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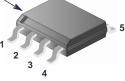
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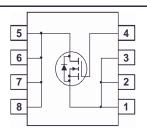
FAIRCHILD SEMICONDUCTOR® FDS3682	September 2002	FDS3682
N-Channel PowerTrench [®] MOSFET 100V, 6A, 35m Ω		
Features	Applications	
• $r_{DS(ON)} = 30m\Omega$ (Typ.), $V_{GS} = 10V$, $I_D = 6A$	DC/DC converters and Off-Line UPS	
• Q _g (tot) = 19nC (Typ.), V _{GS} = 10V	Distributed Power Architectures and VRMs	
Low Miller Charge	 Primary Switch for 24V and 48V Systems 	
 Low Q_{RR} Body Diode Optimized efficiency at high frequencies 	High Voltage Synchronous Rectifier	

- UIS Capability (Single Pulse and Repetitive Pulse)
- Direct Injection / Diesel Injection Systems
- 42V Automotive Load Control
- Electronic Valve Train Systems



Formerly developmental type 82755





SO-8 MOSFET Maximum Ratings $T_A = 25^{\circ}C$ unless otherwise noted

Symbol	Parameter	Ratings	Units	
V _{DSS}	Drain to Source Voltage	100	V	
V _{GS}	Gate to Source Voltage	±20	V	
	Drain Current			
	Continuous (T _A = 25 ^o C, V _{GS} = 10V, R _{θJA} = 50 ^o C/W)	6.0	А	
I _D	Continuous (T _A = 100°C, V _{GS} = 10V, R _{θJA} = 50°C/W)	3.7	A	
	Pulsed	Figure 4	A	
E _{AS}	Single Pulse Avalanche Energy (Note 1)	156	mJ	
D	Power dissipation	2.5	W	
P _D	Derate above 25°C	20	mW/ºC	
T _J , T _{STG}	Operating and Storage Temperature	-55 to 150	°C	

Thermal Characteristics

R_{\thetaJA}	Thermal Resistance, Junction to Ambient at 10 seconds (Note 3)	50	°C/W
R_{\thetaJA}	Thermal Resistance, Junction to Ambient at 1000 seconds (Note 3)	80	°C/W
$R_{ extsf{ heta}JC}$	Thermal Resistance, Junction to Case (Note 2)	25	°C/W

Package Marking and Ordering Information

Device Marking	Device	Package	Reel Size	Tape Width	Quantity
FDS3682	FDS3682	SO-8	330mm	12mm	2500 units

Symbol	Parameter	Test Cond	itions	Min	Тур	Max	Units
Off Chara	cteristics						
B _{VDSS}	Drain to Source Breakdown Voltage	I _D = 250μA, V _{GS} :	= 0V	100	-	-	V
		V _{DS} = 80V		-	-	1	•
I _{DSS}	Zero Gate Voltage Drain Current	$V_{GS} = 0V$	$T_{C} = 150^{\circ}C$	-	-	250	μA
I _{GSS}	Gate to Source Leakage Current	$V_{GS} = \pm 20V$		-	-	±100	nA
On Chara	cteristics	·	· · · · ·				
V _{GS(TH)}	Gate to Source Threshold Voltage	$V_{GS} = V_{DS}, I_D = 2$	250μΑ	2	-	4	V
. ,	Drain to Source On Resistance	I _D = 6A, V _{GS} = 10		-	0.030	0.035	
r		$I_{D} = 3A, V_{GS} = 6V$		-	0.038	0.057	Ω
rds(ON)		$I_D = 6A, V_{GS} = 1$ $T_C = 150^{\circ}C$	0V,	-	0.060	0.070	22
Dynamic	Characteristics						
C _{ISS}	Input Capacitance		o) /	-	1300	-	pF
C _{OSS}	Output Capacitance	── V _{DS} = 25V, V _{GS} = ── f = 1MHz	= 0V,	-	190	-	pF
C _{RSS}	Reverse Transfer Capacitance	1 = 1101112		-	45	-	pF
Q _{g(TOT)}	Total Gate Charge at 10V	$V_{GS} = 0V$ to 10V		-	19	25	nC
Q _{g(TH)}	Threshold Gate Charge	$V_{GS} = 0V$ to 2V	V _{DD} = 50V	-	2.4	3.2	nC
Q _{gs}	Gate to Source Gate Charge		I _D = 6A	-	6.0	-	nC
Q _{gs2}	Gate Charge Threshold to Plateau		I _g = 1.0mA		3.6	-	nC
Q _{gd}	Gate to Drain "Miller" Charge			-	4.5	-	nC
	Switching Characteristics (V _G	_S = 10V)					
t _{ON}	Turn-On Time			-	-	71	ns
t _{d(ON)}	Turn-On Delay Time			-	12	-	ns
t _r	Rise Time	V _{DD} = 50V, I _D = 6A		-	35	_	ns

	_					
t _{ON}	Turn-On Time		-	-	71	ns
t _{d(ON)}	Turn-On Delay Time		-	12	-	ns
t _r	Rise Time	$V_{DD} = 50V, I_{D} = 6A$	-	35	-	ns
t _{d(OFF)}	Turn-Off Delay Time	$V_{GS} = 10V, R_{GS} = 16\Omega$	-	34	-	ns
t _f	Fall Time		-	37	-	ns
t _{OFF}	Turn-Off Time		-	-	107	ns

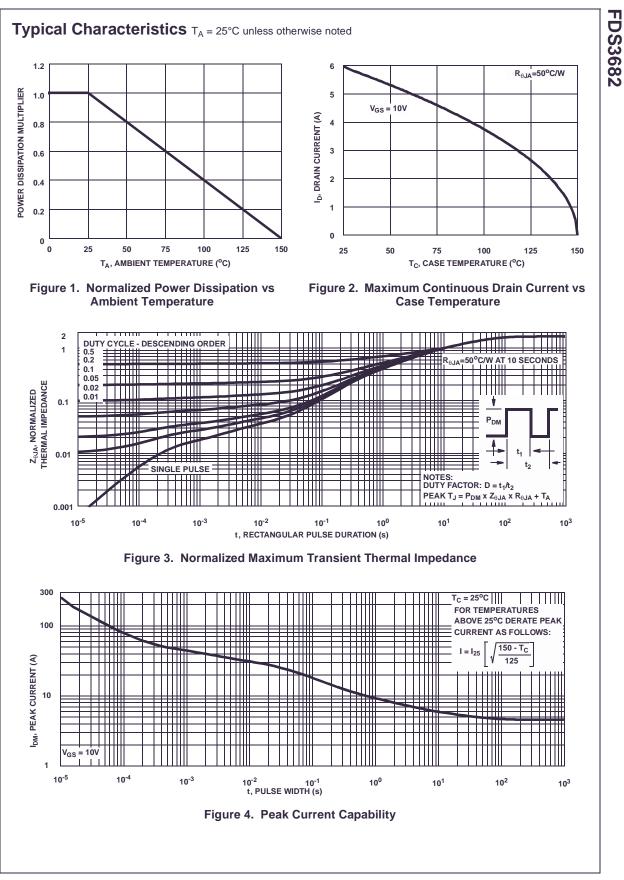
Drain-Source Diode Characteristics

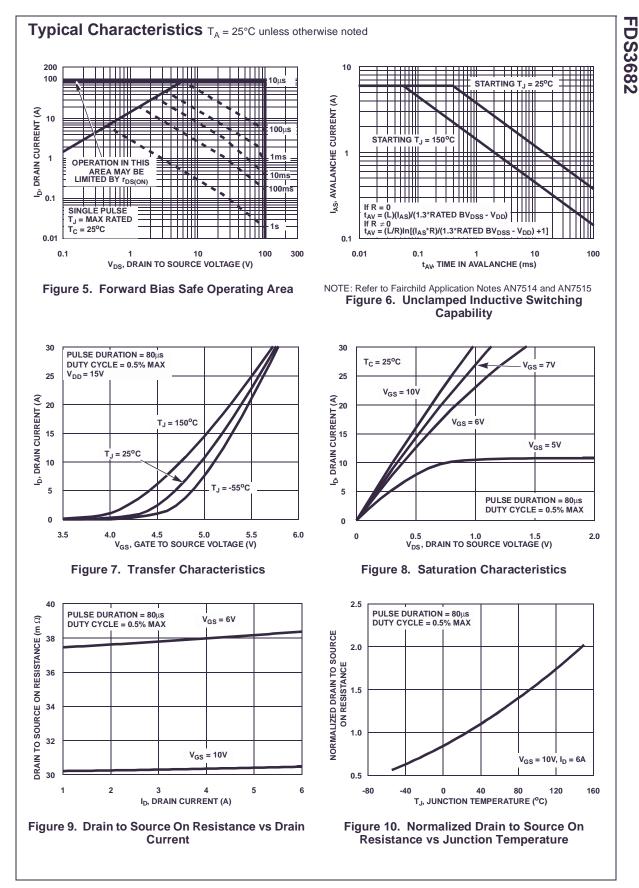
V _{SD}	Source to Drain Diode Voltage	$I_{SD} = 6A$	-	-	1.25	V
		I _{SD} = 3A	-	-	1.0	V
t _{rr}	Reverse Recovery Time	$I_{SD} = 6A$, $dI_{SD}/dt = 100A/\mu s$	-	-	50	ns
Q _{RR}	Reverse Recovered Charge	$I_{SD} = 6A$, $dI_{SD}/dt = 100A/\mu s$	-	-	75	nC

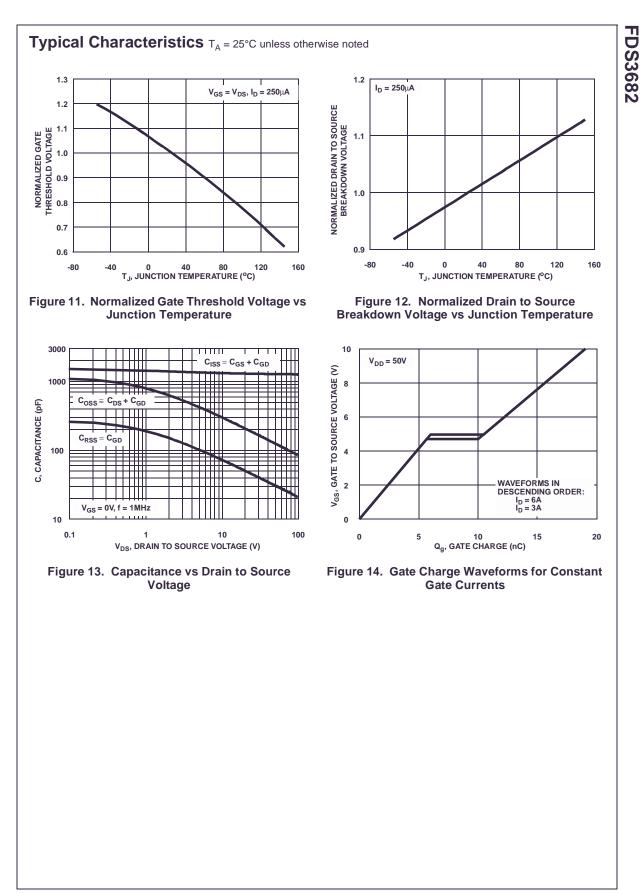
Notes:
1: Starting T_J = 25°C, L = 8.7mH, I_{AS} = 6A.
2: R_{θJA} is the sum of the junction-to-case and case-to-ambient thermal resistance where the case thermal referance is defined as the solder mounting surface of the drain pins. R_{θJC} is guaranteed by design while R_{θCA} is determined by the user's board design.

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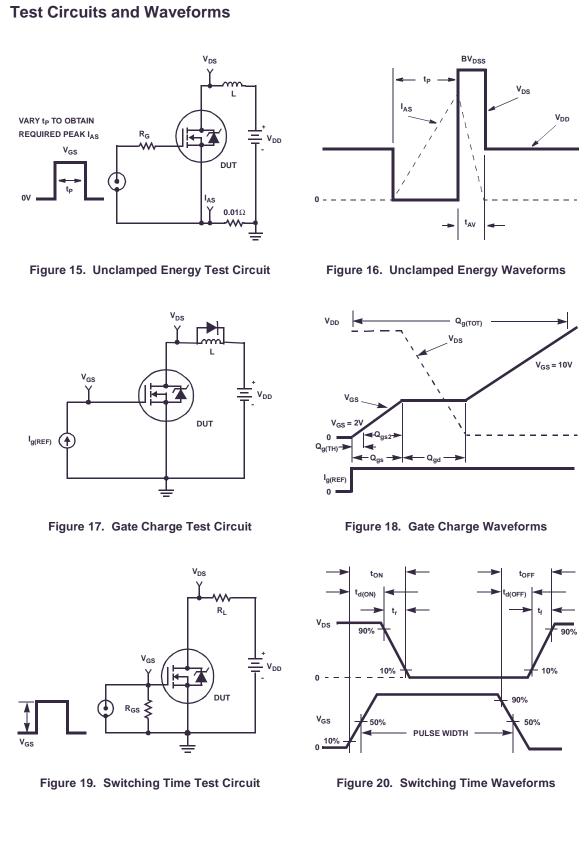
FDS3682











Thermal Resistance vs. Mounting Pad Area

The maximum rated junction temperature, T_{JM} , and the thermal resistance of the heat dissipating path determines the maximum allowable device power dissipation, P_{DM} , in an application. Therefore the application's ambient temperature, T_A (°C), and thermal resistance $R_{\theta JA}$ (°C/W) must be reviewed to ensure that T_{JM} is never exceeded. Equation 1 mathematically represents the relationship and serves as the basis for establishing the rating of the part.

$$P_{DM} = \frac{(T_{JM} - T_A)}{R_{\theta JA}}$$
(EQ. 1)

In using surface mount devices such as the SO8 package, the environment in which it is applied will have a significant influence on the part's current and maximum power dissipation ratings. Precise determination of P_{DM} is complex and influenced by many factors:

- Mounting pad area onto which the device is attached and whether there is copper on one side or both sides of the board.
- 2. The number of copper layers and the thickness of the board.
- 3. The use of external heat sinks.
- 4. The use of thermal vias.
- 5. Air flow and board orientation.
- 6. For non steady state applications, the pulse width, the duty cycle and the transient thermal response of the part, the board and the environment they are in.

Fairchild provides thermal information to assist the designer's preliminary application evaluation. Figure 21 defines the $R_{\theta,JA}$ for the device as a function of the top copper (component side) area. This is for a horizontally positioned FR-4 board with 1oz copper after 1000 seconds of steady state power with no air flow. This graph provides the necessary information for calculation of the steady state junction temperature or power dissipation. Pulse applications can be evaluated using the Fairchild device Spice thermal model or manually utilizing the normalized

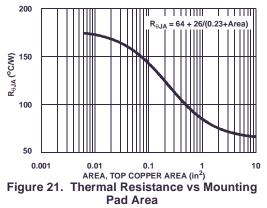
maximum transient thermal impedance curve.

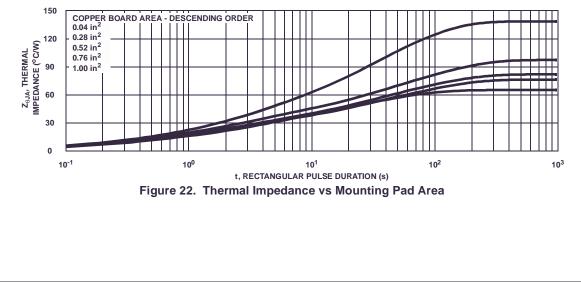
Thermal resistances corresponding to other copper areas can be obtained from Figure 21 or by calculation using Equation 2. The area, in square inches is the top copper area including the gate and source pads.

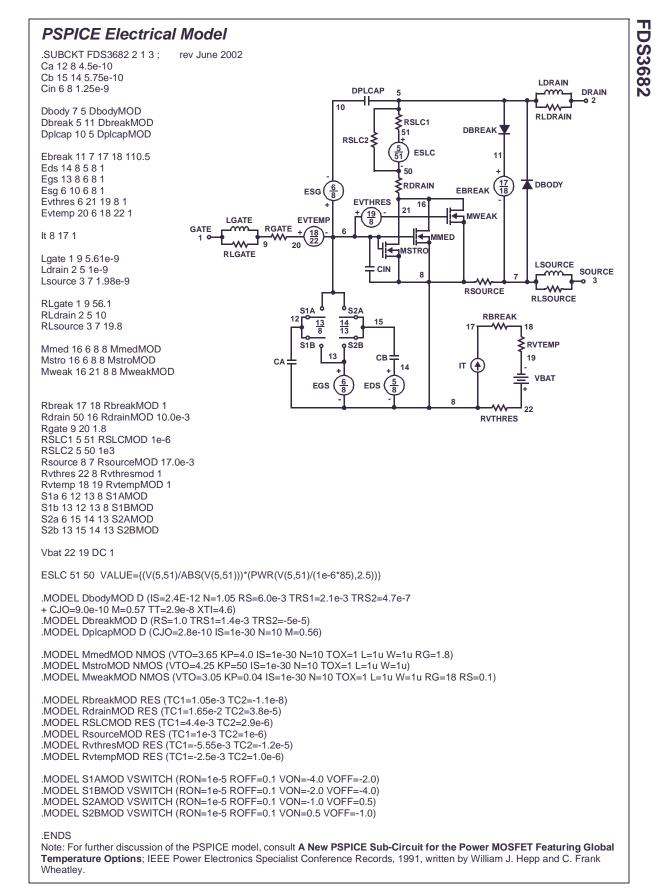
$$R_{\theta JA} = 64 + \frac{26}{0.23 + Area}$$
 (EQ. 2)

The transient thermal impedance $(Z_{\theta,JA})$ is also effected by varied top copper board area. Figure 22 shows the effect of copper pad area on single pulse transient thermal impedance. Each trace represents a copper pad area in square inches corresponding to the descending list in the graph. Spice and SABER thermal models are provided for each of the listed pad areas.

Copper pad area has no perceivable effect on transient thermal impedance for pulse widths less than 100ms. For pulse widths less than 100ms the transient thermal impedance is determined by the die and package. Therefore, CTHERM1 through CTHERM5 and RTHERM1 through RTHERM5 remain constant for each of the thermal models. A listing of the model component values is available in Table 1.







DS3682

LDRAIN

m

RI DRAIN

DBODY

LSOURCE

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RLSOURCE

18

19

22

₹RVTEMP

VBAT

DRAIN

SOURCE

3 o

02

DPLCAP

RSI C2

EVTHRES

<u>19</u> 8

10

<u>6</u> 8

ESG(

EVTEMP

<u>13</u> 8

S1B

<u>14</u> 13

6 EGS

o S2B 13

+  $\begin{pmatrix} 18\\ 22 \end{pmatrix}$ 

20

RGATE

CA

٩

5

ERSLC1

DBREAK

MWEAK

EBREAK

RSOURCE

17

IT

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11

RBREAK

RVTHRES

51

50

21

MSTRO

CIN

15

СВ

EDS 5 14

€RDRAIN

16

8

MMED

Ð ISCL

#### REV June 2002 template FDS3682 n2,n1,n3 electrical n2,n1,n3 var i iscl dp..model dbodymod = (isl=2.4e-12,nl=1.05,rs=6.0e-3,trs1=2.1e-3,trs2=4.7e-7,cjo=9.0e-10,m=0.57,tt=2.9e-8,xti=4.6) dp..model dbreakmod = (rs=1.0.trs1=1.4e-3.trs2=-5e-5)dp..model dplcapmod = (cjo=2.8e-10,isl=10e-30,nl=10,m=0.56) m..model mmedmod = (type=\_n,vto=3.65,kp=4.0,is=1e-30, tox=1) m..model mstrongmod = (type=\_n,vto=4.25,kp=50,is=1e-30, tox=1) m..model mweakmod = $(type=_n, vto=3.05, kp=0.04, is=1e-30, tox=1, rs=0.1)$ sw\_vcsp..model s1amod = (ron=1e-5,roff=0.1,von=-4.0,voff=-2.0) sw\_vcsp..model s1bmod = (ron=1e-5,roff=0.1,von=-2.0,voff=-4.0) sw\_vcsp..model s2amod = (ron=1e-5,roff=0.1,von=-1.0,voff=0.5)

sw\_vcsp..model s2bmod = (ron=1e-5,roff=0.1,von=0.5,voff=-1.0)

c.cin n6 n8 = 1.25e-9 dp.dbody n7 n5 = model=dbodymod dp.dbreak n5 n11 = model=dbreakmod dp.dplcap n10 n5 = model=dplcapmod spe.ebreak n11 n7 n17 n18 = 110.5 LGATE spe.eds n14 n8 n5 n8 = 1 GATE  $\sim$ spe.egs n13 n8 n6 n8 = 1 ~~~ spe.esg n6 n10 n6 n8 = 1 RLGATE spe.evthres n6 n21 n19 n8 = 1 spe.evtemp n20 n6 n18 n22 = 1

SABER Electrical Model

i.it n8 n17 = 1

l.lgate n1 n9 = 5.61e-9 I.Idrain n2 n5 = 1e-9l.lsource n3 n7 = 1.98e-9

c.ca n12 n8 = 4.5e-10

c.cb n15 n14 = 5.75e-10

res.rlgate n1 n9 = 56.1 res.rldrain n2 n5 = 10 res.rlsource n3 n7 = 19.8

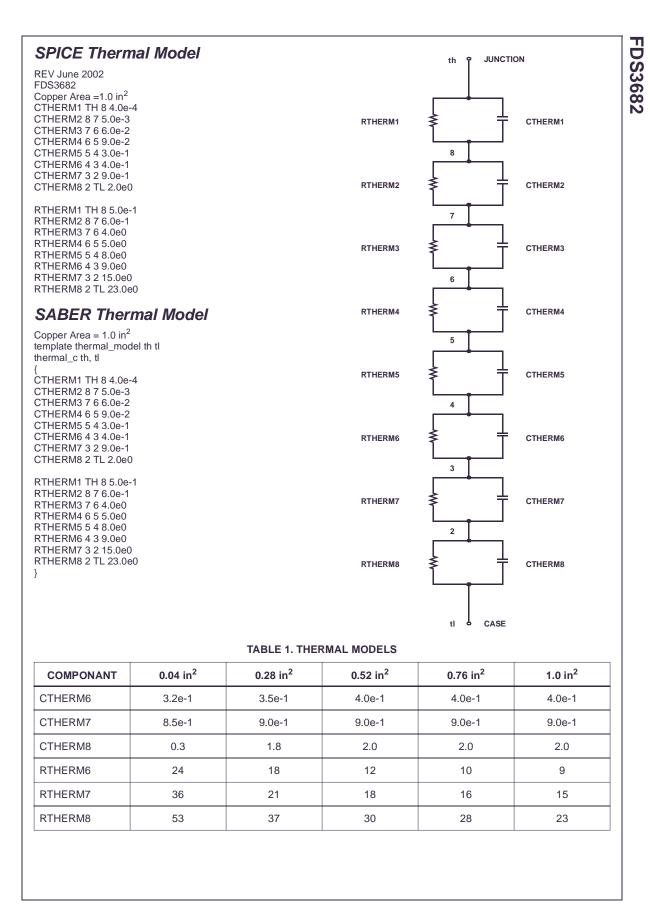
m.mmed n16 n6 n8 n8 = model=mmedmod, l=1u, w=1u m.mstrong n16 n6 n8 n8 = model=mstrongmod, l=1u, w=1u m.mweak n16 n21 n8 n8 = model=mweakmod, l=1u, w=1u

res.rbreak n17 n18 = 1, tc1=1.05e-3,tc2=-1.1e-8 res.rdrain n50 n16 = 10.0e-3, tc1=1.65e-2,tc2=3.8e-5 res.rgate n9 n20 = 1.8res.rslc1 n5 n51 = 1e-6, tc1=4.4e-3,tc2=2.9e-6 res.rslc2 n5 n50 = 1e3 res.rsource n8 n7 = 17.0e-3, tc1=1e-3,tc2=1e-6 res.rvthres n22 n8 = 1, tc1=-5.55e-3,tc2=-1.2e-5 res.rvtemp n18 n19 = 1. tc1=-2.5e-3.tc2=1.0e-6 sw\_vcsp.s1a n6 n12 n13 n8 = model=s1amod sw\_vcsp.s1b n13 n12 n13 n8 = model=s1bmod sw\_vcsp.s2a n6 n15 n14 n13 = model=s2amod sw\_vcsp.s2b n13 n15 n14 n13 = model=s2bmod

v.vbat n22 n19 = dc=1 equations { i (n51->n50) +=iscl iscl: v(n51,n50) = ((v(n5,n51)/(1e-9+abs(v(n5,n51))))\*((abs(v(n5,n51)\*1e6/85))\*\*2.5)))}

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