## feATURES

- 300MHz Bandwidth on Single 5V and $\pm 5 \mathrm{~V}$ ( $A_{V}=1,2$ and -1)
- 0.1dB Gain Flatness: $150 \mathrm{MHz}\left(A_{V}=1,2\right.$ and -1$)$
- High Slew Rate: 800V/us
- Wide Supply Range:
$\pm 2 \mathrm{~V}$ to $\pm 6 \mathrm{~V}$ (Dual Supply)
4V to 12V (Single Supply)
- 80mA Output Current
- Low Supply Current: 3.9mA/Amplifier
- Shutdown Mode
- Fast Turn-On Time: 30ns
- Fast Turn-Off Time: 40ns
- Small 0.75 mm Tall 16 -Lead $3 \mathrm{~mm} \times 3 \mathrm{~mm}$ QFN Package


## APPLICATIONS

- RGB/YP $P_{B} P_{R}$ Cable Drivers
- LCD Projectors
- KVM Switches
- A/V Receivers
- MUX Amplifiers
- Composite Video Cable Drivers
- ADC Drivers


## Low Cost $5 \mathrm{~V} / \pm 5 \mathrm{~V} 300 \mathrm{MHz}$ Triple Video Amplifier in $3 \mathrm{~mm} \times 3 \mathrm{~mm}$ QFN DESCRIPTION

The LT® ${ }^{\oplus} 659$ is a low cost, high speed, triple amplifier that has been optimized for excellent video performance on a single 5V supply, yet fits in the small footprint of a $3 \mathrm{~mm} \times$ 3 mm QFN package. With a -3 dB bandwidth of 300 MHz , a 0.1 dB bandwidth of 150 MHz , and a slew rate of $800 \mathrm{~V} / \mu \mathrm{s}$, the LT6559's dynamic performance is an excellent match for high speed RGB or $\mathrm{YP}_{\mathrm{B}} \mathrm{P}_{\mathrm{R}}$ video applications.
For multiplexing applications such as KVM switches or selectable video inputs, each channel has an independent high speed enable/disable pin. Each amplifier will turn on in 30 ns and off in 40 ns . When enabled, each amplifier draws 3.9 mA from a 5 V supply. The LT6559 operates on a single supply voltage ranging from 4 V to 12 V , and on split supplies ranging from $\pm 2 \mathrm{~V}$ to $\pm 6 \mathrm{~V}$.
The LT6559 comes in a compact 16 -lead $3 \mathrm{~mm} \times 3 \mathrm{~mm}$ QFN package, and operates over a $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$ temperature range. The LT6559 is manufactured on Linear Technology's proprietary complementary bipolar process.
$\boldsymbol{\Omega}$, LT, LTC and LTM are registered trademarks of Linear Technology Corporation. All other trademarks are the property of their respective owners.

## TYPICAL APPLICATION

3-Input Video MUX Cable Driver


Square Wave Response

ABSOLUTE MAXIMUM RATIOGS(Note 1)
Total Supply Voltage ( $\mathrm{V}^{+}$to $\mathrm{V}^{-}$) ..... 12.6 V
Input Current (Note 2). ..... $\pm 10 \mathrm{~mA}$
Output Current ..... $\pm 100 \mathrm{~mA}$
Differential Input Voltage (Note 2) ..... $\pm 5 \mathrm{~V}$
Output Short-Circuit Duration (Note 3) ..... Continuous
Operating Temperature Range (Note 9) ..... $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$
Specified Temperature Range (Note 4) .. $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$Storage Temperature Range. $-65^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$
Junction Temperature (Note 5) ..... $125^{\circ} \mathrm{C}$

PACKAGE/ORDER INFORMATION


Consult LTC Marketing for parts specified with wider operating temperature ranges.

* Ground pins are not internally connected. For best channel isolation, connect to ground.
$5 V$ ELECTRICAL CHARACTERISTICS The $\bullet$ denotes specifications which apply over the specified operating temperature range, otherwise specifications are at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$. For each amplifier: $\mathrm{V}_{C M}=2.5 \mathrm{~V}, \mathrm{~V}_{S}=5 \mathrm{~V}, \mathrm{EN}=0 \mathrm{~V}$, pulse tested, unless otherwise noted. (Note 4)

| SYMBOL | PARAMETER | CONDITIONS |  | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\text {OS }}$ | Input Offset Voltage |  | $\bullet$ |  | 1.5 | $\begin{aligned} & 10 \\ & 12 \end{aligned}$ | mV mV |
| $\Delta \mathrm{V}_{\text {OS }} / \Delta \mathrm{T}$ | Input Offset Voltage Drift |  | $\bullet$ |  | 15 |  | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| $\mathrm{liN}^{+}$ | Noninverting Input Current |  | - |  | 10 | $\begin{aligned} & 25 \\ & 30 \end{aligned}$ | $\mu \mathrm{A}$ $\mu \mathrm{A}$ |
| $1 \mathrm{IN}^{-}$ | Inverting Input Current |  | $\bullet$ |  | 10 | $\begin{aligned} & 60 \\ & 70 \end{aligned}$ | $\mu \mathrm{A}$ $\mu \mathrm{A}$ |
| $\mathrm{e}_{\mathrm{n}}$ | Input Noise Voltage Density | $f=1 \mathrm{kHz}, R_{F}=1 \mathrm{k}, R_{G}=10 \Omega, R_{S}=0 \Omega$ |  |  | 4.5 |  | $\mathrm{nV} / \sqrt{\mathrm{Hz}}$ |
| $+i_{n}$ | Noninverting Input Noise Current Density | $\mathrm{f}=1 \mathrm{kHz}$ |  |  | 6 |  | $\mathrm{pA} / \sqrt{\mathrm{Hz}}$ |
| $-i_{n}$ | Inverting Input Noise Current Density | $\mathrm{f}=1 \mathrm{kHz}$ |  |  | 25 |  | $\mathrm{pA} / \sqrt{\mathrm{Hz}}$ |
| $\mathrm{R}_{\text {IN }}$ | Input Resistance | $\mathrm{V}_{\text {IN }}= \pm 1 \mathrm{~V}$ |  |  | 0.14 |  | $\mathrm{M} \Omega$ |
| $\mathrm{C}_{\text {IN }}$ | Input Capacitance | Amplifier Enabled Amplifier Disabled |  |  | $\begin{aligned} & 2.0 \\ & 2.5 \end{aligned}$ |  | pF pF |
| Cout | Output Capacitance | Amplifier Disabled |  |  | 8.5 |  | pF |
| $\mathrm{V}_{\text {INH }}$ | Input Voltage Range, High |  |  | 3.5 | 4.0 |  | V |
| $V_{\text {INL }}$ | Input Voltage Range, Low |  |  |  | 1.0 | 1.5 | V |
| VOUTH | Maximum Output Voltage Swing, High | $\mathrm{R}_{\mathrm{L}}=100 \mathrm{k}$ |  | 4.1 | 4.15 |  | V |
| $V_{\text {OUTL }}$ | Maximum Output Voltage Swing, Low | $\mathrm{R}_{\mathrm{L}}=100 \mathrm{k}$ |  |  | 0.85 | 0.9 | V |
| $\mathrm{V}_{\text {OUTH }}$ | Maximum Output Voltage Swing, High | $\begin{aligned} & R_{L}=150 \Omega \\ & R_{L}=150 \Omega \end{aligned}$ | $\bullet$ | $\begin{aligned} & 3.85 \\ & 3.65 \end{aligned}$ | 3.95 |  | V |
|  |  |  |  |  |  |  | $6559 f$ |

$5 V$ ELECTRICAL CHARACTERISTICS The e denotes speciificaions which apply over the specified operating temperature range, otherwise specifications are at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$. For each amplifier: $\mathrm{V}_{\mathrm{CM}}=2.5 \mathrm{~V}, \mathrm{~V}_{S}=5 \mathrm{~V}, \mathrm{EN}=0 \mathrm{~V}$, pulse tested, unless otherwise noted. (Note 4)

| SYMBOL | PARAMETER | CONDITIONS |  | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $V_{\text {OUTL }}$ | Maximum Output Voltage Swing, Low | $\begin{aligned} & R_{L}=150 \Omega \\ & R_{L}=150 \Omega \\ & \hline \end{aligned}$ | $\bullet$ |  | 1.05 | $\begin{aligned} & 1.15 \\ & 1.35 \end{aligned}$ | V |
| CMRR | Common Mode Rejection Ratio | $\mathrm{V}_{\mathrm{CM}}=1.5 \mathrm{~V}$ to 3.5 V |  | 40 | 50 |  | dB |
| PSRR | Power Supply Rejection Ratio | $\mathrm{V}_{\mathrm{S}}= \pm 2 \mathrm{~V}$ to $\pm 5 \mathrm{~V}, \overline{\mathrm{EN}}=\mathrm{V}^{-}$ |  | 56 | 70 |  | dB |
| $\underline{\mathrm{R}_{0 \mathrm{~L}}}$ | Transimpedance, $\Delta \mathrm{V}_{\text {OUT }} / \Delta \mathrm{I}_{\text {IN }}{ }^{-}$ | $\mathrm{V}_{\text {OUT }}=1.5 \mathrm{~V}$ to 3.5V, $\mathrm{R}_{\mathrm{L}}=150 \Omega$ |  | 40 | 80 |  | k $\Omega$ |
| IOUT | Maximum Output Current | $\mathrm{R}_{\mathrm{L}}=0 \Omega$ |  |  | 65 |  | mA |
| $\mathrm{I}_{S}$ | Supply Current per Amplifier |  | $\bullet$ |  | 3.9 | 6.1 | mA |
|  | Disable Supply Current per Amplifier | $\overline{\mathrm{EN}}$ Pin Voltage $=4.5 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=150 \Omega$ | $\bullet$ |  | 0.1 | 100 | $\mu \mathrm{A}$ |
| IEN | Enable Pin Current |  |  |  | 30 |  | $\mu \mathrm{A}$ |
| SR | Slew Rate (Note 6) | $A_{V}=10, R_{L}=150 \Omega, V_{S}= \pm 5 \mathrm{~V}$ |  |  | 500 |  | $\mathrm{V} / \mathrm{\mu s}$ |
| ton | Turn-On Delay Time (Note 7) | $\mathrm{R}_{\mathrm{F}}=\mathrm{R}_{\mathrm{G}}=301 \Omega, \mathrm{R}_{\mathrm{L}}=150 \Omega, \mathrm{~V}_{S}= \pm 5 \mathrm{~V}$ |  |  | 30 | 75 | ns |
| $\mathrm{t}_{\text {OFF }}$ | Turn-Off Delay Time (Note 7) | $\mathrm{R}_{F}=\mathrm{R}_{\mathrm{G}}=301 \Omega, \mathrm{R}_{\mathrm{L}}=150 \Omega, \mathrm{~V}_{S}= \pm 5 \mathrm{~V}$ |  |  | 40 | 100 | ns |
| $\mathrm{tr}_{\mathrm{r}} \mathrm{t}_{\mathrm{f}}$ | Small-Signal Rise and Fall Time | $\begin{aligned} & \mathrm{R}_{\mathrm{F}}=\mathrm{R}_{\mathrm{G}}=301 \Omega, \mathrm{R}_{\mathrm{L}}=150 \Omega, \mathrm{~V}_{\text {OUT }}=1 \mathrm{~V}_{\mathrm{P}-\mathrm{P},} \\ & \mathrm{~V}_{\mathrm{S}}= \pm 5 \mathrm{~V} \end{aligned}$ |  |  | 1.3 |  | ns |
| $t_{\text {PD }}$ | Propagation Delay | $\begin{aligned} & \mathrm{R}_{\mathrm{F}}=\mathrm{R}_{\mathrm{G}}=301 \Omega, \mathrm{R}_{\mathrm{L}}=150 \Omega, \mathrm{~V}_{\text {OUT }}=1 \mathrm{~V}_{\mathrm{P}-\mathrm{P},} \\ & \mathrm{~V}_{\mathrm{S}}= \pm 5 \mathrm{~V} \end{aligned}$ |  |  | 2.5 |  | ns |
| OS | Small-Signal Overshoot | $\begin{aligned} & \mathrm{R}_{\mathrm{F}}=\mathrm{R}_{\mathrm{G}}=301 \Omega, \mathrm{R}_{\mathrm{L}}=150 \Omega, \mathrm{~V}_{0 U T}=1 \mathrm{~V}_{\mathrm{P}-\mathrm{P},} \\ & \mathrm{~V}_{\mathrm{S}}= \pm 5 \mathrm{~V} \end{aligned}$ |  |  | 10 |  | \% |
| $\mathrm{t}_{5}$ | Settling Time | $\begin{aligned} & 0.1 \%, A_{V}=-1 V, R_{F}=R_{G}=301 \Omega, R_{L}= \\ & 150 \Omega, V_{S}= \pm 5 \mathrm{~V} \end{aligned}$ |  |  | 25 |  | ns |
| dG | Differential Gain (Note 8) | $\mathrm{R}_{F}=\mathrm{R}_{\mathrm{G}}=301 \Omega, \mathrm{R}_{\mathrm{L}}=150 \Omega, \mathrm{~V}_{S}= \pm 5 \mathrm{~V}$ |  |  | 0.13 |  | \% |
| dP | Differential Phase (Note 8) | $\mathrm{R}_{\mathrm{F}}=\mathrm{R}_{\mathrm{G}}=301 \Omega, \mathrm{R}_{\mathrm{L}}=150 \Omega, \mathrm{~V}_{S}= \pm 5 \mathrm{~V}$ |  |  | 0.10 |  | DEG |

## $\pm 5 V$ ELECTRICAL CHARACTERISTICS The • denotes specifications which apply over the specified

operating temperature range, otherwise specifications are at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$. For each amplifier: $\mathrm{V}_{\mathrm{CM}}=\mathrm{OV}, \mathrm{V}_{\mathrm{S}}= \pm 5 \mathrm{~V}, \mathrm{EN}=0 \mathrm{~V}$, pulse tested, unless otherwise noted. (Note 4)

$\pm 5 V$ ELECTRICAL CHARACTGRISTICS The • denotes specifications which apply over the specified operating temperature range, otherwise specifications are at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$. For each amplifier: $\mathrm{V}_{\mathrm{CM}}=\mathrm{OV}, \mathrm{V}_{\mathrm{S}}= \pm 5 \mathrm{~V}, \mathrm{EN}=\mathrm{OV}$, pulse tested, unless otherwise noted. (Note 4)

| SYMBOL | PARAMETER | CONDITIONS |  | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| VOUTL | Maximum Output Voltage Swing, Low | $\mathrm{R}_{\mathrm{L}}=100 \mathrm{k}$ |  |  | -4.2 | -4.0 | V |
| VOUTH | Maximum Output Voltage Swing, High | $\begin{aligned} & \mathrm{R}_{\mathrm{L}}=150 \Omega \\ & \mathrm{R}_{\mathrm{L}}=150 \Omega \\ & \hline \end{aligned}$ | $\bullet$ | $\begin{aligned} & 3.4 \\ & 3.2 \end{aligned}$ | 3.6 |  | V |
| $V_{\text {OUTL }}$ | Maximum Output Voltage Swing, Low | $\begin{aligned} & \mathrm{R}_{\mathrm{L}}=150 \Omega \\ & \mathrm{R}_{\mathrm{L}}=150 \Omega \end{aligned}$ | $\bullet$ |  | -3.6 | $\begin{aligned} & \hline-3.4 \\ & -3.2 \end{aligned}$ | V |
| CMRR | Common Mode Rejection Ratio | $\mathrm{V}_{\mathrm{CM}}= \pm 3.5 \mathrm{~V}$ |  | 42 | 52 |  | dB |
| PSRR | Power Supply Rejection Ratio | $\mathrm{V}_{S}= \pm 2 \mathrm{~V}$ to $\pm 5 \mathrm{~V}, \overline{\mathrm{EN}}=\mathrm{V}^{-}$ |  | 56 | 70 |  | dB |
| $\mathrm{R}_{\text {OL }}$ | Transimpedance, $\Delta \mathrm{V}_{\text {OUT }} / \Delta \mathrm{I}_{\text {IN }}{ }^{-}$ | $\mathrm{V}_{\text {OUT }}= \pm 2 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=150 \Omega$ |  | 40 | 100 |  | k $\Omega$ |
| IOUT | Maximum Output Current | $\mathrm{R}_{\mathrm{L}}=0 \Omega$ |  |  | 100 |  | mA |
| IS | Supply Current per Amplifier | $\mathrm{V}_{\text {OUT }}=0 \mathrm{~V}$ | $\bullet$ |  | 4.6 | 6.5 | mA |
|  | Disable Supply Current per Amplifier | $\overline{\mathrm{EN}}$ Pin Voltage $=4.5 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=150 \Omega$ | $\bullet$ |  | 0.1 | 100 | $\mu \mathrm{A}$ |
| IEN | Enable Pin Current |  |  | 30 |  |  | $\mu \mathrm{A}$ |
| SR | Slew Rate (Note 6) | $A_{V}=10, R_{L}=150 \Omega$ |  | 500 | 800 |  | V/ $/ \mathrm{s}$ |
| $\mathrm{t}_{\mathrm{ON}}$ | Turn-On Delay Time (Note 7) | $\mathrm{R}_{\mathrm{F}}=\mathrm{R}_{\mathrm{G}}=301 \Omega, \mathrm{R}_{\mathrm{L}}=150 \Omega$ |  |  | 30 | 75 | ns |
| $\mathrm{t}_{\text {OFF }}$ | Turn-Off Delay Time (Note 7) | $\mathrm{R}_{\mathrm{F}}=\mathrm{R}_{\mathrm{G}}=301 \Omega, \mathrm{R}_{\mathrm{L}}=150 \Omega$ |  |  | 40 | 100 | ns |
| $\mathrm{t}_{\mathrm{r}}, \mathrm{t}_{\mathrm{f}}$ | Small-Signal Rise and Fall Time | $\mathrm{R}_{\mathrm{F}}=\mathrm{R}_{\mathrm{G}}=301 \Omega, \mathrm{R}_{\mathrm{L}}=150 \Omega, \mathrm{~V}_{\text {OUT }}=1 \mathrm{~V}_{P-P}$ |  |  | 1.3 |  | ns |
| $t_{\text {PD }}$ | Propagation Delay | $\mathrm{R}_{\mathrm{F}}=\mathrm{R}_{\mathrm{G}}=301 \Omega, \mathrm{R}_{\mathrm{L}}=150 \Omega, \mathrm{~V}_{\text {OUT }}=1 \mathrm{~V}_{P-P}$ |  |  | 2.5 |  | ns |
| OS | Small-Signal Overshoot | $\mathrm{R}_{\mathrm{F}}=\mathrm{R}_{\mathrm{G}}=301 \Omega, \mathrm{R}_{\mathrm{L}}=150 \Omega, \mathrm{~V}_{\text {OUT }}=1 \mathrm{~V}_{P-P}$ |  |  | 10 |  | \% |
| ts | Settling Time | $0.1 \%, A_{V}=-1, R_{F}=R_{G}=301 \Omega, R_{L}=150 \Omega$ |  |  | 25 |  | ns |
| dG | Differential Gain (Note 8) | $\mathrm{R}_{\mathrm{F}}=\mathrm{R}_{\mathrm{G}}=301 \Omega, \mathrm{R}_{\mathrm{L}}=150 \Omega$ |  |  | 0.13 |  | \% |
| dP | Differential Phase (Note 8) | $\mathrm{R}_{\mathrm{F}}=\mathrm{R}_{\mathrm{G}}=301 \Omega, \mathrm{R}_{\mathrm{L}}=150 \Omega$ |  |  | 0.10 |  | DEG |

Note 1: Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. Exposure to any Absolute Maximum Rating condition for extended periods may affect device reliability and lifetime.
Note 2: This parameter is guaranteed to meet specified performance through design and characterization. It has not been tested.
Note 3: A heat sink may be required depending on the power supply voltage and how many amplifiers have their outputs short circuited.
Note 4: The LT6559 is guaranteed to meet specified performance from $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ and is designed, characterized and expected to meet these extended temperature limits, but is not tested or QA sampled at $-40^{\circ} \mathrm{C}$ and $85^{\circ} \mathrm{C}$.
Note 5: $T_{j}$ is calculated from the ambient temperature $T_{A}$ and the power dissipation $P_{D}$ according to the following formula: $T_{J}=T_{A}+\left(P_{D} \bullet 68^{\circ} \mathrm{C} / \mathrm{W}\right)$
Note 6: At $\pm 5 \mathrm{~V}$, slew rate is measured at $\pm 2 \mathrm{~V}$ on a $\pm 3 \mathrm{~V}$ output signal. At 5 V , slew rate is measured from 2 V to 3 V on a 1.5 V to 3.5 V output signal. Slew
rate is $100 \%$ production tested at $\pm 5 \mathrm{~V}$ for both the rising and falling edge of the $B$ channel. The slew rate of the $R$ and $G$ channels is guaranteed through design and characterization.
Note 7: Turn-on delay time ( $\mathrm{t}_{\mathrm{ON}}$ ) is measured from control input to appearance of 1 V at the output, for $\mathrm{V}_{I N}=1 \mathrm{~V}$. Likewise, turn-off delay time ( $\mathrm{t}_{\mathrm{ofF}}$ ) is measured from control input to appearance of 0.5 V on the output for $\mathrm{V}_{\text {IN }}=0.5 \mathrm{~V}$. This specification is guaranteed by design and characterization.
Note 8: Differential gain and phase are measured using a Tektronix TSG120YC/NTSC signal generator and a Tektronix 1780R Video Measurement Set. The resolution of this equipment is $0.1 \%$ and $0.1^{\circ}$. Ten identical amplifier stages were cascaded giving an effective resolution of $0.01 \%$ and $0.01^{\circ}$.
Note 9: The LT6559 is guaranteed functional over the operating temperature range of $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$.

TYPICAL AC PERFORMANCE

| $\mathbf{V}_{\mathbf{S}}(\mathbf{V})$ | $\mathbf{A}_{\boldsymbol{V}}$ | $\mathbf{R}_{\mathbf{L}}(\Omega)$ | $\mathbf{R}_{\mathbf{F}}(\Omega)$ | $\mathbf{R}_{\mathbf{G}}(\Omega)$ | SMALL SIGNAL <br> -3 dB <br> BW (MHz) | SMALL SIGNAL <br> $\mathbf{0} \mathbf{0} 1 \mathrm{1dB}$ BW (MHz) | SMALL SIGNAL <br> PEAKING (dB) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\pm 5,5$ | 1 | 150 | 365 | - | 300 | 150 | 0.05 |
| $\pm 5,5$ | 2 | 150 | 301 | 301 | 300 | 150 | 0 |
| $\pm 5,5$ | -1 | 150 | 301 | 301 | 300 | 150 | 0 |

## TYPICAL PERFORMANCE CHARACTERISTICS



Large-Signal Transient Response
( $A_{V}=1$ )


Closed-Loop Gain vs Frequency
( $A_{V}=2$ )


Large-Signal Transient Response ( $A_{V}=2$ )


## Maximum Undistorted Output

Voltage vs Frequency


Closed-Loop Gain vs Frequency
( $A_{V}=-1$ )


Large-Signal Transient Response ( $A_{V}=-1$ )



TYPICAL PERFORMANCE CHARACTERISTICS


Maximum Capacitive Load vs Feedback Resistor


6559 G13

Output Impedance vs Frequency


6559 G11
Capacitive Load
vs Output Series Resistor


6559 G14

## Enable Pin Current

 vs Temperature

Output Impedance (Disabled) vs Frequency


Supply Current per Amplifier vs Supply Voltage


Positive Supply Current per Amplifier vs Temperature


## TYPICAL PERFORMANCE CHARACTERISTICS



All Hostile Crosstalk


Propagation Delay

$\mathrm{A}_{\mathrm{V}}=+2 \quad$ TIME $(500 \mathrm{ps} / \mathrm{DIV})$
$R_{L}=150 \Omega$
$\mathrm{R}_{\mathrm{F}}=\mathrm{R}_{\mathrm{G}}=301 \Omega$

Input Bias Currents
vs Temperature


All Hostile Crosstalk (Disabled)


6559 G24

Rise Time and Overshoot

$\mathrm{A}_{\mathrm{V}}=+2 \quad$ TIME ( $500 \mathrm{ps} / \mathrm{DIV}$ )
$R_{L}=150 \Omega$
$R_{F}=R_{G}=301 \Omega$

## PIn fUnCTIOnS

GND (Pins 1, 4): Ground. Not connected internally.
-IN G (Pin 2): Inverting Input of G Channel Amplifier.
+IN G (Pin 3): Noninverting Input of G Channel Amplifier.
+IN B (Pin 5): Noninverting Input of B Channel Amplifier.
-IN B (Pin 6): Inverting Input of B Channel Amplifier.
$\overline{\text { EN }}$ B (Pin 7): B Channel Enable Pin. Logic low to enable.
OUT B (Pin 8): B Channel Output.
$\mathbf{V}^{-}$(Pin 9): Negative Supply Voltage, Usually Ground or -5 V .

OUT G (Pin 10): G Channel Output.
$\overline{\mathrm{EN}} \mathrm{G}$ (Pin 11): G Channel Enable Pin. Logic low to enable.
$\mathbf{V}^{+}$(Pin 12): Positive Supply Voltage, Usually 5V.
OUT R (Pin 13): R Channel Output.
EN R (Pin 14): R Channel Enable Pin. Logic low to enable.
-IN R (Pin 15): Inverting Input of R Channel Amplifier.
+IN R (Pin 16): Noninverting Input of R Channel Amplifier.
Exposed Pad (Pin 17): V . Must Be Soldered to the PCB.

## APPLICATIONS INFORMATION

## Feedback Resistor Selection

The small-signal bandwidth of the LT6559 is set by the external feedback resistors and the internal junction capacitors. As a result, the bandwidth is a function of the supply voltage, the value of the feedback resistor, the closed-loop gain and the load resistor. Optimized for $\pm 5 \mathrm{~V}$ and single-supply 5 V operation, the LT6559 has a -3 dB bandwidth of 300 MHz at gains of $+1,-1$, or +2 . Refer to the resistor selection guide in the Typical AC Performance table.

## Capacitance on the Inverting Input

Currentfeedback amplifiers require resistive feedback from the output to the inverting input for stable operation. Take care to minimize the stray capacitance between the output and the inverting input. Capacitance on the inverting input to ground will cause peaking in the frequency response and overshoot in the transient response.

## Capacitive Loads

The LT6559 can drive many capacitive loads directly when the proper value of feedback resistor is used. The required value for the feedback resistor will increase as load capacitance increases and as closed-loop gain decreases. Alternatively, a small resistor ( $5 \Omega$ to $35 \Omega$ ) can be put in series with the output to isolate the capacitive load from the amplifier output. This has the advantage that the ampli-
fier bandwidth is only reduced when the capacitive load is present. The disadvantage is that the gain is a function of the load resistance.

## Power Supplies

The LT6559 will operate from single or split supplies from $\pm 2 \mathrm{~V}$ ( 4 V total) to $\pm 6 \mathrm{~V}$ ( 12 V total). It is not necessary to use equal value split supplies, however the offset voltage and inverting input bias current will change. The offset voltage changes about $600 \mu \mathrm{~V}$ per volt of supply mismatch. The inverting bias current will typically change about $2 \mu \mathrm{~A}$ per volt of supply mismatch.

## Slew Rate

Unlike a traditional voltage feedback op amp, the slew rate of a current feedback amplifier is dependent on the amplifier gain configuration. In a current feedback amplifier, both the input stage and the output stage have slew rate limitations. In the inverting mode, and for gains of 2 or more in the noninverting mode, the signal amplitude between the input pins is small and the overall slew rate is that of the output stage. For gains less than 2 in the noninverting mode, the overall slew rate is limited by the input stage.

The inputslew rate of the LT6559 is approximately $600 \mathrm{~V} / \mu \mathrm{s}$ and is set by internal currents and capacitances. The output slew rate is set by the value of the feedback resistor and

## APPLICATIONS InFORMATION

internal capacitance. At a gain of 2 with $301 \Omega$ feedback and gain resistors and $\pm 5 \mathrm{~V}$ supplies, the output slew rate is typically $800 \mathrm{~V} / \mu \mathrm{s}$. Larger feedback resistors will reduce the slew rate as will lower supply voltages.

## Enable/Disable

Each amplifier of the LT6559 has a unique high impedance, zero supply current mode which is controlled by its own $\overline{E N}$ pin. These amplifiers are designed to operate with CMOS Iogic; the amplifiers draw $0.1 \mu \mathrm{~A}$ of current when these pins are high or floated. To activate each amplifier, its $\overline{E N}$ pin is normally pulled to a logic low. However, supply current will vary as the voltage between the $\mathrm{V}^{+}$supply and EN is varied. As seen in Figure 1, $+l_{S}$ does vary with $\left(\mathrm{V}^{+}-\mathrm{V}_{\overline{\mathrm{EN}}}\right)$, particularly when the voltage difference is less than 3V. For normal operation, it is important to keep the $\overline{E N}$ pin at least 3 V below the $\mathrm{V}^{+}$supply. If a $\mathrm{V}^{+}$of less than 3 V is used, for the amplifier to remain enabled at all times the $\overline{\mathrm{EN}}$ pin should be tied to the $\mathrm{V}^{-}$supply. The enable pin current is approximately $30 \mu \mathrm{~A}$ when activated. If using CMOS open-drain logic, an external 1 k pull-up resistor is recommended to ensure that the LT6559 remains disabled regardless of any CMOS drain-leakage currents.


Figure 1. + $\mathrm{I}_{\mathrm{S}}$ vs $\left(\mathrm{V}^{+}-\mathrm{V}_{\mathrm{EN}}\right)$

The enable/disable times are very fast when driven from standard 5V CMOS logic. Each amplifier enables in about 30 ns ( $50 \%$ point to $50 \%$ point) while operating on $\pm 5 \mathrm{~V}$ supplies (Figure 2). Likewise, the disable time is approximately 40ns (50\% point to 50\% point) (Figure 3).


Figure 2. Amplifier Enable Time, $A_{V}=2$


Figure 3. Amplifier Disable Time, $A_{V}=2$

## Differential Input Signal Swing

To avoid any breakdown condition on the input transistors, the differential input swing must be limited to $\pm 5 \mathrm{~V}$. In normal operation, the differential voltage between the input pins is small, so the $\pm 5 \mathrm{~V}$ limit is not an issue. In the disabled mode however, the differential swing can be the same as the input swing, and there is a risk of device breakdown if the input voltage range has not been properly considered.

## TYPICAL APPLICATIONS

## 3-Input Video MUX Cable Driver

The application on the first page of this data sheet shows a low cost, 3-input video MUX cable driver. The scope photo below (Figure 4) displays the cable output of a 30 MHz square wave driving $150 \Omega$. In this circuit the active amplifier is loaded by the sum of $R_{F}$ and $R_{G}$ of each disabled amplifier. Resistor values have been chosen to keep the total back termination at $75 \Omega$ while maintaining a gain of 1 at the $75 \Omega$ load. The switching time between any two channels is approximately 32 ns when both enable pins are driven (Figure 5).
When building the board, care was taken to minimize trace lengths at the inverting inputs. The ground plane was also pulled a few millimeters away from $R_{F}$ and $R_{G}$ on both sides of the board to minimize stray capacitance.

## Using the LT6559 to Drive LCD Displays

Driving a variety of XGA and UXGA LCD displays can be a difficult problem because they are usually a capacitive load of over 300pF, and require fast settling.

The LT6559 is particularly well suited for driving these LCD displays because it can drive large capacitive loads with a small series resistor at the output, minimizing settling time. As seen in Figure 6, at a gain of +3 with a $16.9 \Omega$ output series resistor and a 330pF load, the LT6559 is capable of settling to $0.1 \%$ in 30 ns for a 6 V step.


Figure 5. 3-Input Video MUX Switching Response $\left(A_{V}=2\right)$


Figure 6. Large-Signal Pulse Response

## TYPICAL APPLICATIONS

## Buffered RGB to $\mathrm{YP}_{\mathrm{B}} \mathrm{P}_{\mathrm{R}}$ Conversion

An LT6559 and an LT1395 can be used to map RGB signals into $\mathrm{YP}_{\mathrm{B}} \mathrm{P}_{\mathrm{R}}$ "component" video as shown in Figure 7.
The LT1395 performs a weighted inverting addition of all three inputs. The LT1395 output includes an amplification of the $R$ input by:

$$
\frac{-324}{1.07 \mathrm{k}}=-0.30
$$

The amplification of the $G$ input is by:

$$
\frac{-324}{549}=-0.59
$$

Finally, the B input is amplified by:

$$
\frac{-324}{2.94 k}=-0.11
$$

Therefore, the LT1395 output is:

$$
-0.3 R-0.59 G-0.11 B=-Y .
$$

This output is further scaled and inverted by $-301 / 150$ $=-2$ by LT6559 section A2, thus producing 2 Y . With the division by two that occurs due to the termination resistors, the desired $Y$ signal is generated at the load.

The LT6559 section A1 provides a gain of 2 for the R signal, and performs a subtraction of 2 Y from the section A2 output. The output resistor divider provides a scaling factor of 0.71 and forms the $75 \Omega$ back-termination resistance. Thus, the signal seen at the terminated load is the desired $0.71(R-Y)=P_{R}$.
The LT6559 section A3 provides a gain of 2 for the $B$ signal, and also performs a subtraction of $2 Y$ from the section A2 output. The output resistor divider provides a scaling factor of 0.57 and forms the $75 \Omega$ back-termination resistance. Thus the signal seen at the terminated load is the desired $0.57(\mathrm{~B}-\mathrm{Y})=\mathrm{P}_{\mathrm{B}}$.

For this circuit to develop a normal sync on the $Y$ signal, a normal sync must be inserted on each of the R, G, and $B$ inputs. Alternatively, additional circuitry could be added to inject sync directly at the $Y$ output with controlled current pulses.


Figure 7. RGB to $\mathrm{YP}_{\mathrm{B}} \mathrm{P}_{\mathrm{R}}$ Conversion

## LT6559

## TYPICAL APPLICATIONS

## $\mathrm{YP}_{\mathrm{B}} \mathrm{P}_{\mathrm{R}}$ to RGB Conversion

Two LT6559s can be used to map the $\mathrm{Y}_{\mathrm{B}} \mathrm{P}_{\mathrm{R}}$ "component" video into the RGB color space as shown in Figure 8. The $Y$ input is properly terminated with $75 \Omega$ and buffered with a gain of 2 by amplifier A 2 . The $\mathrm{P}_{\mathrm{R}}$ input is terminated and buffered with a gain of 2.8 by amplifier $A 1$. The $P_{B}$ input is terminated and buffered with a gain of 3.6 by amplifier A3.

Amplifier B 1 performs an equally weighted addition of amplifiers A1 and A2 outputs, thereby producing $2\left(\mathrm{Y}+1.4 \mathrm{P}_{\mathrm{R}}\right)$, which generates the desired R signal at the terminated load due to the voltage division by 2 caused by the termination resistors. Amplifier B3 forms the equally weighted addition of amplifiers A 2 and A 3 outputs, thereby producing $2\left(Y+1.8 \mathrm{P}_{\mathrm{B}}\right)$, which generates the desired B signal at the terminated load.

Amplifier B2 performs a weighted summation of all three inputs. The $P_{B}$ signal is amplified overall by:

$$
\frac{-301}{1.54 \mathrm{k}} \cdot 3.6=2(-0.34)
$$

The $P_{\mathrm{R}}$ signal is amplified overall by:

$$
\frac{-301}{590} \cdot 2.8=2(-0.71)
$$

The Y signal is amplified overall by:

$$
\frac{1 \mathrm{k}}{1 \mathrm{k}+698} \cdot 1+\frac{301}{590 \| 1.54 \mathrm{k}} \cdot 2=2(1)
$$

Therefore the amplifier B2 output is:

$$
2\left(Y-0.34 P_{B}-0.71 P_{R}\right)
$$

which generates the desired G signal at the terminated load.
The sync present on the $Y$ input is reconstructed on all three R, G, and B outputs.


Figure 8. $\mathrm{YP}_{\mathrm{B}} \mathrm{P}_{\mathrm{R}}$ to RGB Conversion

## LT6559

## TYPICAL APPLICATIONS

## Application (Demo) Boards

The DC1063A demo board has been created for evaluating the LT6559 and is available directly from Linear Technology. It has been designed as an RGB video buffer/cable driver, using standard VGA 15-pin D-Sub (HD-15) connectors for input and output signals. All sync signals are also passed directly from the input to the output, so the LT6559's performance can be determined by applying a 5 V supply to the DC1063A demo board and then inserting the board between a computer's analog video output and
a monitor. Schematics for the DC1063A demo board can be found on the back page of this datasheet.
As seen in the DC1063A schematic, each amplifier is configured in a gain of 2 , witha $75 \Omega$ back-termination resulting in a final gain of 1 . Each input is properly terminated for $75 \Omega$ input impedance with AC coupling capacitors at each input and output. Additionally, for proper operation, the positive input of each amplifier is biased to mid-supply with a high impedance resistor divider.

As seen below, the DC1063A is a 2-sided board.


Figure 9. DC1063A Component Locator


Figure 10. DC1063A Top Side


Figure 11. DC1063A Bottom Side

LT6559
SIMPLIFIED SCHEMATIC, each amplifier


PACKAGE DESCRIPTION

## UD Package

16-Lead Plastic QFN ( $3 \mathrm{~mm} \times 3 \mathrm{~mm}$ )
(Reference LTC DWG \# 05-08-1691)

recommended solder pad pitch and dimensions


NOTE:

1. DRAWING CONFORMS TO JEDEC PACKAGE OUTLINE MO-220 VARIATION (WEED-2)
2. DRAWING NOT TO SCALE
3. ALL DIMENSIONS ARE IN MILLIMETERS
4. DIMENSIONS OF EXPOSED PAD ON BOTTOM OF PACKAGE DO NOT INCLUDE MOLD FLASH. MOLD FLASH, IF PRESENT, SHALL NOT EXCEED 0.15 mm ON ANY SIDE
5. EXPOSED PAD SHALL BE SOLDER PLATED
6. SHADED AREA IS ONLY A REFERENCE FOR PIN 1 LOCATION ON THE TOP AND BOTTOM OF PACKAGE

Information furnished by Linear Technology Corporation is believed to be accurate and reliable. However, no responsibility is assumed for its use. Linear Technology Corporation makes no representation that the interconnection of its circuits as described herein will not infringe on existing patent rights.

## LT6559

## TYPICAL APPLICATION

DC1063A Demo Circuit Schematic


## reLATED PARTS

| PART NUMBER | DESCRIPTION | COMMENTS |
| :---: | :---: | :---: |
| LT1203/LT1205 | 150MHz Video Multiplexers | 2:1 and Dual 2:1 MUXs with 25ns Switch Time |
| LT1204 | 4-Input Video MUX with Current Feedback Amplifier | Cascadable Enable 64:1 Multiplexing |
| LT1395/LT1396/LT1397 | Single/Dual/Quad Current Feedback Amplifiers | 400 MHz Bandwidth, 0.1dB Flatness $>100 \mathrm{MHz}$ |
| LT1399 | 300MHz Triple Current Feedback Amplifier | 0.1 dB Gain Flatness to 150MHz, Shutdown |
| LT1675/LT1675-1 | Triple/Single 2:1 Buffered Video Mulitplexer | 2.5ns Switching Time, 250MHz Bandwidth |
| LT1806/LT1807 | Single/Dual 325MHz Rail-to-Rail In/Out Op Amp | Low Distortion, Low Noise |
| LT1809/LT1810 | Single/Dual 180MHz Rail-to-Rail In/Out Op Amp | Low Distortion, Low Noise |
| LT6550/LT6551 | 3.3V Triple and Quad Video Buffers | 110MHz Gain of 2 Buffers in MS Package |
| LT6553 | 650MHz Gain of 2 Triple Video Amplifier |  |
| LT6554 | 650 MHz Gain of 1 Triple Video Amplifier | Same Pinout as the LT6553 but Optimized for High Impedance Loads |
| LT6555 | 650MHz Gain of 2 Triple 2:1 Video Multiplexor |  |
| LT6556 | 750MHz Gain of 1 Triple 2:1 Video Multiplexor | Same Pinout as the LT6553 but Optimized for High Impedance Loads |
| LT6557 | 500 MHz Gain of 2 Single-Supply Triple Video Amplifier | Optimized for Single 5V Supply, 2200V/us Slew Rate, Input Bias Control |
| LT6558 | 550MHz Gain of 1 Single-Supply Triple Video Amplifier | Optimized for Single 5V Supply, 2200V/us Slew Rate, Input Bias Control |
|  |  | 6559f |
|  |  |  |

