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January 2014

FAN103 Primary-Side-Regulation PWM Controller (PWM-PSR)

Features

- Low Standby Power Under 30 mW
- High Voltage Startup

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- Fewest External Component Counts
- Constant-Voltage (CV) and Constant-Current (CC) Control without Secondary-Feedback Circuitry
- Green-Mode Function: Linearly-Decreasing PWM Frequency
- Fixed PWM Frequency at 50 kHz with Frequency Hopping to Solve EMI Problem
- Cable Compensation in CV Mode
- Peak-Current-Mode Control in CV Mode
- Cycle-by-Cycle Current Limiting
- V_{DD} Over-Voltage Protection with Auto Restart
- V_{DD} Under-Voltage Lockout (UVLO)
- Gate Output Maximum Voltage Clamped at 15 V
- Fixed Over-Temperature Protection with Auto Restart
- Available in the 8-Lead SOP Package

Applications

- Battery chargers for cellular phones, cordless phones, PDA, digital cameras, power tools, etc.
- Replaces linear transformer and RCC SMPS

Description

This third-generation Primary-Side-Regulation (PSR) and highly integrated PWM controller provides several features to enhance the performance of low-power flyback converters. The proprietary topology, TRUECURRENT[®], of FAN103 enables precise CC regulation and simplified circuit for battery charger applications. A low-cost, smaller and lighter charger results as compared to a conventional design or a linear transformer.

To minimize standby power consumption, the proprietary green-mode function provides off-time modulation to linearly decrease PWM frequency under light-load conditions. This green mode assists the power supply in meeting the power conservation requirement.

By using the FAN103, a charger can be implemented with few external components and minimized cost. A typical output CV/CC characteristic envelope is shown in Figure 1.

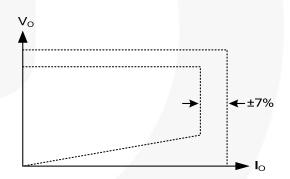


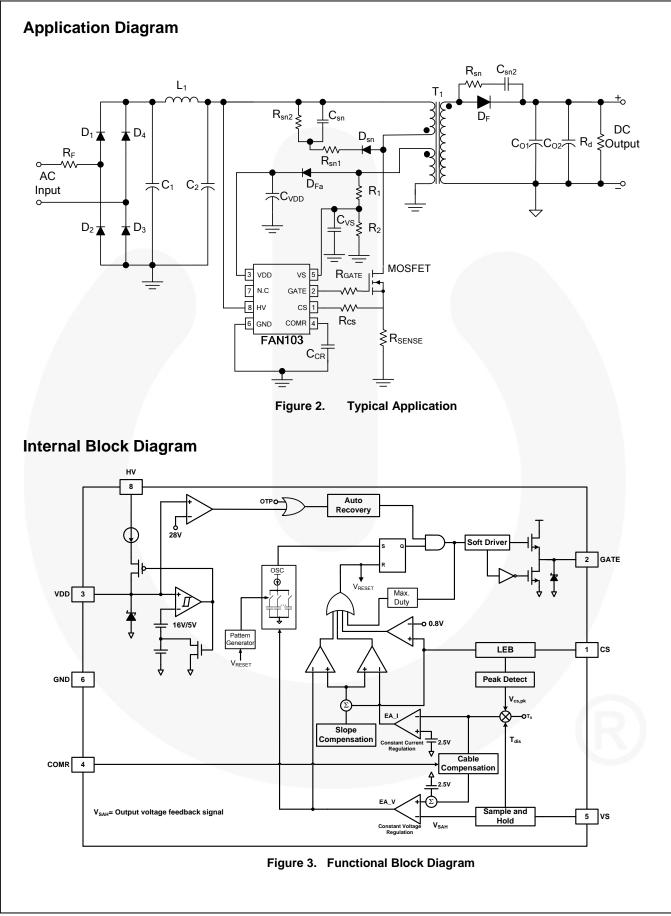
Figure 1. Typical Output V-I Characteristic

Ordering Information						
Part Number	Operating Temperature Range	Package	Packing Method			
FAN103MY	-40°C to +105°C	8-Lead, Small Outline Package (SOP-8)	Tape & Reel			

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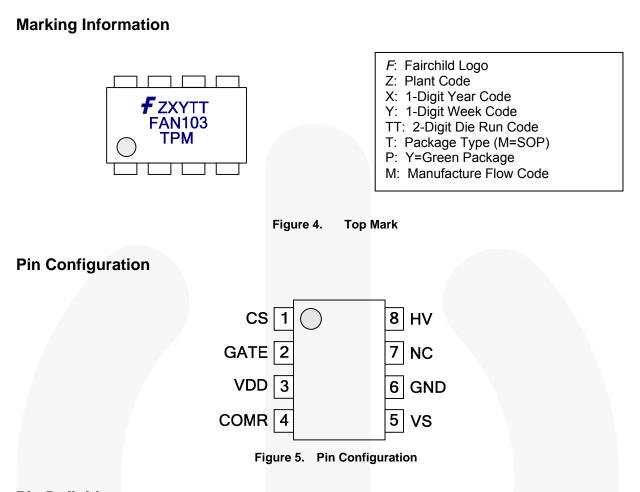
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Pin Definitions

Pin #	Name	Description			
1	CS	Current Sense . This pin connects a current sense resistor, to detect the MOSFET current for peak-current-mode control in CV mode, and provides the output-current regulation in CC mode.			
2	GATE	WM Signal Output . This pin uses the internal totem-pole output driver to drive the power MOSFET. It is internally clamped below 15 V.			
3	VDD	Power Supply . IC operating current and MOSFET driving current are supplied using this pin. This pin is connected to an external V_{DD} capacitor of typically 10 μ F. The threshold voltages for startup and turn-off are 16 V and 5 V, respectively. The operating current is lower than 5 mA.			
4	COMR	Cable Compensation . This pin connects a capacitance between the COMR and GND pins for compensation voltage drop due to output cable loss in CV mode.			
5	VS	Voltage Sense . This pin detects the output voltage information and discharge time based on voltage of auxiliary winding.			
6	GND	Ground			
7	NC	No Connect			
8	HV	High Voltage. This pin connects to bulk capacitor for high-voltage startup.			

Absolute Maximum Ratings

Stresses exceeding the absolute maximum ratings may damage the device. The device may not function or be operable above the recommended operating conditions and stressing the parts to these levels is not recommended. In addition, extended exposure to stresses above the recommended operating conditions may affect device reliability. The absolute maximum ratings are stress ratings only.

Symbol	Parameter			Max.	Unit
V _{HV}	HV Pin Input Voltage			500	V
V _{VDD}	DC Supply Voltage ⁽¹⁾⁽²⁾			30	V
V _{VS}	VS Pin Input Voltage	e	-0.3	7.0	V
V _{CS}	CS Pin Input Voltage	e	-0.3	7.0	V
V _{COMV}	Voltage Error Amplif	fier Output Voltage	-0.3	7.0	V
V _{COMI}	Current Error Amplifier Output Voltage			7.0	V
PD	Power Dissipation (T _A <50°C)			660	mW
heta ja	Thermal Resistance (Junction-to-Air)			150	°C/W
heta JC	Thermal Resistance (Junction-to-Case)			39	°C/W
TJ	Operating Junction Temperature			+150	°C
T _{STG}	Storage Temperature Range			+150	°C
TL	Lead Temperature (+260	°C	
ESD	Electrostatic	Human Body Model, JEDEC-JESD22_A114	5000 1 2000		v
LOD	Discharge Capability Except HV Pin ⁽³⁾	Charged Device Model, JEDEC-ESD22_C101			Ň

Notes:

- 1. Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device.
- 2. All voltage values, except differential voltages, are given with respect to GND pin.
- 3. Including HV pin: HBM=500 V, CDM=750 V.

Recommended Operating Conditions

The Recommended Operating Conditions table defines the conditions for actual device operation. Recommended operating conditions are specified to ensure optimal performance to the datasheet specifications. Fairchild does not recommend exceeding them or designing to Absolute Maximum Ratings.

Symbol	Parameter	Min.	Max.	Unit
T _A	Operating Ambient Temperature	-40	+105	°C

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V _{DD} Section	า		
V _{OP}	Continuously Operating Voltage		
$V_{\text{DD-ON}}$	Turn-On Threshold Voltage	6	
$V_{\text{DD-OFF}}$	Turn-Off Threshold Voltage		
I _{DD-OP}	Operating Current		
I _{DD-GREEN}	Green-Mode Operating Supply Cur	rent	
V _{DD-OVP}	V _{DD} Over-Voltage Protection Level		

Parameter

V_{DD} Over-Voltage-Protection Debounce Time

Center Frequency

Frequency Hopping Range

Minimum Startup Voltage on HV Pin

Supply Current Drawn from Pin HV

Leakage Current after Startup

Frequency Hopping Period

Minimum Frequency at CCM

Minimum Frequency at No-Load

Frequency Variation vs. V_{DD} Deviation

Frequency Variation vs. Temperature

Green-Mode Starting Voltage on EA_V

Green-Mode Ending Voltage on EA_V

Propagation Delay to GATE Output

Threshold Voltage for Current Limit

Threshold Voltage on VS Pin Smaller than

Minimum On Time at No-Load

Adaptive Bias Voltage Dominated by VCOMV

Condition

V_{DC}=100 V

V_{DD}=10~25 V

fosc=-2 kHz

fosc=1 kHz

R_{VS}=20 kΩ

V_{COMR}=1 V

T_A=-40°C to +105°C

_{OFF} +1 V

HV=500 V, V_{DD}=V_{DD}-

Min.

15

4.5

90

47

±1.5

2.475

Typ.

16

5.0

3.2

0.95

28

200

1.2

0.5

50

±2.0

3

370

13

1

2.500

2.5

0.5

1.4

10

90

950

0.8

0.25

Max.

25

17

5.5

5.0

1.20

350

50

5.0

3.0

53

±2.5

2

15

2.525

200

Unit

V

V

V

mΑ

mΑ V

us

V

Hz

kHz

%

%

V V

V

V

μA

ns

ns

V

V

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Electrical Characteristics

HV Startup Current Source Section

Frequency

Deviation Voltage-Error-Amplifier Section

Reference Voltage

IC Bias Current

Symbol

t_{D-VDDOVP}

V_{HV-MIN}

 I_{HV}

I_{HV-LC}

fosc

t_{FHR}

fosc-n-min

fosc-cm-min f_{DV}

 \mathbf{f}_{DT}

V_{VR}

 V_N

 V_{G}

VBIAS-COMV

I_{tc}

t_{PD}

t_{MIN-N}

VTH

 V_{TL}

Voltage-Sense Section

Current-Sense Section

0.5 V

Oscillator Section

Unless otherwise specified, V_{DD} =15 V and T_A=25 °C.

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mΑ μA kHz ms

Symbol	Parameter	Condition	Min.	Тур.	Max.
•	rror-Amplifier Section				indixi
V _{IR}	Reference Voltage		2.475	2.500	2.525
Cable Con	npensation Section				
V _{COMR}	COMR Pin for Cable Compensation			0.85	
Gate Secti	ion				
DCY_MAX	Maximum Duty Cycle		76	81	86
V _{OL}	Output Voltage Low	V _{DD} =20 V, Gate Sinks 10 mA			1.5
V _{OH}	Output Voltage High	V _{DD} =8 V, Gate Sources 1 mA	5		
tr	Rising Time	C∟=1 nF		200	250
t _f	Falling Time	C _L =1 nF		60	100
V _{CLAMP}	Output Clamp Voltage	V _{DD} =25 V		15	18
Over-Tem	perature-Protection Section				
TOTP	Threshold Temperature for OTP ⁽⁴⁾			+140	

Note:

4. When the over-temperature protection is activated, the power system enters auto restart mode and output is disabled.

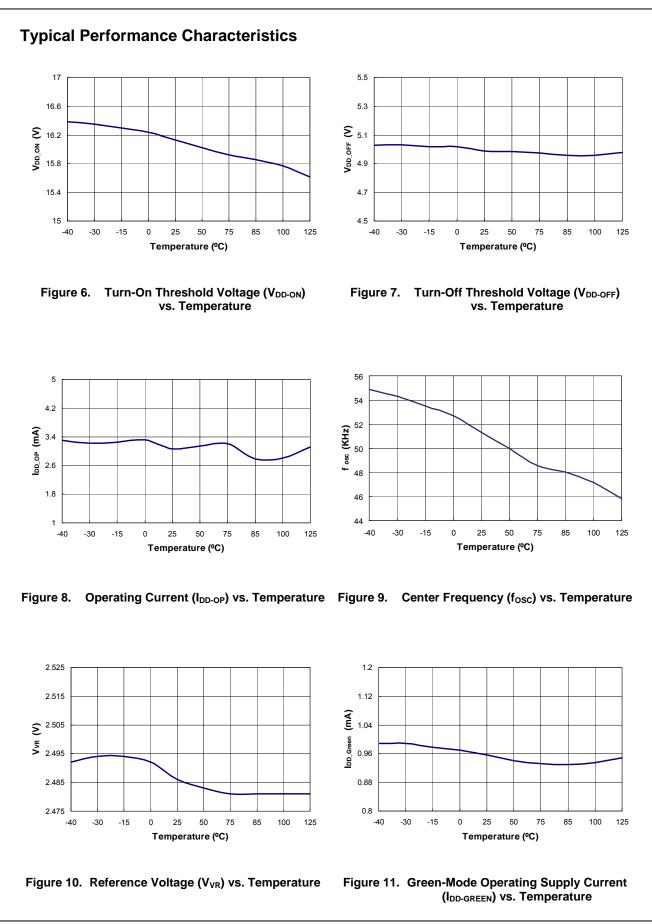
Unit

V

V

% V Ns ns V

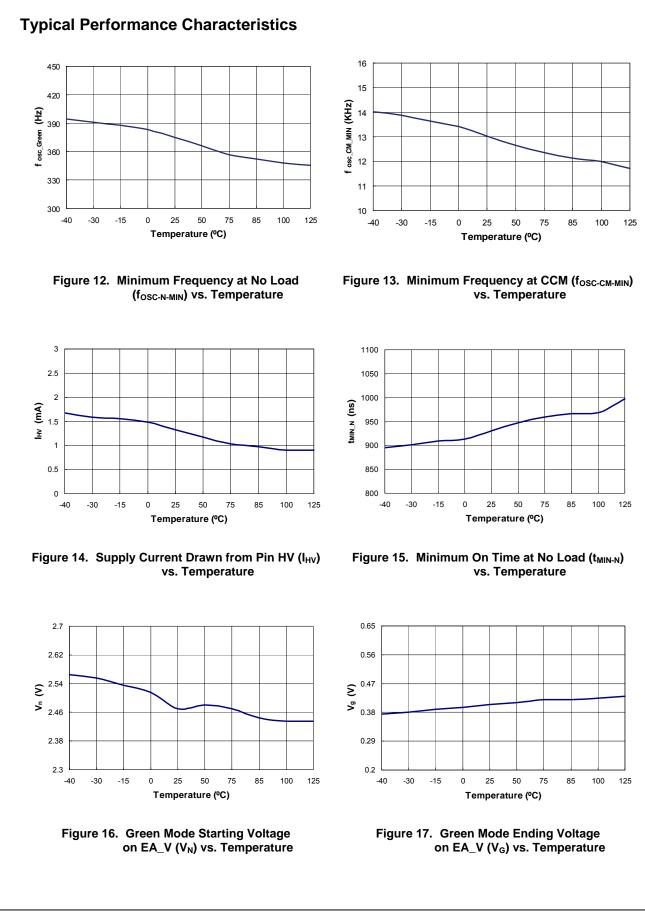
°C



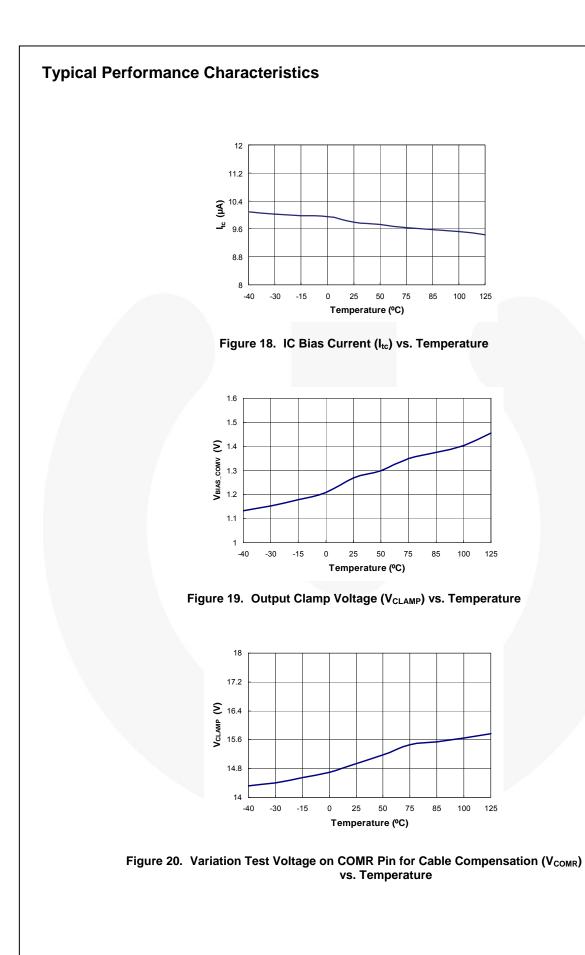
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Functional Description

Figure 21 shows the basic circuit diagram of a primaryside regulated flyback converter with typical waveforms shown in Figure 22. Generally, discontinuous conduction mode (DCM) operation is preferred for primary-side regulation since it allows better output regulation. The operation principles of DCM flyback converter are as follows:

During the MOSFET on time (t_{ON}) , input voltage (V_{DL}) is applied across the primary-side inductor (L_m). Then, MOSFET current (Ids) increases linearly from zero to the peak value (I_{nk}) . During this time, the energy is drawn from the input and stored in the inductor.

When the MOSFET is turned off, the energy stored in the inductor forces the rectifier diode (D) to be turned on. While the diode is conducting, the output voltage (V_o) , together with diode forward voltage drop (V_F) , are applied across the secondary-side inductor $(L_m \times N_s^2/N_s^2)$ $N_{\rm p}^{2}$) and the diode current (I_D) decreases linearly from the peak value $(I_{pk} \times N_p/N_s)$ to zero. At the end of inductor current discharge time (t_{DIS}), all the energy stored in the inductor has been delivered to the output.

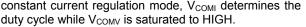
When the diode current reaches zero, the transformer auxiliary winding voltage (V_w) begins to oscillate by the resonance between the primary-side inductor (L_m) and the effective capacitor loaded across MOSFET.

During the inductor current discharge time, the sum of output voltage and diode forward-voltage drop is reflected to the auxiliary winding side as $(V_0+V_F) \times$ N_a/N_s . Since the diode forward-voltage drop decreases as current decreases, the auxiliary winding voltage reflects the output voltage best at the end of diode conduction time, where the diode current diminishes to zero. Thus, by sampling the winding voltage at the end of the diode conduction time, the output voltage information can be obtained. The internal error amplifier for output voltage regulation (EA_V) compares the sampled voltage with internal precise reference to generate error voltage (V_{COMV}), which determines the duty cycle of the MOSFET in CV mode.

Meanwhile, the output current can be estimated using the peak drain current and inductor current discharge time since output current is same as average of the diode current in steady state.

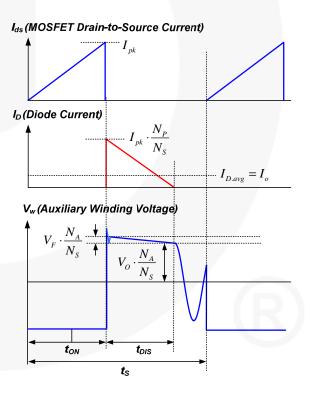
The output current estimator recognizes the peak value of the drain current with a peak-detection circuit and calculates the output current using inductor discharge time (t_{DIS}) and switching period (t_s). This output information is compared with internal precise reference to generate error voltage (V_{COMI}), which determines the duty cycle of the MOSFET in CC Mode. With Fairchild's innovative TRUECURRENT[®] technique, constant current (CC) output can be precisely controlled.

Among the two error voltages, V_{COMV} and V_{COMI} , the small one determines the duty cycle. Therefore, during constant voltage regulation mode, V_{COMV} determines the duty cycle while V_{COMI} is saturated to HIGH. During constant current regulation mode, V_{COMI} determines the duty cycle while V_{COMV} is saturated to HIGH.



V_{DI} VAC Gate EA CS lo Estimator R_{cs} Ret Vs P\//M t _{DIS} Detector Control V_{DD} N, COM Vo Estimator EA V Ref Primary-Side Regulation Controller

Figure 21. Simplified PSR Flyback Converter Circuit





Cable Voltage Drop Compensation

When it comes to cellular phone charger applications, the battery is located at the end of cable, which causes, typically, several percentage of voltage drop on the actual battery voltage. FAN103 has a built-in cable voltage drop compensation, which provides a constant output voltage at the end of the cable over the entire load range in CV mode. As load increases, the voltage drop across the cable is compensated by increasing the reference voltage of voltage regulation error amplifier.

Operating Current

The operating current in FAN103 is as small as 3.2 mA. The small operating current results in higher efficiency and reduces the V_{DD} hold-up capacitance requirement. Once FAN103 enters deep-green mode, the operating current is reduced to 0.95 mA, assisting the power supply in meeting power conservation requirements.

Green-Mode Operation

The FAN103 uses voltage regulation error amplifier output (V_{COMV}) as an indicator of the output load and modulates the PWM frequency, as shown in Figure 23. The switching frequency decreases as load decreases. In heavy load conditions, the switching frequency is fixed at 50 kHz. Once V_{COMV} decreases below 2.5 V, the PWM frequency linearly decreases from 50 kHz. When FAN103 enters into deep-green mode, the PWM frequency is reduced to a minimum frequency of 370 Hz, gaining power saving to help meet international power conservation requirements.

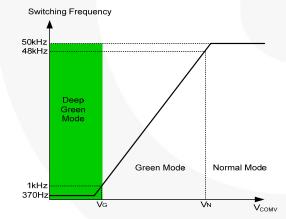
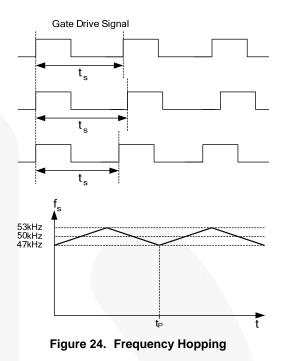


Figure 23. Switching Frequency in Green Mode

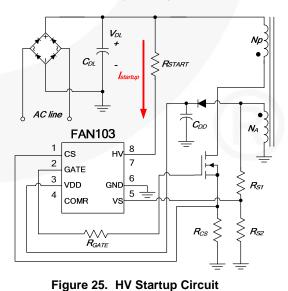
Frequency Hopping

EMI reduction is accomplished by frequency hopping, which spreads the energy over a wider frequency range than the bandwidth measured by the EMI test equipment. FAN103 has an internal frequency hopping circuit that changes the switching frequency between 47 kHz and 53 kHz with a period, as shown in Figure 24.



High-Voltage Startup

Figure 25 shows the HV-startup circuit for FAN103 applications. The HV pin is connected to the line input or bulk capacitor through a resistor, R_{START} (100 k Ω is recommended). During startup, the internal startup circuit in FAN103 is enabled. Meanwhile, line input supplies the current, $I_{STARTUP}$, to charge the hold-up capacitor, C_{DD} , through R_{START} . When the V_{DD} voltage reaches V_{DD-ON} , the internal startup circuit is disabled, blocking $I_{STARTUP}$ from flowing into the HV pin. Once the IC turns on, C_{DD} is the only energy source to supply the IC consumption current before the PWM starts to switch. Thus, C_{DD} must be large enough to prevent V_{DD} from dropping to V_{DD-OFF} before the power can be delivered from the auxiliary winding.



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Under-Voltage Lockout (UVLO)

The turn-on and turn-off thresholds are fixed internally at 16 V and 5 V, respectively. During startup, the hold-up capacitor must be charged to 16 V through the startup resistor to enable the FAN103. The hold-up capacitor continues to supply V_{DD} until power can be delivered from the auxiliary winding of the main transformer. V_{DD} is not allowed to drop below 5 V during this startup process. This UVLO hysteresis window ensures that hold-up capacitor properly supplies V_{DD} during startup.

Protections

The FAN103 has several self-protection functions, such as Over-Voltage Protection (OVP), Over-Temperature Protection (OTP), and Pulse-by-Pulse Current limit. All the protections are implemented as auto-restart mode. Once an abnormal condition occurs, switching is terminated and the MOSFET remains off, causing V_{DD} to drop. When V_{DD} drops to the V_{DD} turn-off voltage of 5 V, the internal startup circuit is enabled again, then the supply current drawn from HV pin charges the hold-up capacitor. When V_{DD} reaches the turn-on voltage of 16 V, FAN103 resumes normal operation. In this manner, the auto-restart alternately enables and disables the switching of the MOSFET until the abnormal condition is eliminated (see Figure 26).

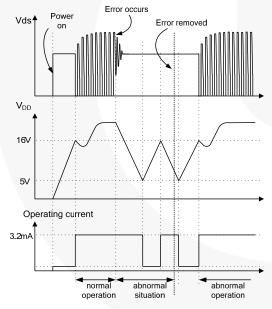


Figure 26. Auto Restart Operation

V_{DD} Over-Voltage Protection (OVP)

 V_{DD} over-voltage protection prevents damage from overvoltage conditions. If the V_{DD} voltage exceeds 28 V at open-loop feedback condition, OVP is triggered and the PWM switching is disabled. The OVP has a de-bounce time (typically 200 μs) to prevent false triggering due to switching noises.

Over-Temperature Protection (OTP)

The built-in temperature-sensing circuit shuts down PWM output if the junction temperature exceeds 140°C.

Pulse-by-pulse Current Limit

When the sensing voltage across the current sense resistor exceeds the internal threshold of 0.8 V, the MOSFET is turned off for the remainder of switching cycle. In normal operation, the pulse-by-pulse current limit is not triggered since the peak current is limited by the control loop.

Leading-Edge Blanking (LEB)

Each time the power MOSFET switches on, a turn-on spike occurs at the sense resistor. To avoid premature termination of the switching pulse, a leading-edge blanking time is built in. Conventional RC filtering can be omitted. During this blanking period, the currentlimit comparator is disabled and cannot switch off the gate driver.

Gate Output

The FAN103 output stage is a fast totem-pole gate driver. Cross conduction has been avoided to minimize heat dissipation, increase efficiency, and enhance reliability. The output driver is clamped by an internal 15 V Zener diode to protect power MOSFET transistors against undesired over-voltage gate signals.

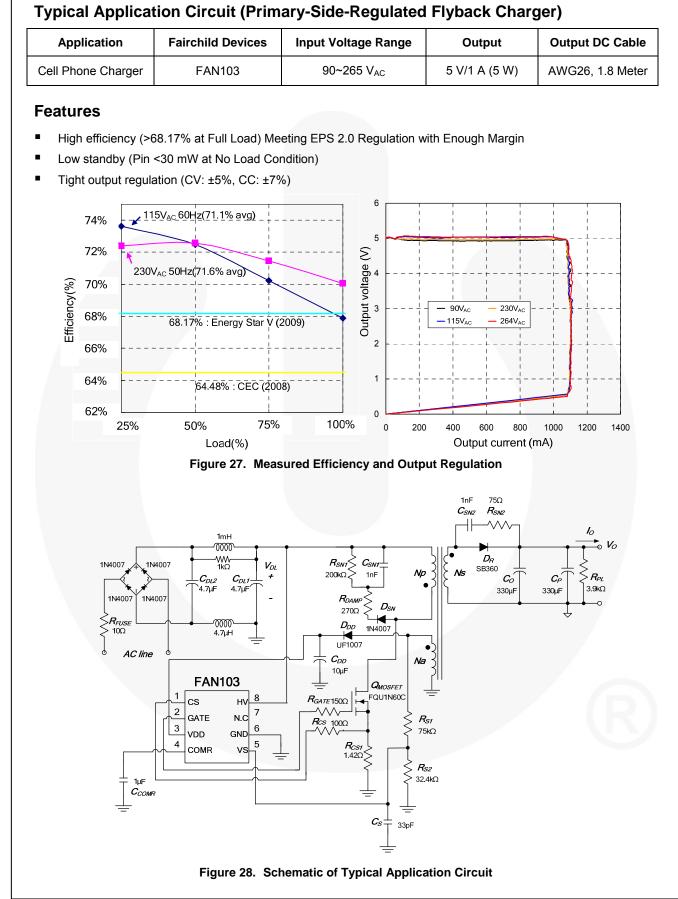
Built-in Slope Compensation

The sensed voltage across the current sense resistor is used for current mode control and pulse-by-pulse current limiting. Built-in slope compensation improves stability and prevents sub-harmonic oscillations due to peak-current mode control. The FAN103 has a synchronized, positive-slope ramp built-in at each switching cycle.

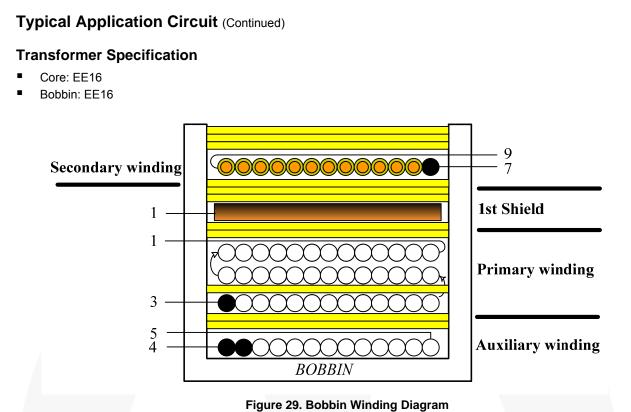
Noise Immunity

Noise from the current sense or the control signal can cause significant pulse-width jitter, particularly in continuous-conduction mode. While slope compensation helps alleviate these problems, further precautions should still be taken. Good placement and layout practices should be followed. Avoiding long PCB traces and component leads, locating compensation and filter components near the FAN103, and increasing the power MOS gate resistance is advised.

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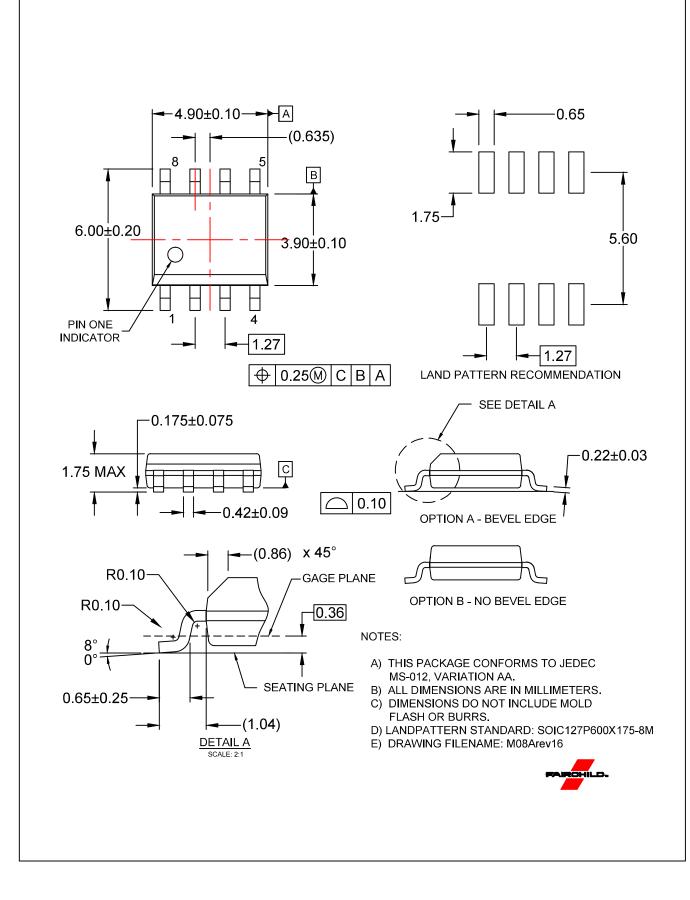
Notes:

- When W4R's winding is reversed winding, it must wind one layer. 5.
- When W2 is winding, put 1 layer tape after wind first layer. 6.

NO	TERM	IINAL	WIRE	Ta	INSULATION	BARRIER	
NO	S	F		Ts	Ts	Primary	Seconds
W1	4	5	2UEW 0.23*2	15	2		
				40	1		
W2	3	1	2UEW 0.17*1	40	0		
				37	2		
W3	1		COPPER SHIELD	1.2	3		
W4R	7	9	TEX-E 0.6*1	9	3		
			CORE ROUNDING TAPE		3		

	Pin	Specification	Remark
Primary-Side Inductance	1-3	1.75 mH ± 5%	100 kHz, 1 V
Primary-Side Effective Leakage	1-3	80 μH ± 5%	Short One of the Secondary Windings

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