

High Efficiency Inductorless Step-Down DC/DC Converters

FEATURES

- Input Voltage Range: 2.4V to 6V
- Fixed Output Voltages: 1.8V ±4%, 2V ±4%
- Output Current: Up to 100mA
- No Inductors
- Typical Efficiency 25% Higher than LDOs
- Low Operating Current: 25µA
- Low Shutdown Current: 5µA
- 600kHz Switching Frequency
- Shutdown Disconnects Load from V_{IN}
- Soft-Start Limits Inrush Current at Turn-On
- Short-Circuit and Overtemperature Protected
- Available in 8-Pin MSOP and SO Packages

APPLICATIONS

- Cellular Phones
- Handheld Computers
- Smart Card Readers
- Low Power DSP Supplies
- Portable Electronic Equipment
- Handheld Medical Instruments

DESCRIPTION

The LTC®1503-1.8/LTC1503-2 are switched capacitor step-down DC/DC converters that produce a regulated output from a 2.4V to 6V input. The parts use switched capacitor fractional conversion to achieve high efficiency over the entire input range. No inductors are required. Internal circuitry controls the step-down conversion ratio to optimize efficiency as the input voltage and load conditions vary. Typical efficiency is 25% higher than that of a low dropout (LDO) linear regulator.

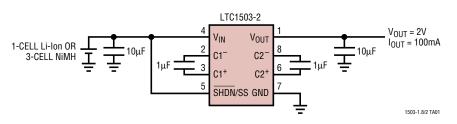
Regulation is achieved by sensing the output voltage and enabling the internal switching network as needed to maintain a fixed output voltage. This method of regulation enables the parts to achieve high efficiency at extremely light loads. Low operating current (25 μ A with no load, 5 μ A in shutdown) and low external parts count (two 1 μ F flying capacitors and two 10 μ F bypass capacitors) make the LTC1503-1.8/LTC1503-2 ideally suited for space constrained battery-powered applications. The parts are fully short-circuit and overtemperature protected.

The LTC1503-1.8/LTC1503-2 are available in 8-pin MSOP and SO packages.

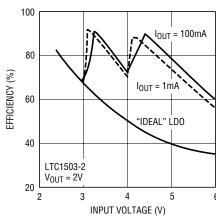
17, LTC and LT are registered trademarks of Linear Technology Corporation.

TYPICAL APPLICATION

Single Li-Ion to 2V DC/DC Converter



Efficiency vs Input Voltage



503-1.8/2 TA02

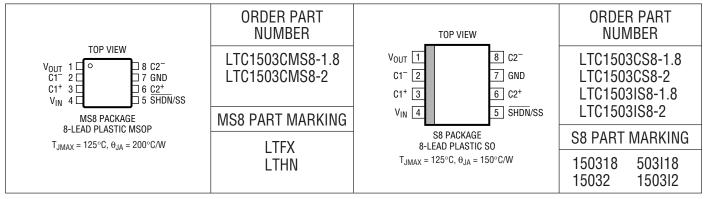


ABSOLUTE MAXIMUM RATINGS (Note 1)

V_{IN} , C1+, C1-, C2+, C2- to GND	0.3V to 6.5V
SHDN/SS to GND	$-0.3V$ to $(V_{IN} + 0.3V)$
V _{OUT} Short-Circuit Duration	Indefinite
Commercial Temperature Range.	40°C to 85°C

Industrial Temperature Range40°C to	$85^{\circ}C$
Specified Temperature Range (Note 2)40°C to	$85^{\circ}C$
Storage Temperature Range65°C to 1	$50^{\circ}C$
Lead Temperature (Soldering, 10 sec) 3	800°C

PACKAGE/ORDER INFORMATION



Consult factory for Military grade parts.

ELECTRICAL CHARACTERISTICS

The ullet denotes specifications which apply over the full operating temperature range, otherwise specifications are at $T_A = 25^{\circ}C$. $V_{IN} = V_{IN(MIN)}$ to $V_{IN(MAX)}$, $C1 = C2 = 1\mu F$, $C_{IN} = C_{OUT} = 10\mu F$ unless otherwise noted.

PARAMETER	CONDITIONS		MIN	TYP	MAX	UNITS
V _{IN} Operating Voltage		•	2.4		6	V
V _{OUT}	LTC1503-1.8, 0mA < I _{OUT} < 100mA LTC1503-2, 0mA < I _{OUT} < 100mA	•	1.728 1.920	1.8 2.0	1.872 2.080	V
V _{IN} Operating Current	I _{OUT} = 0mA	•		25	50	μΑ
V _{IN} Shutdown Current	SHDN/SS = 0V	•		5	10	μΑ
Output Ripple Voltage	LTC1503-X, V _{IN} = 3.6V, I _{OUT} = 100mA			25		mV _{P-P}
Efficiency	LTC1503-2, V _{IN} = 3.6V, I _{OUT} = 100mA			82.9		%
Switching Frequency	Oscillator Free Running			600		kHz
SHDN/SS Input Threshold		•	0.2	0.35	0.5	V
SHDN/SS Input Current	V _{SHDN/SS} = 0V (Note 3) V _{SHDN/SS} = V _{IN}	•	-3.5 -1	-2	-1 1	μA μA
V _{OUT} Short-Circuit Current	V _{OUT} = 0V (Note 4)	•	8	22	50	mA
V _{OUT} Turn-On Time	C_{SS} = 0nF, V_{IN} = 3.6V, C_{OUT} = 10 μ F C_{SS} = 10nF			0.1 8		ms ms

Note 1: Absolute Maximum Ratings are those values beyond which the life of a device may be impaired.

Note 2: The LTC1503C is guaranteed to meet specified performance from 0° C to 70° C and is designed, characterized and expected to meet these extended temperature limits, but are not tested at -40° C and 85° C. The LTC1503I is guaranteed to meet the extended temperature limits.

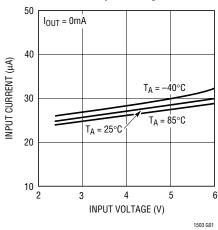
Note 3: Currents flowing into the device are positive polarity. Currents flowing out of the device are negative polarity.

Note 4: When V_{OUT} is less than 150mV, I_{OUT} is limited to much less than the maximum rated output current to prevent damage to the output devices.

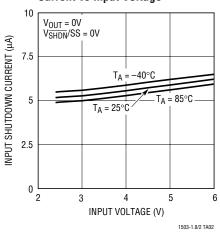


TYPICAL PERFORMANCE CHARACTERISTICS

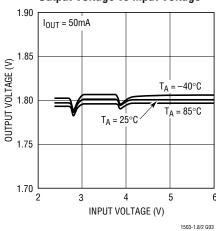




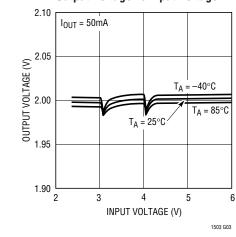
LTC1503-X Input Shutdown Current vs Input Voltage



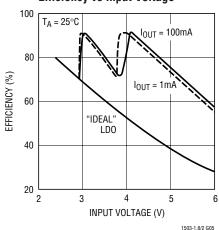
LTC1503-1.8 Output Voltage vs Input Voltage



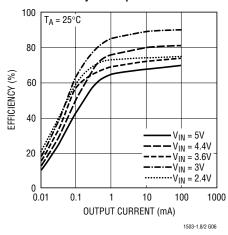
LTC1503-2 Output Voltage vs Input Voltage



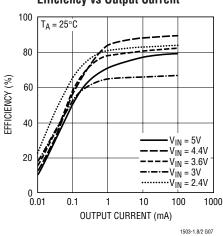
LTC1503-1.8 Efficiency vs Input Voltage



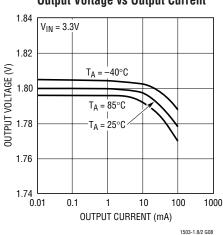
LTC1503-1.8 Efficiency vs Output Current



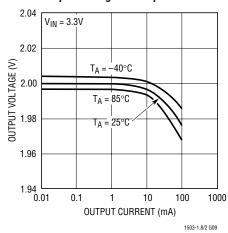
LTC1503-2 Efficiency vs Output Current



LTC1503-1.8 Output Voltage vs Output Current

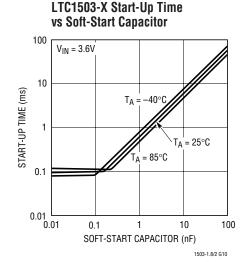


LTC1503-2 Output Voltage vs Output Current



TYPICAL PERFORMANCE CHARACTERISTICS

LTC1503-X Output Short-Circuit **Current vs Input Voltage** V_{OUT} SHORTED TO GND 30 OUTPUT CURRENT (mA) = -40°C 20 $T_A = 25^{\circ}C$ T_A = 85°C 10 0 3 5 2 INPUT VOLTAGE (V) 1503-1.8/2 G10

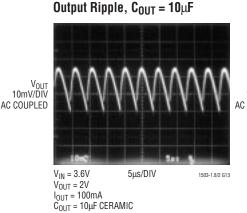


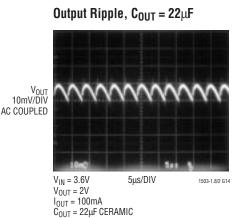
(LTC1503-1.8,1mA to 100mA Step)

100mA
100mA
50mA/DIV
1mA
Vout
50mV/DIV
AC COUPLED

1ms/DIV
1503-1.82 612

Output Load Transient Response





PIN FUNCTIONS

 V_{OUT} (Pin 1): Regulated Output Voltage. V_{OUT} is disconnected from V_{IN} during shutdown. Bypass V_{OUT} to ground with $a \ge 10 \mu F$ low ESR capacitor.

C1⁻ (Pin 2): Flying Capacitor One Negative Terminal.

C1+ (Pin 3): Flying Capacitor One Positive Terminal.

 V_{IN} (Pin 4): Input Voltage. V_{IN} may be between 2.4V and 6V. Bypass V_{IN} to ground with a \geq 10 μ F low ESR capacitor.

SHDN/SS (Pin 5): Shutdown/Soft-Start Control. The pin is designed to be driven with an external open-drain

output. Holding the SHDN/SS pin below 0.25V will force the part into shutdown mode. An internal pull-up current of $2\mu A$ will force the SHDN/SS voltage to climb to V_{IN} once the device driving the pin is forced into a Hi-Z state. To limit inrush current on start-up, connect a capacitor between the \overline{SHDN}/SS pin and ground. Capacitance on the \overline{SHDN}/SS pin will limit the dV/dt of the pin during turn-on which, in turn, will limit the dV/dt of V_{OUT} . By selecting an appropriate soft-start capacitor for a known output capacitor, the user can control the inrush current during

PIN FUNCTIONS

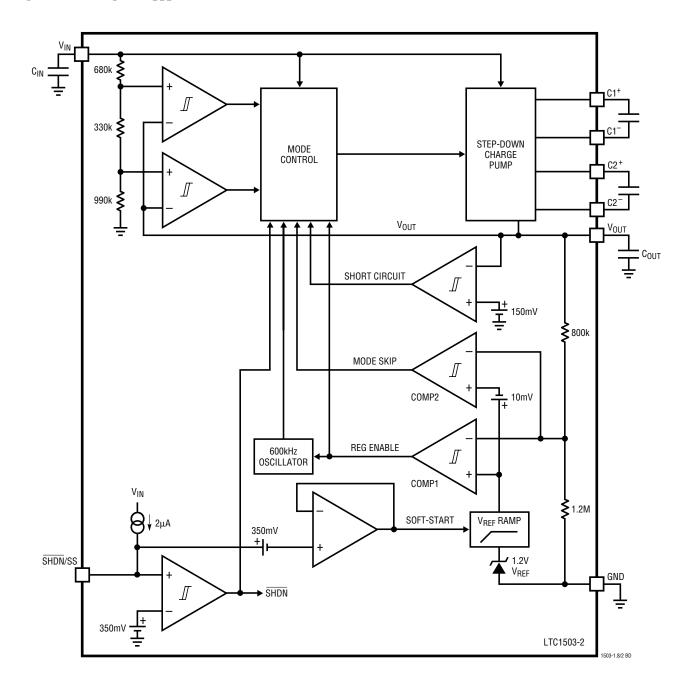
turn-on (see Applications Information). If neither of the two functions are desired, the pin may be floated or tied to $V_{\text{IN}}.$

C2+ (Pin 6): Flying Capacitor Two Positive Terminal.

GND (Pin 7): Ground. Connect to a ground plane for best performance.

C2⁻ (**Pin 8**): Flying Capacitor Two Negative Terminal.

BLOCK DIAGRAM



General Operation

The two most common methods for providing regulated step-down DC/DC conversion are linear DC/DC conversion (used by LDOs) and inductor-based DC/DC conversion. Linear regulation provides low cost and low complexity, but the conversion efficiency is poor since all of the load current must come directly from V_{IN} . Inductor-based step-down conversion provides the highest efficiency, but the solution cost and circuit complexity are much higher. The LTC1503-X provides the efficiency advantages associated with inductor-based circuits as well as the cost and simplicity advantages of an inductorless converter.

The LTC1503-X is a switched capacitor step-down DC/DC converter. The part uses an internal switch network and fractional conversion ratios to achieve high efficiency over widely varying V_{IN} and output load conditions. Internal control circuitry selects the appropriate step-down conversion ratio based on V_{IN}, V_{OUT} and load conditions to optimize efficiency. The part has three possible step-down modes: 2-to-1, 3-to-2 or 1-to-1 (gated switch) step-down mode. Only two external flying caps are needed to operate in all three modes. 2-to-1 mode is chosen when V_{IN} is greater than two times the desired V_{OUT}. 3-to-2 mode is chosen when V_{IN} is greater than 1.5 times V_{OUT} but less than 2 times V_{OUT} . 1-to-1 mode is chosen when V_{IN} falls below 1.5 times V_{OUT}. An internal mode skip function will switch the step-down ratio as needed to maintain output regulation under heavy load conditions.

Regulation is achieved by sensing the divided down output voltage and enabling the charge pump as needed to boost the output back into regulation. This method of regulation allows the LTC1503-X to achieve high efficiency at very light loads. The part has shutdown capability as well as user controlled inrush current limiting. In addition, the part can withstand an indefinite short-circuit condition on V_{OLIT} and is also overtemperature protected.

Step-Down Charge Pump Operation

Figure 1a shows the charge pump switch configuration that is used for 2-to-1 step down. When the charge pump is enabled in this mode, a two phase nonoverlapping clock generates the switch control signals. On phase one of the clock, flying capacitor C1 is connected through switches

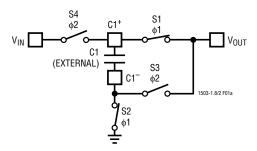


Figure 1a. Step-Down Charge Pump in 2-to-1 Mode

S1 and S2 across V_{OUT} . If the voltage on C1 is greater than the voltage on C_{OUT} , charge is transferred from C1 onto C_{OUT} . On phase two, the top plate of C1 is connected to V_{IN} and the bottom plate is connected to V_{OUT} . If the voltage across C1 is less than $V_{IN}/2$ during phase two, charge will be transferred from C1 onto C_{OUT} thereby boosting the voltage on C_{OUT} and raising the voltage across C1. Thus, in 2-to-1 mode, charge transfer from C1 onto C_{OUT} occurs on both phases of the clock, and the voltage on C_{OUT} is driven towards $1/2V_{IN}$ until the output is back in regulation. Since charge current is sourced from ground on phase one of the clock, current multiplication is realized with respect to V_{IN} , i.e., I_{VOUT} equals approximately 2 • I_{VIN} . This results in significant efficiency improvement relative to a linear regulator.

The 3-to-2 conversion mode also uses a nonoverlapping clock for switch control but requires two flying capacitors and a total of seven switches (see Figure 1b). On phase one, C1 and C2 are connected in series across V_{OLIT} . If the sum of the voltages across C1 and C2 is greater than V_{OUT} , charge is transferred from the flying caps onto C_{OUT} thereby reducing the average voltage on the flying caps and raising the voltage on the output capacitor. On phase two, the two flying capacitors are connected on parallel between V_{IN} and V_{OLIT}. Since the average voltage across the two capacitors during phase one is $V_{OUT}/2$, charge will be transferred from V_{IN} to V_{OUT} through the two flying caps if V_{IN} minus $V_{\text{OUT}}/2$ is greater than V_{OUT} . In this manner, charge is again transferred from the flying caps to the output on both phases of the clock, and the voltage on C_{OLIT} is driven towards (2/3) V_{IN} until the part is back in regulation. As in 2-to-1 mode, charge current is sourced from ground on phase one of the clock which results in increased power efficiency. IVOLIT in 3-to-2 mode equals approximately (3/2)I_{VIN}.



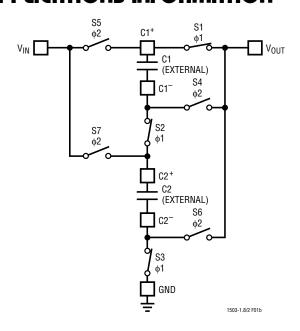


Figure 1b. Step-Down Charge Pump in 3-to-2 Mode

In 1-to-1 mode, switch S1 and S2 are connected in series between V_{IN} and V_{OUT} as needed to boost V_{OUT} back into regulation (see Figure 1c). The REG ENABLE signal from the main comparator (COMP1) controls switches S1 and S2 directly. Since all of the V_{OUT} current is sourced from V_{IN} , the efficiency in 1-to-1 mode is approximately equal to that of a linear regulator.

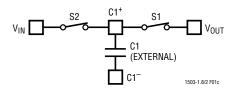


Figure 1c. Step-Down Charge Pump in 1-to-1 Mode

Mode Selection and Mode Skipping

The optimal step-down conversion mode is chosen based on V_{IN} to V_{OUT} differential voltage and output load conditions. Two internal comparators are used to select the default step-down mode based on the V_{IN} and V_{OUT} voltage. A separate comparator (COMP2) is used to sense a droop on V_{OUT} due to a heavy output load and force the charge pump to skip to a higher output current mode to

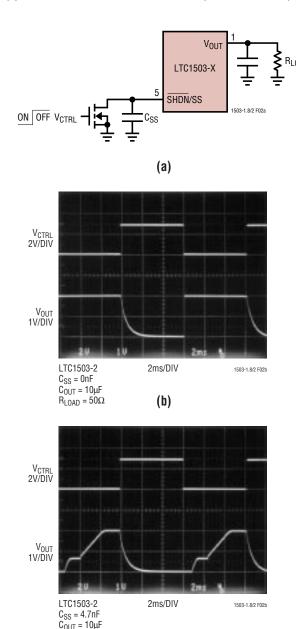
maintain regulation. This will only occur as V_{IN}/V_{OUT} nears a 3-to-2 or 1-to-1 transition point. For example, under light load conditions, the LTC1503-X can operate in 2-to-1 mode when V_{IN} equals 4.1V with greater than 90% efficiency. However, when the load is increased, the part can no longer supply enough output current in 2-to-1 mode to maintain regulation. This causes V_{OUT} to droop below the regulation point until COMP2 trips and forces the part to skip from 2-to-1 mode to 3-to-2 mode. The COMP2 threshold is about 17mV (V_{OUT} referred) below the main comparator regulation point. Hysteresis in COMP2 will force the part to transition in and out of mode skipping. This will result in a slight V_{OUT} decrease of approximately 20mV under mode skipping conditions.

Shutdown/Soft-Start Operation

The SHDN/SS pin is used to implement both low current shutdown and soft-start. The soft-start feature limits inrush currents when the regulator is initially powered up or taken out of shutdown. Forcing a voltage lower than 0.35V (typ) will put the part into shutdown mode. Shutdown mode disables all control circuitry and forces the charge pump V_{OUT} into a high impedance state. A $2\mu A$ pullup current on the \overline{SHDN}/SS pin will force the part into active mode if the pin is left floating or is driven with an open-drain output that is in a high impedance state. If the pin is not driven with an open-drain device, it must be forced to a logic high voltage of 2.2V (min) to ensure proper V_{OUT} regulation. The \overline{SHDN}/SS pin should not be driven to a voltage higher than V_{IN} .

To implement soft-start, the SHDN/SS pin must be driven with an open-drain device and a capacitor must be connected from the SHDN/SS pin to GND. Once the open-drain device is turned off, a $2\mu A$ pull-up current will begin charging the external SS capacitor and force the voltage on the pin to ramp towards $V_{IN}.$ As soon as the SHDN threshold is reached (0.35V typ), the internal reference voltage which controls the V_{OUT} regulation point will follow the ramp voltage on the SHDN/SS pin (minus a 0.35V offset to account for the SHDN threshold) until the reference reaches its final band gap voltage. This occurs when the voltage on the SHDN/SS pin reaches

approximately 1.9V. Since the ramp rate on the SHDN/SS pin controls the ramp rate on V_{OUT} , the average inrush current can be controlled through selection of C_{SS} and C_{OUT} . For example, a 4.7nF capacitor on SHDN/SS results in a 4ms ramp time from 0.35V to 1.9V on the pin. If C_{OUT} is $10\mu F$, the 4ms V_{REF} ramp time results in an average C_{OUT} charge current of only 5mA (see Figure 2c).



(c)
Figure 2. Shutdown/Soft-Start Operation

 $R_{LOAD} = 50\Omega$

Capacitor Selection

For best performance, it is recommended that low ESR capacitors be used for C_{IN} and C_{OUT} to reduce noise and ripple. If the ESR of the output capacitor is too high (>0.5 Ω), both efficiency and output load regulation may be degraded. The C_{IN} and C_{OUT} capacitors should be either ceramic or tantalum and should be $10\mu F$ or greater. If the input source impedance is very low (<0.5 Ω), C_{IN} may not be needed. Ceramic capacitors are recommended for the flying caps C1 and C2 with values of $0.47\mu F$ to $2.2\mu F$. Smaller values may be used in low output current applications (e.g., I_{OUT} < 10mA). For best performance choose the same capacitance value for both C1 and C2.

Output Ripple

Normal LTC1503-X operation produces voltage ripple on the V_{OUT} pin. Output voltage ripple is required for the parts to regulate. Low frequency ripple exists due to the hysteresis in the sense comparator and propagation delays in the charge pump enable/disable circuits. High frequency ripple is also present mainly from the ESR (equivalent series resistance) in the output capacitor. Typical output ripple ($V_{IN} = 3.6V$) under maximum load is 25mV peak-to-peak with a low ESR $10\mu F$ output capacitor.

The magnitude of ripple voltage depends on several factors. High input voltages increase the output ripple since more charge is delivered to C_{OUT} per charging cycle. Large output current load and/or a small output capacitor (< $10\mu F$) results in higher ripple due to higher output voltage dV/dt. High ESR capacitors (ESR > 0.5Ω) on the output pin cause high frequency voltage spikes on V_{OUT} with every clock cycle.

There are several ways to reduce the output voltage ripple (see Figure 3). A larger C_{OUT} capacitor ($22\mu F$ or greater) will reduce both the low and high frequency ripple due to the lower C_{OUT} charging and discharging dV/dt and the lower ESR typically found with higher value (larger case size) capacitors. A low ESR ceramic output capacitor will minimize the high frequency ripple, but will not reduce the low frequency ripple unless a high capacitance value is chosen. A reasonable compromise is to use a $10\mu F$ to $22\mu F$ tantalum capacitor in parallel with a $1\mu F$ to $3.3\mu F$ ceramic

capacitor on V_{OUT} to reduce both the low and high frequency ripple. An RC filter may also be used to reduce high frequency voltage spikes.

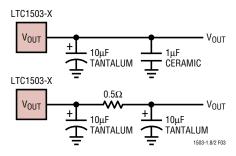


Figure 3. Output Ripple Reduction Techniques

Protection Features

The LTC1503-X contains both thermal shutdown and short-circuit protection features. The charge pump will shut down when the junction temperature reaches approximately 150°C and will resume operation once the junction temperature has dropped back to 125°C. The part will limit output current to 20mA (typ) when a short-circuit condition (V_{OUT} < 150mV) exists to prevent damage to the internal switches. During start-up, the 20mA current limit

is disabled once V_{OUT} reaches 0.7V (typ). The part can survive an indefinite short from V_{OUT} to GND.

Layout Considerations

For best regulation and noise performance, careful board layout is required. Improper bypassing and grounding may lead to poor load regulation and output ripple performance. All capacitors, especially C_{IN} and C_{OUT} , must be as close as possible to the V_{IN} and V_{OUT} pins. Connecting the GND pin and all bypass capacitors to an uninterrupted ground plane is also advised. See Figure 4 for recommended component placement and grounding.

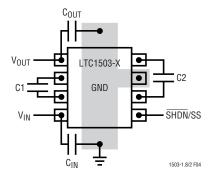
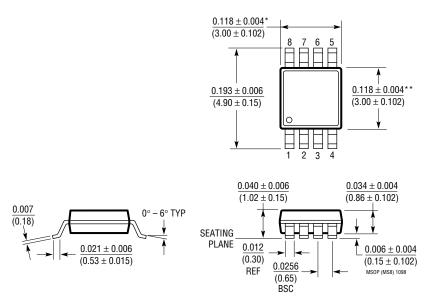


Figure 4. Recommended Component Placement and Grounding

PACKAGE DESCRIPTION Dimensions in inches (millimeters) unless otherwise noted.

MS8 Package 8-Lead Plastic MSOP

(LTC DWG # 05-08-1660)



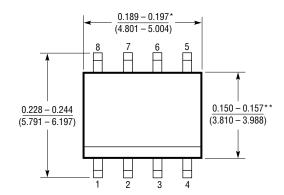
- * DIMENSION DOES NOT INCLUDE MOLD FLASH, PROTRUSIONS OR GATE BURRS. MOLD FLASH, PROTRUSIONS OR GATE BURRS SHALL NOT EXCEED 0.006" (0.152mm) PER SIDE
- ** DIMENSION DOES NOT INCLUDE INTERLEAD FLASH OR PROTRUSIONS. INTERLEAD FLASH OR PROTRUSIONS SHALL NOT EXCEED 0.006" (0.152mm) PER SIDE

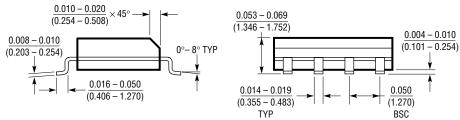
PACKAGE DESCRIPTION

Dimensions in inches (millimeters) unless otherwise noted.

S8 Package 8-Lead Plastic Small Outline (Narrow 0.150)

(LTC DWG # 05-08-1610)



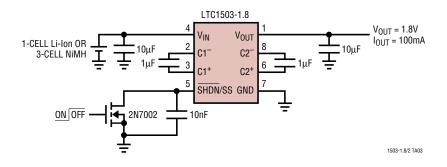


- *DIMENSION DOES NOT INCLUDE MOLD FLASH. MOLD FLASH SHALL NOT EXCEED 0.006" (0.152mm) PER SIDE
- **DIMENSION DOES NOT INCLUDE INTERLEAD FLASH. INTERLEAD FLASH SHALL NOT EXCEED 0.010" (0.254mm) PER SIDE

S08 1298

TYPICAL APPLICATION

DC/DC Converter with Shutdown and Soft-Start



RELATED PARTS

PART NUMBER	DESCRIPTION	COMMENTS
LTC1474/LTC1475	Low Quiescent Current Step-Down DC/DC Converter	I _{OUT} to 250mA, I _Q = 10μA; 8-Lead MSOP
LTC1502-3.3	Single Cell to 3.3V Quadrupler Charge Pump	$V_{IN} = 0.9V \text{ to } 1.8V, I_{OUT} = 10\text{mA}; I_{Q} = 40\mu\text{A}$
LTC1514/LTC1515	Micropower, Regulated 5V Step-Up/Step-Down Charge Pump DC/DC Converters	2V to 10V Input Range; Up to 50mA Output Current: Short-Circuit and Overtemperature Protected
LTC1555/LTC1556	SIM Power Supply and Level Translator	Step-Up/Step-Down Charge Pump Generates 5V or 3V
LTC1627	Monolithic Synchronous Buck Step-Down Switching Regulator	2.65V to 8.5V Input Range; V _{OUT} from 0.8V, I _{OUT} to 500mA; Low Dropout Operation; 100% Duty Cycle
LTC1754-3.3	3.3V Charge Pump with Shutdown in SOT-23	50mA Output Current, I _{CC} = 13μA
LTC1754-5	5V Charge Pump with Shutdown in SOT-23	50mA Output Current, I _{CC} = 13μA