# 1.5 A Adjustable and 3.3 V **Fixed Output Linear** Regulator

The NCP1086 linear regulator provides 1.5 A at 3.3 V or adjustable output voltage. The adjustable output voltage device uses two external resistors to set the output voltage within a 1.25 V to 5.5 V range.

The regulators is intended for use as post regulator and microprocessor supply. The fast loop response and low dropout voltage make this regulator ideal for applications where low voltage operation and good transient response are important.

The circuit is designed to operate with dropout voltages less than 1.4 V at 1.5 A output current. Device protection includes overcurrent and thermal shutdown.

This device is pin compatible with LT1086 family of line regulators and has lower dropout voltage.

The regulators are available in TO-220-3, surface mo D<sup>2</sup>PAK-3, and SOT-223 packages.

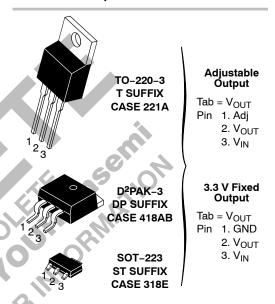
#### **Features**

- Output Current to 1.5 A
- Output Accuracy to ±1% Over Temperature
- Dropout Voltage (Typical) 1.05 V @ 1.5 A
- Fast Transient Response
- Fault Protection Circuitry
  - Current Limit
  - Thermal Shutdown
- Pb-Free Packages are Avan.



# ON Semiconductor®

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#### **ORDERING INFORMATION**

See detailed ordering and shipping information in the package dimensions section on page 9 of this data sheet.

#### **DEVICE MARKING INFORMATION**

See general marking information in the device marking section on page 10 of this data sheet.

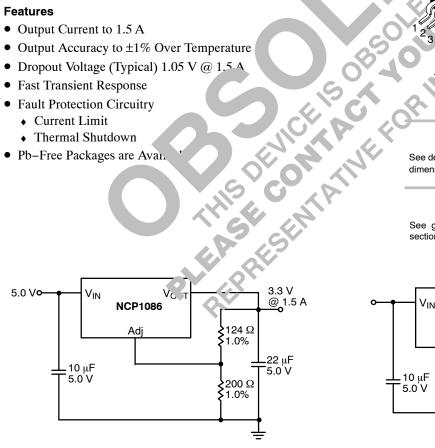


Figure 1. Application Diagram, Adjustable Output

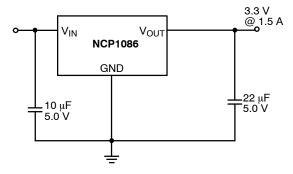


Figure 2. Application Diagram, 3.3 V Fixed Output

### **MAXIMUM RATINGS\***

Parameter	Value	Unit
Supply Voltage, V <sub>CC</sub>	7.0	٧
Operating Temperature Range	-40 to +70	°C
Junction Temperature	150	°C
Storage Temperature Range	-60 to +150	°C
Lead Temperature Soldering: Wave Solder (through hole styles only) Note 1 Reflow (SMD styles only) Note 2	260 Peak 230 Peak	°C
ESD Damage Threshold	2.0	kV

Stresses exceeding Maximum Ratings may damage the device. Maximum Ratings are stress ratings only. Functional operation above the Recommended Operating Conditions is not implied. Extended exposure to stresses above the Resonant American Conditions may affect device reliability.

- 1. 10 second maximum.
- 2. 60 second maximum above 183°C.

**ELECTRICAL CHARACTERISTICS** ( $C_{IN}$  = 10  $\mu$ F,  $C_{OUT}$  = 22  $\mu$ F Tantalum,  $V_{C}$ + V<sub>DROPC</sub>  $_{1N}$  < 7.0 V, 0°C ≤  $T_A$  ≤ 70°C,  $T_J \le +150^{\circ}C$ , unless otherwise specified,  $I_{full\ load} = 1.5\ A.$ )

IJ S +150 C, unless otherwise specified, Ifull load = 1.5 A.)									
Characteristic	Test Conditions	Min	Tr-c	Max	Unit				
ADJUSTABLE OUTPUT VOLTAGE	ADJUSTABLE OUTPUT VOLTAGE								
Reference Voltage (Notes 3 and 4)	$V_{IN} - V_{OUT} = 1.5 \text{ V}; V_{Adj} = 0 \text{ V},$ $10 \text{ mA} \le I_{OUT} \le 1.5$	1.241 (-1, )	1.2(4	1.266 (+1%)	V				
Line Regulation	1.5 V ≤ V <sub>IN</sub> – V ··· τ ≤ 5. V; I <sub>C</sub> = 10 · ¬A	<b>2</b> - 3	0.02	0.2	%				
Load Regulation (Notes 3 and 4)	V <sub>IN</sub> - V <sub>OU</sub> 1.5 V; mA - OUT = 1.5 A	CAI	0.04	0.4	%				
Dropout Voltage (Note 5)	I <sub>OUT</sub> = 1.5	ÇO.	1.05	1.4	V				
Current Limit	, V - √OLIT = C , J ≥ 25°C	1.6	3.1	-	Α				
Minimum Load Current (Note 6)	.u V, <sub>\dj</sub> = 0	-	0.6	2.0	mA				
Adjust Pin Current	V <sub>IN</sub> - = 3 CV: I <sub>OU</sub> = 7 5 mA	-	50	100	μΑ				
Thermal Regulation (Note 7)	3 is pulse: 1 = 20 C	-	0.002	0.02	%/W				
Ripple Rejection (Note	= $120  ^{1}$ $I_{OU}$ = 1.5 A; $V_{N} \cdot V_{OUT}$ = 3.0 V; $V_{R, SP, SE}$ = 1.5 $V_{P-P}$	-	80	-	dB				
Thermal Shutdown (N 98)		150	180	210	°C				
Thermal Shutdown Hyster	9	-	25	-	°C				
FIXED OUTPUT VOLTAGE	47								
Output Voltage (Notes 3 and 4)	$V_{IN}$ - $V_{OJT}$ = 1.5 V, $0 \le I_{OUT} \le 1.5$ A	3.25 (-1.5%)	3.3	3.35 (+1.5%)	V				
Line Regulation	$0.0 \text{ V} \le \text{V}_{\text{IN}} - \text{V}_{\text{OUT}} \le 3.7 \text{ V}; \text{I}_{\text{OUT}} = 10 \text{ mA}$	-	0.02	0.2	%				
Load Regulation (Notes 3 and 4)	$V_{IN} - V_{OUT}$ = 2.0 V; 10 mA $\leq$ I <sub>OUT</sub> $\leq$ 1.5 A	-	0.04	0.4	%				
Dropout Voltage (Note 5)	I <sub>OUT</sub> = 1.5 A	_	1.05	1.4	V				
Current Limit	V <sub>IN</sub> – V <sub>OUT</sub> = 3.0 V	1.6	3.1	-	Α				
Quiescent Current	I <sub>OUT</sub> = 10 mA	_	5.0	10	mA				
Thermal Regulation (Note 7)	30 ms pulse; T <sub>A</sub> = 25°C	-	0.002	0.02	%/W				

- 3. Load regulation and output voltage are measured at a constant junction temperature by low duty cycle pulse testing. Changes in output voltage due to thermal gradients or temperature changes must be taken into account separately.
- 4. Specifications apply for an external Kelvin sense connection at a point on the output pin 1/4" from the bottom of the package.
- 5. Dropout voltage is a measurement of the minimum input/output differential at full load.
- 6. The minimum load current is the minimum current required to maintain regulation. Normally the current in the resistor divider used to set the output voltage is selected to meet the minimum requirement.
- 7. Guaranteed by design, not 100% tested in production.8. Thermal shutdown is 100% functionally tested in production.

**ELECTRICAL CHARACTERISTICS (continued)** ( $C_{IN}$  = 10  $\mu$ F,  $C_{OUT}$  = 22  $\mu$ F Tantalum,  $V_{OUT}$  +  $V_{DROPOUT}$  <  $V_{IN}$  < 7.0 V, 0°C  $\leq$  T<sub>A</sub>  $\leq$  70°C, T<sub>J</sub>  $\leq$  +150°C, unless otherwise specified, I<sub>full load</sub> = 1.5 A.)

Characteristic	Test Conditions	Min	Тур	Max	Unit		
FIXED OUTPUT VOLTAGE (continued)							
Ripple Rejection (Note 9)	$f = 120 \text{ Hz; } I_{OUT} = 1.5 \text{ A; } V_{IN} - V_{OUT} = 3.0 \text{ V;} \\ V_{RIPPLE} = 1.0 \text{ V}_{P-P}$	-	80	ı	dB		
Thermal Shutdown (Note 10)	-	150	180	210	°C		
Thermal Shutdown Hysteresis (Note 10)	-	_	25	_	°C		

<sup>9.</sup> Guaranteed by design, not 100% tested in production.

# PACKAGE PIN DESCRIPTION, ADJUSTABLE OUTPUT

Pa	Package Pin Number				
D <sup>2</sup> PAK-3	TO-220-3	SOT-223	Pin Symbol	Function	
1	1	1	Adj	A st pin (lo. 'de of the internal re'arence).	
2	2	2	V <sub>OUT</sub>	Reo .ed output voltage (case)	
3	3	3	V <sub>IN</sub>	ut vol <sup>v</sup> ,e.	

# PACKAGE PIN DESCRIPTION, 3.3 V FIXED OUTPUT

Pa	ıckage Pin Numb	per		CO III CIVI
D <sup>2</sup> PAK-3	TO-220-3	SOT-223	Pin Sym	Function
1	1	1		Ground connection.
2	2	2	V <sub>OU7</sub>	Regulater cortput voltage (case).
3	3		V <sub>IN</sub>	Input vettige.

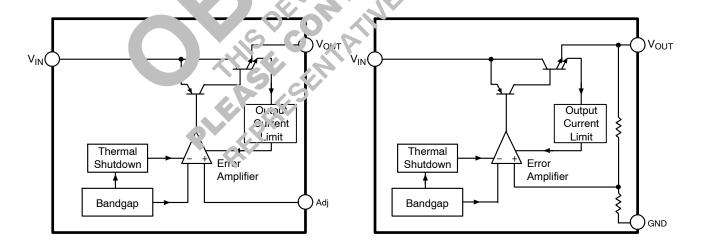
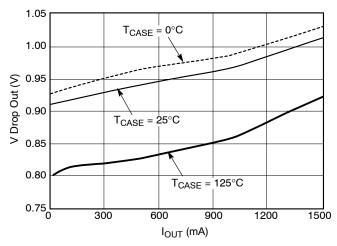


Figure 3. Block Diagram, Adjustable Output

Figure 4. Block Diagram, 3.3 V Fixed Output

<sup>10.</sup> Thermal shutdown is 100% functionally tested in production.

### TYPICAL PERFORMANCE CHARACTERISTICS



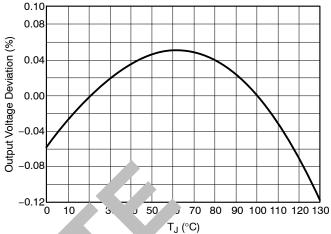
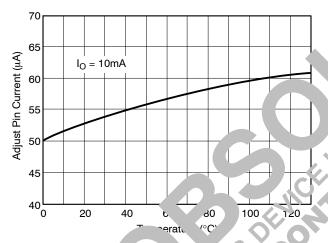


Figure 5. Dropout Voltage vs. Output Current

. ıguı Reference Voltage vs. Temperature



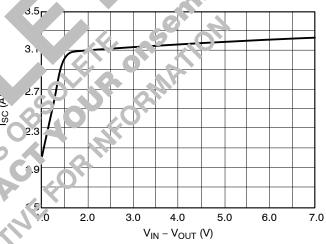
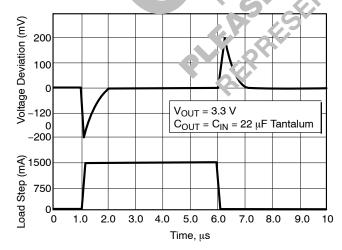


Figure 7. Adjust in Curi t vs. fempe atula (Ao stable C put)

Figure 8. Short Circuit Current vs V<sub>IN</sub> - V<sub>OUT</sub>



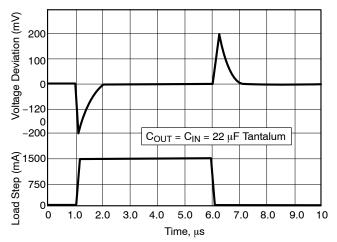


Figure 9. Transient Response (Adjustable Output)

Figure 10. Transient Response (3.3 V Fixed Output)

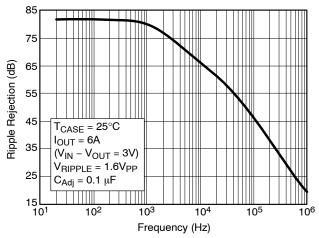
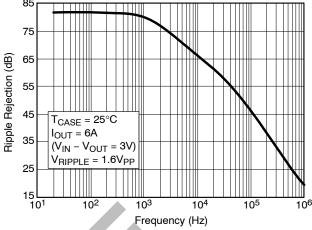


Figure 11. Ripple Rejection vs. Frequency (Adjustable Output)



Figu 12. pple Rejection vs. Frequency (3.3 ixed Output)

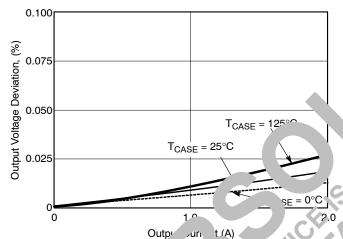


Figure 13. Load Regintion ... itput Corrent (Adjusta, utpu

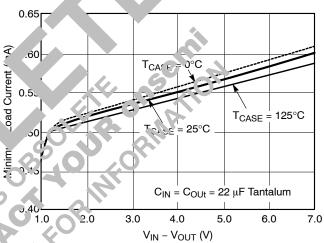


Figure 14. Minimum Load Current vs V<sub>IN</sub> – V<sub>OUT</sub> (Adjustable Output)

# AFPLICATIONS INFORMATION

The NCP1086 voltage regulator series recides adjustable and 3.3 V output voltages recurrent reported 1.5 A. The regulator is protected against overcore conditions and includes thermal shutdown

The NCP1086 series has a composite NCP-NPN output transistor and requires an output capacitor for stability. A detailed procedure for selecting this capacitor is included in the Stability Considerations section.

### **Adjustable Operation**

The adjustable output device has an output voltage range of 1.25 V to 5.5 V. An external resistor divider sets the output voltage as shown in Figure 15. The regulator maintains a fixed 1.25 V (typical) reference between the output pin and the adjust pin.

A resistor divider network R1 and R2 causes a fixed current to flow to ground. This current creates a voltage across R2 that adds to the 1.25 V across R1 and sets the overall output voltage. The adjust pin current (typically  $50~\mu A$ ) also flows through R2 and adds a small error that should be taken into account if precise adjustment of  $V_{OUT}$  is necessary.

The output voltage is set according to the formula:

$$V_{OUT} = V_{REF} \times \left(\frac{R1 + R2}{R1}\right) + I_{Adj} \times R2$$

The term  $I_{Adj} \times R2$  represents the error added by the adjust pin current.

R1 is chosen so that the minimum load current is at least 2.0 mA. R1 and R2 should be the same type, e.g. metal film for best tracking over temperature.

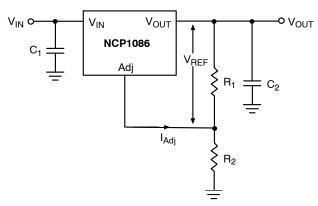


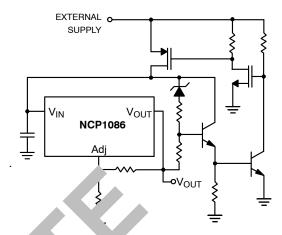
Figure 15. Resistor Divider Scheme

The adjustable output linear regulator has an absolute maximum specification of 7.0 V for the voltage difference between  $V_{\rm IN}$  and  $V_{\rm OUT}$ . However, the IC may be used to regulate voltages in excess of 7.0 V. The main considerations in such a design are powerup and short circ apability.

In most applications, ramp-up of the power supp<sup>1</sup> is fairly slow, typically on the order of seve I tens milliseconds, while the regulator responds in le than one microsecond. In this case, the linear late begir charging the load as soon as the V<sub>IN</sub> to OUT differential is large enough that the pass transistor co cu. nt. The load at this point is essentially rund, and 2 suppry ην, ...in the result voltage is on the order of sever nun that the pass transistor is in  $\alpha$ . As  $e \sup_{\lambda} v_{\lambda}$ . increases, the pass transfer we seem a in dispose, and current is passed to t' 10ad to 1 V<sub>t</sub> reaches the point at which the IC is in regulation. If ther increase in the supply voltage brings the paransis out of dropo. The result is that the output voltage . . . ws the power sur ply rand-up, staying in dropout until the regulation point is reached. In this manner, any output voltage may regular a. There is no theoretical limit to the regulate voltage as long as the  $V_{IN}$  to  $V_{OUT}$  differential of 7.0  $\checkmark$  is not  $\checkmark$  ceeded.

However, the possibility of destroying the IC in a short circuit condition is very real for this type of design. Short circuit conditions will result in the immediate operation of the pass transistor outside of its safe operating area. Overvoltage stresses will then cause destruction of the pass transistor before overcurrent or thermal shutdown circuitry can become active. Additional circuitry may be required to clamp the V<sub>IN</sub> to V<sub>OUT</sub> differential to less than 7.0 V if fail–safe operation is required. One possible clamp circuit is illustrated in Figure 16; however, the design of clamp circuitry must be done on an application by application basis. Care must be taken to ensure the clamp actually protects the design. Components used in the clamp design

must be able to withstand the short circuit condition indefinitely while protecting the IC.



Figu. e 16. Port Circuit Protection Circuit for High Voltage Application

### y Considerations ،

three . In characteristic, of a life a regulator: startup delay, load ransient response and load stability.

The capacitor due and type is based on cost, availability, size 2.11 temper ture constraints. A tantalum or aluminum electrolytic apacitor is best, since a film or ceramic expacitor with about zero ESR can cause instability. The alminum electrolytic capacitor is the least expensive solution. For ever, when the circuit operates at low temperatures, both the value and ESR of the capacitor will vary considerably. The capacitor manufacturers' data sheet provides this information.

A 22  $\mu F$  tantalum capacitor will work for most applications, but with high current regulators such as the NCP1086 series the transient response and stability improve with higher values of capacitance. The majority of applications for this regulator involve large changes in load current, so the output capacitor must supply the instantaneous load current. The ESR of the output capacitor causes an immediate drop in output voltage given by:

$$\Delta V = \Delta I \times ESR$$

For microprocessor applications it is customary to use an output capacitor network consisting of several tantalum and ceramic capacitors in parallel. This reduces the overall ESR and reduces the instantaneous output voltage drop under load transient conditions. The output capacitor network should be as close as possible to the load for the best results.

#### **Protection Diodes**

When large external capacitors are used with a linear regulator it is sometimes necessary to add protection diodes. If the input voltage of the regulator gets shorted, the output capacitor will discharge into the output of the regulator. The discharge current depends on the value of the capacitor, the output voltage and the rate at which  $V_{\rm IN}$  drops. In the NCP1086 series linear regulator, the discharge path is through a large junction and protection diodes are not usually needed. If the regulator is used with large values of output capacitance and the input voltage is instantaneously shorted to ground, damage can occur. In this case, a diode connected as shown in Figure 17 or Figure 18 is recommended.

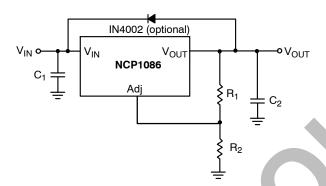


Figure 17. Protection Diode Scheme for larg hutput Capacitors (Adjustable C. put)

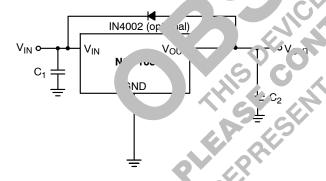


Figure 18. Protection Diode Scheme for Large Output Capacitors (3.3 V Fixed Output)

#### **Output Voltage Sensing**

Since the NCP1086 is a three terminal regulator, it is not possible to provide true remote load sensing. Load regulation is limited by the resistance of the conductors connecting the regulator to the load.

For best results the fixed output regulator should be connected as shown in Figure 19.

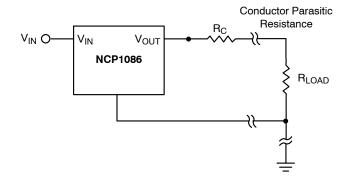


Figure 19. Conductor Parasitic Resistance Effects
Can Be Minimized with the Above Grounding
Scheme / Fixed Output Regulators

For the actus, 'regul' or, the best load regulation occurs whe R1 is consecuted to the output pin of the regulation own in regulation own in regulation of the load' R<sub>C</sub> is must lied by the divider ratio and the effective restance between the regulator and the load becomes

$$R_C \times \frac{(1) + R_2}{R_1}$$

where  $R_C = c$  inductor parasition resistance.

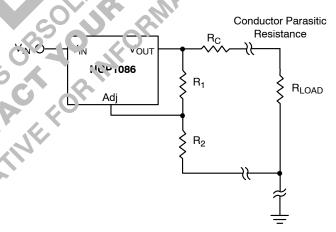


Figure 20. Grounding Scheme for the Adjustable Output Regulator to Minimize Parasitic Resistance Effects

# Calculating Power Dissipation and Heatsink Requirements

The NCP1086 linear regulator includes thermal shutdown and current limit circuitry to protect the device. High power regulators such as these usually operate at high junction temperatures so it is important to calculate the power dissipation and junction temperatures accurately to ensure that an adequate heatsink is used.

The case is connected to V<sub>OUT</sub>, and electrical isolation may be required for some applications. Thermal compound should always be used with high current regulators such as these.

The thermal characteristics of an IC depend on the following four factors:

- Maximum Ambient Temperature T<sub>A</sub> (°C)
- 2. Power dissipation  $P_D$  (W)
- Maximum junction temperature T<sub>J</sub> (°C)
- Thermal resistance junction to ambient  $R_{\theta JA}$  (°C/W)

These four are related by the equation

$$T_J = T_A + P_D \times R_{\theta JA}$$
 (eq. 1)

The maximum ambient temperature and the power dissipation are determined by the design while the maximum junction temperature and the thermal resistance depend on the manufacturer and the package type.

The maximum power dissipation for a regulator is:

$$P_{D(max)} = \{V_{IN(max)} - V_{OUT(min)}\}I_{OUT(max)} + V_{IN(max)}I_{Q}$$

(eq. 2)

where:

 $V_{IN(max)}$  is the maximum input voltage,

V<sub>OUT(min)</sub> is the minimum output voltage,

I<sub>OUT(max)</sub> is the maximum output current, for the plication

Io is the maximum quiescent current at Io max

A heatsink effectively increases the artace area package to improve the flow of heat a into the surrounding air.

Each material in the heat flow path between the IC and the outside environment has a thermal resistance. Like series electrical resistances, these resistances are summed to determine  $R_{\theta JA}$ , the total thermal resistance between the junction and the surrounding air.

- Thermal Resistance of the junction to case,  $R_{\theta JC}$  $(^{\circ}C/W)$
- Thermal Resistance of the case to Heatsink,  $R_{\theta CS}$  $(^{\circ}C/W)$
- Thermal Resistance of the Heatsink to the ambient air,  $R_{\theta SA}$  (°C/W)

These are connected by the equation:

$$R_{\theta}JA = R_{\theta}JC + R_{\theta}CS + R_{\theta}SA$$
 (eq. 3)

The value for R \( \) is calculated using Equation 3 and the result can be su itut in Equation 1.

The valve for C is S°C/W. For a high current h as the 1086 the majority of the heat is regulator genera d in e power transistor section. The value for  $R_{\rm f}$  depends the heatsink type, while  $R_{\rm \theta CS}$  depends on tors uch as package type heatsink interface (is an or ar thermal greas (sed?), and the contact area bet in he heatsink win the pickage. Once these ons

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IC and calcultions are complete, the maximum permissible value of JA can be conculated and the proper heatsink selected. r further dis viction or and tsink selection, see application note "Then. "I Ma. agement," document number A) 1/803c T via our vebsite at www.onsemi.com.

# **ORDERING INFORMATION**

Device	Туре	Package	Shipping <sup>†</sup>
NCP1086D2T-ADJ		D <sup>2</sup> PAK	50 Units/Rail
NCP1086D2T-ADJG		D <sup>2</sup> PAK (Pb-Free)	50 Units/Rail
NCP1086D2T-ADJR4		D <sup>2</sup> PAK	
NCP1086D2TADJR4G		D <sup>2</sup> PAK (Pb-Free)	750 Tape & Reel
NCP1086ST-ADJT3	Adjustable	SOT-223	
NCP1086ST-ADJT3G		SOT-223 (Pb-Free)	2500 Tape & Reel
NCP1086T-ADJ		TO220	4
NCP1086T-ADJG		TO220 (Pb-Free)	50 Units/Rail
NCP1086D2T-033		D <sup>2</sup> PAK	50 Units/Rail
NCP1086D2T-33R4		D <sup>2</sup> F	
NCP1086D2T-33R4G		(br 3)	750 Tape & Reel
NCP1086ST-33T3	3.3 V	SOT-2.	
NCP1086ST-33T3G	3.3 V	SOT- 3	25∪0 Tape & Reel
NCP1086T-033		10220	OPA!
NCP1086T-033G		たつとつ (i`h- Free)	50 Units/Rail
For information on tape and Specifications Brochure, BRD	08011/D.	ng part orientation and tape sizes, p	olease refer to our Tape and Reel Packagii

<sup>†</sup>For information on tape and reel specific ons Specifications Brochure, BRD8011/D.

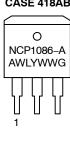
#### **MARKING DIAGRAMS**

#### **Adjustable Output**

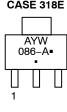
TO-220-3 T SUFFIX CASE 221A



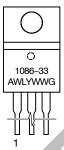
D<sup>2</sup>PAK-3 **D2T SUFFIX** CASE 418AB



SOT-223 ST SUFFIX **CASE 318E** 

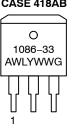


TO-220-3 **T SUFFIX** CASE 221A

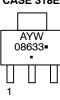


## 3.3 V Fixed Output

D<sup>2</sup>PAK-3 **D2T SUFFIX** CASE 418AB



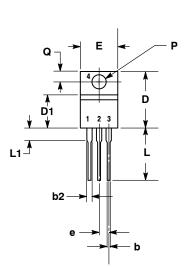


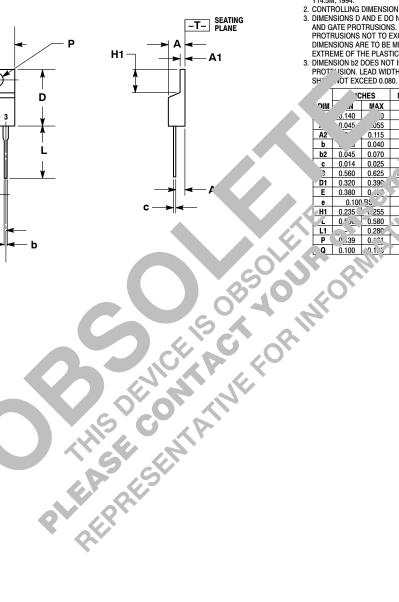


PAR PRESENTATIVE OF INFORMATION

#### PACKAGE DIMENSIONS

## TO-220 3-LEAD **T SUFFIX** CASE 221AF-01 **ISSUE A**





- NOTES:

  1. DIMENSIONING AND TOLERANCING PER ASME Y14.5M, 1994.

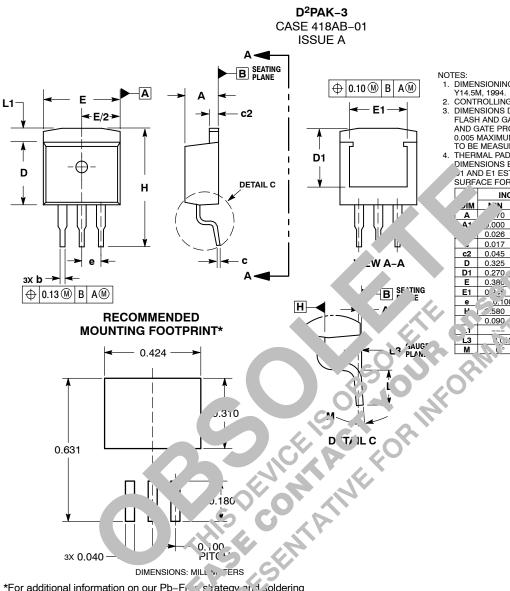
  2. CONTROLLING DIMENSION: INCHES.
- 2. CONTROLLING DIMENSION. INCHES.

  3. DIMENSIONS D AND E DO NOT INCLUDE MOLD FLASH AND GATE PROTRUSIONS. MOLD FLASH AND GATE PROTRUSIONS NOT TO EXCEED 0.005 PER SIDE. THESE DIMENSIONS ARE TO BE MEASURED AT OUTERMOST
- EXTREME OF THE PLASTIC BODY.

  3. DIMENSION 62 DOES NOT INCLUDE DAMBAR PROTE'ISION. LEAD WIDTH INCLUDING PROTRUSION NOT EXCEED 0.080.

	)'C	HES	MILLIN	IETERS	
MIC	N	.N MAX		MAX	
	J.140	)	3.56	4.83	
	0 <u>.04</u> 5	.055	1.14	1.40	
A2	. ~ .	0.115	2.03	2.92	
b	ر	0.040	0.64	1.02	
b2	0.045	0.070	1.14	1.78	
C	0.014	0.025	U 15	0.64	
)	0.560	0.625	, o <sub>2</sub>	15.88	
D1	0.320	0.390	3.13	9.91	
Е	0.380	0	9.65	10.67	
е	0.100	BE .	2.54	700	
<u>H1</u>	0.235	255	£ 97	6.48	
	0 . ′′	0.580	.ou	14.73	
Ľ1_		0.280	7 -	7.11	
P	n ,39	0.101	3.53	4.09	
Q	0.100	0.1.5	2.54	3.43	

#### PACKAGE DIMENSIONS



### NOTES:

- NOTES:

  1. DIMENSIONING AND TOLERANCING PER ASME Y14.5M, 1994.
  2. CONTROLLING DIMENSION: INCHES.
  3. DIMENSIONS D AND E DO NOT INCLUDE MOLD FLASH AND GATE PROTRUSIONS. MOLD FLASH AND GATE PROTRUSIONS NOT TO EXCEED 0.005 MAXIMUM PER SIDE. THESE DIMENSIONS TO BE MEASURED AT DATUM H.
- THERMAL PAD CONTOUR OPTIONAL WITHIN DIMENSIONS E, L1, D1, AND E1. DIMENSIONS 1 AND E1 ESTABLISH A MINIMUM MOUNTING SURFACE FOR THE THERMAL PAD.

4	INC	HES	MILLIM	IETERS
<u> ۱M/د</u>	V MAX		MIN	MAX
_A_	/0	0.180	4.32	4.57
Δ1	000.د	0.010	0.00	0.25
. 4	0.026	0.036	0.66	0.91
	0.017	0.026	0.43	0.66
c2	0.045	055	1.14	1.40
D	0.325	0. <u>~ 38</u>	8.25	9.53
D1	0.270	1 7 THE	6.86	-
E	0.380	0.420	9.65	10.67
E1	0 > 6		6.22	-
е	v.100	BSC	2.54	BSC
P	∠.580	<u>(</u> 62( _	14.73	15.75
K 🔪	0.090	1110	2.29	2.79
.1		0.066		1.68
L3	2.	BSC	0.25	BSC
М		8°	0°	8°

# PACKAGE THERMAL D.V.A

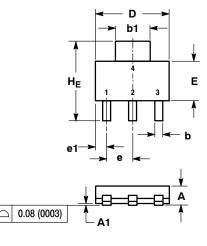
Parameter		TO-220-3	D <sup>2</sup> PAK-3	SOT-223	Unit
$R_{ heta JC}$	Typical	3.5	3.5	15	°C/W
$R_{\theta JA}$	Typical	50	10–50*	156	°C/W

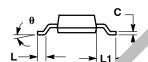
<sup>\*</sup> Depending on thermal properties of substrate.  $R_{\theta JA}$  =  $R_{\theta JC}$  +  $R_{\theta CA}$ 

<sup>\*</sup>For additional information on our Pb-Fi shategvand soldering details, please download the ON S miconductor Soldering and Mounting Techniques Reference is allual, SOLDERRM/D.

#### PACKAGE DIMENSIONS

SOT-223 (TO-261) ST SUFFIX CASE 318E-04 **ISSUE N** 

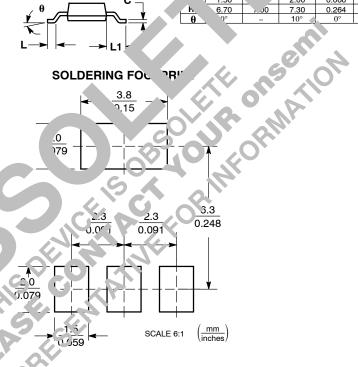




- DIMENSIONING AND TOLERANCING PER ASME Y14.5M, 1994.
- CONTROLLING DIMENSION: INCH

	MILLIMETERS			INCHES		
DIM	MIN	NOM	MAX	MIN	NOM	MAX
Α	1.50	1.63	1.75	0.060	0.064	0.068
A1	0.02	0.06	0.10	0.001	0.002	0.004
b	0.60	0.75	0.89	0.024	0.030	0.035
b1	2.90	3.06	3.20	0.115	0.121	0.126
С	0.24	0.29	0.35	0.009	0.012	0.014
D	6	6.70	6.70	0.249	0.256	0.263
E	5	J	3.70	0.130	0.138	0.145
е		30	2.40	0.087	0.091	0.094
e′	3.0	0.94	1.05	0.033	0.037	0.041
47	0.20	T.		0.008		
	1.50	$^{L}$	2.00	0.060	0.069	0.078
<u>_h_</u>	6.70	0ر ،	7.30	0.264	0.276	0.287
θ	J <sub>o</sub>	_	10°	0°	_	10°





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