis, C1's output goes high, enabling the oscillator, current comparator C2 and driver A3. Quiescent current increases to 2 mA as the device goes into active switching mode. Q1 then turns on in controlled saturation for nominally $6 \mu \mathrm{~s}$ or until current comparator C2 trips, whichever comes first. The switch thenturns offfor approximately $1.5 \mu \mathrm{~s}$, thenturns on again. The LT1303's switching causes current to alternately build up in L1 and dump into output capacitor C 4 via D1, increasing the output voltage. When the output is high enough to cause C1's output to go high, switching action ceases. Capacitor C4 is left to supply current to the load until $V_{\text {OUT }}$ decreases enough to force C1's output high, and the entire cycle repeats. Figure 4 details relevant waveforms. C1's cycling causes low-to-mid-frequency ripple voltage on the output. Ripple can be reduced by making the
output capacitor large. The $100 \mu \mathrm{~F}$ unit specified results in ripple of 50 mV to 100 mV on the 5 V output. A $220 \mu \mathrm{~F}$ capacitor will decrease ripple by approximately $50 \%$.


Figure 4. Burst Mode Operation in Action

If switch current reaches 1A, causing C2 to trip, switch ontime is reduced and off-time increases slightly. This allows continuous operation during bursts. C2 monitors the voltage across $3 \Omega$ resistor R1 which is directly related to the switch current. Q2's collector current is set by the emitter-area ratio to $0.6 \%$ of Q1's collector current. When R1's voltage drop exceeds 18 mV , corresponding to 1 A switch current, C2's output goes high, truncating the ontime portion of the oscillator cycle and increasing off-time

## OPERATION

to about $2 \mu \mathrm{~s}$. Response time of C 2 , which determines minimum on-time, is approximately 300 ns .

## Low Battery Detector

The low battery detector is enabled when SHDN is low and disabled when SHDN is high. The comparator has no

$\mathrm{R} 1=\left(\mathrm{V}_{\text {TRIP }}-1.24 \mathrm{~V}\right)(43.5 \mathrm{k})$ HYSTERESIS $\approx 30 \mathrm{mV}$

Figure 5. R3 Adds Hysteresis to Low-Battery Detector
hysteresis built in, but hysteresis can be added by connecting a high-value resistor from LBI to LBO as shown in Figure 5. The internal reference can be accessed via the comparator as shown in Figure 6.


Figure 6. Accessing Internal Reference

## APPLICATIONS INFORMATION

Inductor Section

Inductors suitable for use with the LT1303 usually fall in the $5 \mu \mathrm{H}$ to $50 \mu \mathrm{H}$ range. The inductor must: (1) handle current of 1.25 A without saturating, (2) have enough inductance to provide a di/dt lower than $400 \mathrm{~mA} / \mu \mathrm{s}$, and (3) have low enough DC resistance to avoid excessive heating or efficiency losses. Higher value inductors will deliver more power but tend to be physically larger. Most ferrite core drum or rod inductors such as those specified in Table 1 are suitable for use. It is acceptable to bias openflux inductors (e.g. Sumida CD54) into saturation by 10 to 20\% without adverse effects.

## Table 1. Recommended Inductors

| VENDOR | SERIES | APPROPRIATE VALUES | PHONE <br> NUMBERS |
| :--- | :--- | :--- | :--- |
| Coilcraft | D03316 <br> D01608 | $10 \mu \mathrm{H}$ to $47 \mu \mathrm{H}$ <br> $10 \mu \mathrm{H}$ | $(708) 639-6400$ |
| Coiltronics | OCTAPAK <br> CTX20-1 | $20 \mu \mathrm{H}$ <br> $20 \mu \mathrm{H}$ | $(407) 241-7876$ |
|  | CTX20-2 |  |  |
| CTX33-4 | $33 \mu \mathrm{H}$ |  |  |
| Sumida | CD54 | $10 \mu \mathrm{H}$ to $33 \mu \mathrm{H}$ | (708) 956-0666 |
| Gowanda | GA10 | $10 \mu \mathrm{H}$ to $33 \mu \mathrm{H}$ | (716) 532-2234 |

Figure 7 shows inductor current of a suitable inductor, di/dt is controlled at all times. The rapid rise in current shown in Figure 8 results from this inductor saturating at approximately 1A. Saturation occurs when the inductor cannot hold any more magnetic energy in the core. Current then increases rapidly, limited only by the resistance of the winding. Figure 9's inductor has high DC resistance which results in the exponential time constant shape of the inductor current.


Figure 7. Properly Chosen Inductor Does Not Saturate

## APPLICATIONS INFORMATION



Figure 8. This Inductor Saturates at $\mathrm{I}_{\mathrm{L}} \sim 1 \mathrm{~A}$. A Poor Choice


Figure 9. Slight Exponential Shape to Inductor Current Waveform Indicates Excessive DC Resistance

## Diode Selection

The LT1303's high switching speed demands a high speed rectifier. Schottky diodes are preferred for their low forward drop and fast recovery. Suitable choices include the 1N5817, MBRS120LT3, and MBR0520LT1. Do not use signal diodes such as 1N4148. They cannot carry 1A current. Also avoid "general-purpose" diodes such as 1N4001. These are far too slow and are unsuitable for any switching regulator application. For high temperature applications a silicon diode such as the MUR105 will have less leakage.

## Capacitor Selection

Input and output capacitors should have low ESR for best efficiency. Recommended capacitors include AVX TPS series, Sprague 595D series, and Sanyo OS-CON. The output capacitor's ESR determines the high frequency ripple amplitude. A $100 \mu \mathrm{~F}$ capacitor is the minimum recommended for a 5 V output. Higher output voltages can use lower capacitance values. For example, a 12 V output can use a $33 \mu \mathrm{~F}$ or $47 \mu \mathrm{~F}$ capacitor. The $\mathrm{V}_{\text {IN }}$ pin of the LT1303 should be decoupled with a $47 \mu \mathrm{~F}$ or $100 \mu \mathrm{~F}$ capacitor at the pin. When driving a transformer, an additional decoupling network of $10 \Omega$ and $0.1 \mu \mathrm{~F}$ ceramic is recommended as shown in Figure 10.


Figure 10. 10 $\Omega$-1 $\mu$ F Network to LT1303 $V_{\text {IN }}$ Pin Provides Additional Decoupling. Recommended When Driving Transformers.

Table 2. Recommended Capacitors

| VENDOR | SERIES | TYPE | PHONE <br> NUMBERS |
| :--- | :--- | :--- | :--- |
| AVX | TPS | Surface Mount | (803) 448-9411 |
| Sanyo | OS-CON | Through-Hole | (619) 661-6835 |
| Panasonic | HFQ | Through-Hole | $(201) 348-5200$ |
| Sprague | 595D | Surface Mount | $(603) 224-1961$ |

## TYPICAL APPLICATIONS

## Setting Output Voltage on LT1303



5V Step-Up Converter with Reference Output


## TYPICAL APPLICATIONS

4-, 5-Cell to 5V Converter with Output Disconnect


3-Cell to 3.3V Boost/Linear Converter with Output Disconnect


TYPICAL APPLICATIONS

## EL Panel Driver



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## LT1303/LT1303-5

PACKAGE DESCRIPTIO Dimensions in inches (millimeters) unless otherwise noted.

*THESE DIMENSIONS DO NOT INCLUDE MOLD FLASH OR PROTRUSIONS.
MOLD FLASH OR PROTRUSIONS SHALL NOT EXCEED 0.010 INCH ( 0.254 mm )


## RELATGD PARTS

| PART NUMBER | DESCRIPTION | COMMENTS |
| :--- | :--- | :--- |
| LT1129 | Micropower Low Dropout Regulator | 700mA Output Current in S0-8 Package |
| LT1182/83/84 | LCD and CCFL Backlight Controller | High Efficiency and Excellent Backlight Control Range |
| LT1301 | 5V to 12V/200mA Step-Up DC/DC Converter | 120 $\mu$ A Quiescent Current |
| LT1302 | 2-Cell to 5V/600mA Step-Up DC/DC Converter | 200 $\mu$ A Quiescent Current |
| LT1305 | Micropower 2A Switch DC/DC Converter with Low-Battery Detect | 2V to 5V at 400mA |
| LT1372 | 500kHz Step-Up PWM, 1.5A Switch | Low Noise, Fixed Frequency Operation |
| LTC ${ }^{\circledR} 1472$ | PCMCIA Host Switch with Protection | Includes Current Limit and Thermal Shutdown |


[^0]:    *ADD C1 FOR OPEN-PANEL PROTECTION
    **DALE LPE5047-A132 1:15 TURNS RATIO (605) 666-9301
    ${ }^{\dagger}$ R1 ADJUSTS V ${ }_{\text {OUT }} 83 \mathrm{~V}_{\text {RMS }}$ TO $115 \mathrm{~V}_{\text {RMS }}$

